## REVISED TRAFFIC

 ANALYSIS SUPPLEMENTAL TECHNICAL REPORTOregon Department of Transportation December 7, 2023

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## Executive Summary

This Revised Traffic Analysis Supplemental Technical Report provides the traffic analysis results of the 2045 Revised Build Alternative and compares those with the updated traffic analysis results of the 2045 No-Build Alternative. Updated and/or revised information since the 2022 Land Use Supplemental Technical Report is shown in bold text. The 2045 Revised Build Alternative is expected to improve traffic operations on both the I-5 mainline and local street system when compared to the 2045 No-Build Alternative. There are locations where certain modes may experience a degradation in performance, but, in general, traffic, bicycle/pedestrian, and transit operations will be improved in the study area.

The 2045 Revised Build Alternative design elements on the freeway segments are similar to those in the Build Alternative with continuous auxiliary lanes in both northbound and southbound directions and 12 -foot right shoulders. The 2045 Revised Build Alternative would provide narrower median shoulders when compared to the Build Alternative but wider than those in the 2045 No-Build Alternative. Freeway and weaving segment lengths and traffic volumes in the 2045 Revised Build Alternative would be similar to those proposed in the Build Alternative. The minor differences are not expected to cause a substantive difference to the expected mainline operational benefits identified in the 2019 Traffic Analysis Technical Report.

For the local street analysis, the 2045 Revised Build Alternative would also include a new local street connection of NE Hancock Street to N Flint Avenue and relocation of the I-5 southbound off-ramp (exit ramp) from N Broadway to $\mathbf{N}$ Williams Avenue at NE Wheeler Avenue (westbound) and to NE Weidler Street at NE Victoria Avenue (eastbound). The exit ramp would divide westbound traffic from eastbound traffic, with a single lane connection at N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way and single lane bridge (flyover) over I-5 to connect with NE Weidler Street. The new I-5 southbound exit ramp will add a second right turn lane at the intersection of NE Weidler Street/ NE Victoria Avenue adjacent to the right turn lane from the I-5 northbound exit ramp. The traffic volumes on the local streets in the 2045 Revised Build Alternative are generally higher than those forecast for the 2045 No-Build Alternative. This Revised Traffic Analysis Supplemental Technical Report also evaluates two design options of the Revised Build Alternative for the local street circulation: 2-way Ramsay Design Option and 2-way Wheeler Design Option. Both design options would allow traffic from the relocated I-5 southbound exit ramp at $\mathbf{N}$ Wheeler Avenue/ N Williams Avenue/ N Ramsay Way to turn left onto southbound N Williams Avenue. The 2-way Ramsay Design Option would convert the existing one-way eastbound N Ramsay Way between NE Wheeler Avenue and N Center Court Street into a 2-way street, allowing westbound travel for the l-5 southbound exit ramp traffic. The 2-way Wheeler Design Option would convert

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N Wheeler Avenue and N Vancouver Avenue between N Ramsay Way and N/ NE Broadway to a 2-way street and add a new travel lane in the northbound direction. This would allow traffic from the I-5 southbound exit ramp traffic to access westbound N Broadway.

Bicycle volumes for both the 2045 No-Build and 2045 Revised Build Alternative have been updated to reflect higher baseline bicycle volumes. These updates are based on additional existing bicycle counts provided by the City of Portland and an anticipated increase in bicycle mode share as forecast in the City of Portland's Central City 2035 Comprehensive Plan mode share target for bicycles within the Central City.

## 2045 Revised Build Alternative - Freeway Analysis

The 2045 Revised Build Alternative would improve traffic operations at all freeway segments including the four weaving segments below in both the AM (7:00 AM to 9:00 AM) and PM (4:00 PM to 6:00 PM) analysis periods when compared to the 2045 No-Build Alternative:

- I-5 NB between the I-84 entrance ramp and NE Weidler Street exit ramp
- I-5 NB between the N Broadway entrance ramp and I-405 exit ramp
- I-5 SB between I-405 entrance ramp and N Broadway exit ramp
- I-5 SB between the N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way entrance ramp and I-84 exit ramp


## 2045 Revised Build Alternative - Local Street Analysis

Traffic operations for local street intersections under the 2045 No-Build and 2045 Revised Build Alternative were updated and evaluated using both Synchro and Vissim analysis. The traffic analysis using Synchro indicates that under the 2045 Revised Build Alternative, all study intersections would operate at acceptable ${ }^{1}$ Level of Service (LOS) except for the $\mathbf{N}$ Wheeler Avenue/ N Williams Avenue/ N Ramsay Way and I-5 southbound entrance and exit ramp terminal intersection, which will operate at LOS E. Compared to the 2045 No-Build Alternative, the 2045 Revised Build Alternative shows LOS would improve at the intersection of N Broadway and N Vancouver Avenue from LOS F in the AM peak hour to LOS B for the 2-way Ramsay Design Option and LOS C for the 2-way Wheeler Design Option. The I-5 northbound exit ramp terminal intersection at NE Weidler Street/ NE Victoria Avenue would improve from LOS E in the AM peak hour to LOS C in both design options.

[^0]The l-5 southbound exit ramp terminal intersection at $\mathbf{N}$ Wheeler Avenue/ N Williams Avenue/ N Ramsay Way is expected to exceed the Highway Design Manual (HDM) mobility target (v/c of 0.75 or lower) in the AM and PM peak hours in both design options. The I-5 northbound exit ramp terminal intersection at NE Weidler Street/ NE Victoria Avenue is expected to exceed the HDM mobility target (v/c of 0.75 or lower.) during the AM peak hour in both design options.

As part of the adoption of the Central City 2035 Plan, the Central City, which includes the I-5 ramp terminal intersections, has been designated as a Multimodal Mixed-Use Area (MMA). This designation provides flexibility for determining effects of land use actions by lifting mobility standards requirements at ODOT facilities. Transportation standards such as safety and multimodal access still apply. Although both ramp terminal intersections exceed the HDM mobility target, the Revised Build Alternative reduces exit ramp queuing and provides bicycle and pedestrian crossing improvements.

Vissim microsimulation analysis results indicate that under the 2045 Revised Build Alternative all intersections would operate at LOS D or better in the AM and PM peak hours for both design options and LOS of several intersections would improve compared to the 2045 No-Build condition. The I-5 northbound exit ramp at the intersection of NE Weidler Street/ NE Victoria Avenue will operate at LOS E in the 2045 No-Build Alternative in both the AM and PM peak hours. In comparison, under the 2045 Revised Build Alternative this intersection will operate at LOS B and C in the AM and PM peak hours, respectively, in both design options.

In the 2045 No-Build Alternative, the N Broadway/N Vancouver Avenue and I-5 southbound exit ramp terminal intersection will operate at LOS F in the PM peak hour. When relocated in the 2045 Revised Build Alternative, the l-5 southbound exit ramp intersection at $\mathbf{N}$ Wheeler Avenue/ N Williams Avenue/ N Ramsay Way would operate at LOS D in both design options. When comparing operations for the I-5 southbound exit ramp in the PM peak hour, the exit ramp approach is operating at LOS F in the 2045 No-Build Alternative at the N Broadway/ N Vancouver Avenue intersection and LOS D in the 2045 Revised Build Alternative at the N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way intersection. The flyover portion of the l-5 southbound exit ramp approach at the NE Weidler Street/ NE Victoria Avenue intersection is operating at LOS C.

Vissim results indicate that $95^{\text {th }}$ percentile queue lengths on the l-5 northbound and southbound exit ramps will not exceed the proposed ramp storage length approaching both ramp terminals in both design options of the 2045 Revised Build Alternative. In comparison, both the I-5 northbound and southbound exit ramp queues exceed the available ramp storage in either the AM or PM peak hours in the No-Build Alternative. In the 2045 No-Build Alternative, queuing on eastbound $N$ Weidler Street is approximately 450 feet east of the NW

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Lovejoy Street and NW Broadway intersection during the PM peak hour and queuing on westbound $N$ Broadway during the AM peak hour extends to the NE Martin Luther King Jr. Boulevard intersection. In the 2045 Revised Build Alternative, eastbound queuing on N Weidler Street in the PM peak hour is less than in the 2045 No-Build Alternative and westbound queuing on N Broadway is less during the AM peak hour but is approaching NE Martin Luther King Jr. Boulevard during the PM peak hour.

Bicycle delays and travel times were also evaluated for the 2045 No-Build and 2045 Revised Build Alternatives. Both alternatives serve a similar volume of bicycles in both the AM and PM peak hours but with considerably more delay in 2045 No-Build for key movements. In the AM peak hour, southbound bicycles on N Vancouver Avenue experience over 2 minutes of delay in the 2045 No-Build Alternative compared to approximately 25 seconds of delay in the 2045 Revised Build Alternative in both design options. In the PM peak hour, northbound bicycles on N Williams Avenue experience 90 seconds of delay crossing NE Weidler Street and 2 minutes of delay crossing $N$ Broadway, compared to approximately 30 seconds at both locations in the 2045 Revised Build Alternative for both design options.

Bicycle travel times for the 2045 Revised Build Alternative are consistently shorter in both design options compared to the 2045 No-Build Alternative. Westbound travel times in both AM and PM peak hours are slightly longer in the 2-way Wheeler Design Option compared to the 2-way Ramsay Design Option due to the additional signal phase at the N Broadway/ N Vancouver Avenue intersection, which results in less green time ${ }^{2}$ for westbound bicycle and vehicular traffic.

Transit travel times were evaluated for bus routes and streetcar routes. Bus travel times would be shorter in the northbound, southbound, and westbound routes during the AM peak period compared to the 2045 No-Build Alternative and would be longer in the eastbound routes by up to 20 to 30 seconds. During the PM peak period, Revised Build Alternative bus travel times would be similar to or shorter in the westbound, eastbound, and northbound directions and would be longer in the southbound direction compared to the 2045 No-Build Alternative. The 2-way Wheeler Design Option is approximately 30 seconds longer in the southbound direction compared to the 2-way Ramsay Design. During the PM peak period, southbound bus service travel times are approximately 20 seconds longer in the 2-way Ramsay Design Option and 50 seconds longer in the 2-way Wheeler Design Option compared to the $\mathbf{2 0 4 5}$ No-Build Alternative. Northbound travel times are similar in the 2-way Wheeler

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Design Option and are less than 20 seconds longer in the 2-way Ramsay Design Option compared to the 2045 No-Build Alternative. In both design options, travel times in the eastbound and westbound bus routes are up to 1 minute shorter compared to the 2045 No-Build Alternative.

Compared to the 2045 No-Build Alternative, there is an additional traffic signal at the N Williams Avenue and NE Hancock Street intersection that affects northbound routes in the 2045 Revised Build Alternative. The relocation of the l-5 southbound exit ramp to the N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way intersection also requires an additional signal phase that reduces the green time for northbound and southbound traffic, affecting the overall transit travel time in both design options. The southbound bus travel time experiences additional delay in the 2-way Wheeler Design Option due to the additional signal phase for the northbound left turn movement, which reduces the green time available for southbound $\mathbf{N}$ Vancouver Avenue. The 2-way Wheeler Design Option also removes the southbound bus only lane between N Broadway and NE Weidler Street, which would have buses traveling with general traffic.

Streetcar travel times for the westbound routes are expected to be shorter during both the AM and PM peak hours in the 2045 Revised Build Alternative, with improvements of $\mathbf{3 0}$ seconds to 1 minute compared to the 2045 No-Build Alternative. Eastbound Streetcar travel times are similar between design options and would generally be within 20 to 25 seconds of the 2045 No-Build travel times during the AM peak period and 1 to $\mathbf{2}$ minutes shorter during the PM peak period.

Refinements to signal timing and signal progression within the project area may shorten bus and Streetcar service travel times and will be further evaluated during design. The addition of transit signal priority, bus only lanes, bus queue jumps, and bus stop consolidation will also be evaluated during design.
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### 1.0 INTRODUCTION

The I-5 Rose Quarter Improvement Project (Project) Environmental Assessment (EA) was released in February 2019. The Federal Highway Administration (FHWA) published a Finding of No Significant Impact (FONSI) and Revised EA (REA) for the Build Alternative on November 6, 2020. Since the issuance of the FONSI, the Oregon Department of Transportation (ODOT) has made changes to the design of the proposed Build Alternative to create a Revised Build Alternative and re-evaluated the changes in the context of the FONSI/REA. At the conclusion of the re-evaluation, FHWA and ODOT agreed that the design changes require additional analyses beyond what was presented in the REA, and FHWA rescinded the FONSI on January 18, 2022. ODOT prepared a Transportation Safety Supplemental Technical Report, which was published with the I-5 Rose Quarter Improvement Project Supplemental Environmental Assessment (SEA) on November 15, 2022. In response to public comments received on the SEA, ODOT refined the design of the Revised Build Alternative. This Revised Transportation Safety Supplemental Technical Report reflects changes to the evaluation of the Transportation Safety impacts based on those design refinements, which are described below in Section 2.0. All updated information is shown in bold text.

### 2.0 BUILD ALTERNATIVE DESIGN CHANGES

Changes to the Build Alternative include modification to the highway cover design and changes associated with advancements in other elements of the project design, some of which require expansion of the Project Area. This section describes the highway cover design changes and design changes that resulted from advancements in project engineering and comments on the SEA. The evaluation of these changes is presented in Section 6.2 of this supplemental technical report.

### 2.1 DESIGN PROCESS

Through 2021, ODOT facilitated an Independent Highway Cover Assessment, as directed by the Oregon Transportation Commission, that engaged the Project's advisory committees and community members in a series of collaborative workshops to explore the design opportunities for the highway cover. The purpose of the Independent Highway Cover Assessment was to understand partner goals and objectives within the Project Area, generate potential highway cover scenarios, and assess the impacts and benefits of these scenarios. The Independent Highway Cover Assessment team worked directly with local community members from the historic Albina neighborhood to understand how the highway cover design concepts might best serve the historic Albina community. The Project's Historic Albina Advisory Board (HAAB),
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Executive Steering Committee (ESC) and the Community Oversight Advisory Board (COAC) also provided input as part of the Independent Highway Cover Assessment process. These sessions explored potential opportunities for economic development in the Albina community and the highway cover design concepts.

In July 2021, Oregon Governor Brown convened a series of meetings with Project partners and community organizations to discuss the design concepts developed in the Independent Highway Cover Assessment. In August 2021, the HAAB—as supported by the ESC and the COAC, and through the Governor-led process-recommended "Hybrid 3" as the preferred highway cover design concept (Figure 1). The Hybrid 3 highway cover design concept represents a proposed community solution to maximize developable space on a single highway cover. The Hybrid 3 highway cover design concept maintains the commitment for the Project to create opportunities for the local community to grow wealth through business ownership and longterm career prospects through the Project's Disadvantaged Business Enterprise and workforce program. Following the community and partner recommendations, in September 2021, the Oregon Transportation Commission directed ODOT to advance further evaluation of the Hybrid 3 highway cover design concept, with conditions related to the Project's funding process and other technical analyses.

In January 2022, Governor Brown entered into a Letter of Agreement with the City of Portland, Metro, and Multnomah County that demonstrated their shared understanding and collective support for the Hybrid 3 concept as part of the Project. The Letter of Agreement specifically highlights the desire to connect the Lower Albina neighborhood, create buildable space, and enhance wealth-generating opportunities for the community, while simultaneously addressing the area's transportation needs. Additionally, the Letter of Agreement supports the development of a process to define the future development vision for what could ultimately be built on top of the highway cover upon Project completion - this process is referred to as a Community Framework Agreement. The Letter of Agreement states that the City of Portland will lead a Community Framework Agreement process and that it should be between the City of Portland, ODOT, other state agencies and local jurisdictions as necessary, with the participation of organizations that represent the Albina community and Black residents. Any future real estate or open space development on top of the cover would require executing long-term air rights and lease agreements, and that any such actions or decisions are subject at all times to applicable local, state, and federal laws including but not limited to land use and NEPA processes.

In June 2022, ODOT and the City of Portland executed an Intergovernmental Agreement (IGA), building upon the January 2022 Letter of Agreement. The IGA further states that the City will lead the future highway cover land use, programming and development processes and development of a Community Framework Agreement, in consultation with the ODOT to ensure
the highway, local streets and resulting land parcels within the Project are coordinated. As such, ODOT would construct the highway cover as part of the Project and the City of Portland would lead the process to define what is ultimately built on the new land created by the Project's highway cover. In the IGA, both ODOT and the City agreed that ODOT will retain ownership of the highway cover structure and the new developable area created on the highway cover structure upon Project completion.

FHWA and ODOT released the I-5 Rose Quarter Improvement SEA on November 15, 2022. In response to comments on the SEA, ODOT refined the design of the Revised Build Alternative. The sections below describe the highway cover design changes and the design changes that resulted from advancements in project engineering and comments on the SEA and are incorporated into the Revised Build Alternative.

Figure 1 Hybrid 3 Highway Cover Design Concept with Ramp Reconfiguration


### 2.2 PROJECT AREA

The Project Area is defined as the area within which improvements are proposed, including where permanent modifications to adjacent parcels may occur and where potential temporary impacts from construction activities could result. As Project design information advanced, some changes required expansion of the Project Area presented in the REA and FONSI. In total, approximately 8.7 acres would be added to the Project Area. The changes are as follows, with letter references to the areas shown in Figure 2:

- A: Utility conflicts with Light Rail Transit (LRT) along NE Holladay Street between N Interstate Avenue and NE Martin Luther King Jr. Boulevard required expanding the Project Area by 1.9 acres to include additional overhead utility relocations (label A in Figure 2).
- B: An existing parking lot (known as Aegean Lot) south of $N$ Interstate Avenue and the Broadway Bridge may be used for contractor staging during construction and is added to the Project Area (label B, Figure 2). ODOT identified this 4.3-acre construction staging area for contractor use based on its location, size, and suitability recognizing that, because of the urban setting and high-density land development in the construction area, it would be difficult for a construction contractor to find the space needed near or next to the project work areas for equipment staging, material storage, and the required co-location space for the contractor/construction personnel. This location meets all of the Project requirements: large level open space, proximity to the project work areas, and access for staging/storage of materials and equipment. Any materials stored in the area and site runoff would be subject to the same regulations as required throughout the project site.
- C: The southern end of the Project Area is expanded by 2.4 acres to include the portion of $\mathrm{I}-5$ south of the Burnside Bridge proposed for a retrofit of the existing bridge rail, restriping the existing freeway, and installation of new guide signs (label C, Figure 2).
- D: At the northernmost end of the Project Area, a 1.1-acre area of ODOT right of way along the I-5 shoulders is now included in the Project Area for fiber optic conduit (label D, Figure 2).

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Figure 2 Previous and Current Project Area.


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Alternative
Additional Area


### 2.3 I-5 MAINLINE IMPROVEMENTS CHANGES

The Build Alternative included relocation of the I-5 southbound entrance ramp at N Wheeler Avenue to N/NE Weidler Street at N Williams Avenue via the new Weidler/Broadway/Ramsay highway cover, construction of auxiliary lanes and full shoulders ( 12 feet in width) on I-5 between I-405 and I-84 in both directions, and associated improvements to I-5 through the Project Area. The Revised Build Alternative includes the following changes to those elements of the Build Alternative:

- Move the I-5 southbound exit ramp termini from N Broadway to N Wheeler Avenue/ N Williams Avenue/N Ramsay Way (westbound) and NE Weidler Street (eastbound). The exit ramp would divide westbound traffic from eastbound traffic as seen in Figure 3, with a single lane connection at N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way and single lane bridge (flyover) over I-5 to connect with NE Weidler Street.
- Reduce the freeway median shoulder through the entire Project Area, from 12 feet to 8 feet ( 4 to 5 feet within highway cover). The outside shoulder width of 12 feet remains unchanged.
- Relocate Noise Wall 24 from N Commercial Avenue near Harriet Tubman Middle School to attach to Walls 1 and 2 along the east edge of I-5.
- Keep the l-5 southbound entrance ramp from $\mathbf{N}$ Wheeler Avenue/ N Williams Avenue/ N Ramsay Way on the existing alignment rather than relocate it to parallel N Williams Avenue.
- On I-5 south of the Burnside Bridge: retrofit existing bridge rail, restripe freeway in both the northbound and southbound directions, and install new guide signs on an existing sign structure in the southbound direction.
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Figure 3 I-5 SB Exit Ramp: Traffic Splitting Eastbound from Westbound Traffic


### 2.4 HIGHWAY COVER CHANGES

The Build Alternative included the construction of two highway cover structures over I-5 for roadway crossings and other purposes. The Revised Build Alternative, based on Hybrid 3 (see Figure 1), includes the following changes to the highway covers:

- Provide one continuous highway cover over I-5 rather than separate covers at the existing N Flint Avenue, NE Weidler Street, NE Broadway, N Williams Avenue, and the N Vancouver Avenue overcrossings.
- Expand the limits of the highway cover by approximately 35 feet to the west and approximately 400 feet to the north.
- Design and construct the highway cover to accommodate multi-story buildings. Due to span length and site constraints, design would constrain building size, location, type, and use on portions of the cover (Figure 4). Generally, buildings up to three stories could be accommodated throughout the highway cover. Buildings of up to six stories could be accommodated where span lengths are shorter than 80 feet with strict design constraints.

Figure 4 Building Parameters on the Cover



Future development on the highway cover would follow a community process according to the City-led Community Framework Agreement, as described in Section 2.1. ODOT anticipates this process could continue past completion of cover construction.

As part of the Project, ODOT anticipates programming interim uses on the highway cover for the time period between Project completion and when the City-led development process would be implemented. Upon Project completion, the added surface space created by the highway cover over l-5 could provide an opportunity for new and modern bicycle facilities, making the area more connected, walkable and bike friendly. It could also provide opportunity for various potential types of public spaces, to be precisely determined during the Project's final design phase and through robust community engagement, consisting of one or more of the following types of uses:

- Landscaped areas for accessible, active, and passive recreation and/or to provide a buffer, backdrop and visual comfort, such as gardens, lawns or planter beds.
- Accessible plazas and hardscaped open space for active and passive recreation, such as courts, plazas, splash pads, picnic areas, and community gathering spaces.
- Accessible interpretive signage, historical markers, landmarks and other areas of historical recognition and narrative such as art pieces and other historical signage/kiosks and pavement focused on the historic Albina community.
- Temporary and lightweight vertical features to support episodic, mobile commercial activities such as accessible food market shed, eating pavilion, food carts, or picnic venues.

These features may be removed upon implementation of the development determined by the community process or may be incorporated into that development.

### 2.5 RELATED LOCAL SYSTEM MULTIMODAL IMPROVEMENTS CHANGES

The Revised Build Alternative includes the following changes to local system multimodal improvements to accommodate the Hybrid 3 design concept and subsequent design refinements (see Figure 5 below):

- Construct the accessible Clackamas Bicycle and Pedestrian Crossing (a.k.a. Clackamas Crossing):
» Realign the crossing to the south to accommodate the flyover to NE Weidler Street
" Relocate the western termination point of the crossing to the triangle of land framed by N Center Court Street, NE Wheeler Avenue, and N Ramsay Way.
" Provide the following connections to the crossing (to be confirmed in the final design phase):

From the southeast corner of the intersection of $\mathbf{N}$ Williams Avenue and $\mathbf{N}$ Weidler Street that spans over N Wheeler Avenue and connects to the crossing, and
/ From the Garden Garage, which is attached to the Moda Center
" Construct wider sidewalks and bike lanes at sidewalk level and physically separated from the roadway with a curb and provide protected bike signal phases at multiple intersections along NE Broadway and NE Weidler Street.

- Connect N Flint Avenue across I-5 from NE Tillamook Street to N Hancock Street and terminate it at N Broadway.
- Remove the NE Hancock Street overcrossing of I-5 from N Williams Avenue to N Dixon Street as proposed in the Build Alternative. NE Hancock Street would be extended across I-5 and reconnect to NE Hancock Street west of N Flint Avenue as part of the expanded highway cover. Permitted traffic modes and roadway profile to be determined during design.
- Remove the two-way cycle track on N Williams Avenue between NE Hancock Street and NE Broadway and a two-way bicycle and pedestrian path between NE Broadway and N Ramsay Way from the design and instead convert the on-road bike lane to a protected bike lane, with a transition to the existing on-road bike lane at or near NE Hancock Street (to be confirmed in the final design phase).

Figure 5 Major Local System Multimodal Design Changes


| Beaverton | $\qquad$ Project Design $\square$ Project Area $\qquad$ Clackamas Crossing | I-5 ROSE QUARTER IMPROVEMENT PROJECT MAJOR LOCAL SYSTEM MULTIMODAL DESIGN CHANGES Dregon of Transportation |
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To accommodate I-5 southbound traffic exiting at $\mathbf{N}$ Wheeler Avenue/ $\mathbf{N}$ Williams Avenue/ N Ramsay Way, ODOT is considering two design options, both of which are evaluated in this report (Figure 6):

- 2-way Ramsay Design Option - Convert N Ramsay Way between N Center Court Street and NE Wheeler Avenue from an eastbound one-way facility to a two-way facility.
- 2-way Wheeler Design Option - Construct a new northbound travel lane on NE Wheeler Avenue between N Broadway and N Ramsay Way and maintain the three existing southbound travel lanes between $\mathbf{N}$ Weidler Street and N Ramsay Way.

Both design options also include a left turn movement from the l-5 southbound exit ramp to southbound $\mathbf{N}$ Williams Avenue. This movement was previously accommodated via N Wheeler Avenue/ N Vancouver Avenue between N Broadway and N Ramsay Way.

Figure 6 Design Options for I-5 SB Exit Ramp: Traffic Heading West


### 3.0 REGULATORY FRAMEWORK

The regulatory framework is the same as was evaluated in the 2019 Traffic Analysis Technical Report.

### 4.0 METHODOLOGY AND DATA SOURCES

The methodology and data sources are the same as those described in the 2019 Traffic Analysis Technical Report with the exception of the methodology used to develop future bicycle volumes and the methodology used to calculate $95^{\text {th }}$ percentile queue length.

Bicycle volumes were updated based on additional existing bicycle counts provided by City of Portland and an anticipated increase in bicycle mode share target within Central City described in the City of Portland's Central City 2035 Comprehensive Plan.

The methodology for calculating the $95^{\text {th }}$ percentile queue length has been updated for improved accuracy. Vissim queue counters were used to record the maximum queue length for each signal cycle length interval. The $95^{\text {th }}$ percentile queue length was calculated for each of the 10 simulation runs based on these "cycle length maximum queues". The resulting values were then averaged. $95^{\text {th }}$ percentile queue length is reported for the I-5 southbound and I-5 northbound exit ramps, the eastbound approach of N Weidler at N Larrabee Avenue, and the westbound approach of NE Broadway at NE Victoria Avenue.

To provide comparable results in this Revised Traffic Analysis Supplemental Technical Report, these changes in methodology were applied to both the 2045 No-Build Alternative and 2045 Revised Build Alternative models. Also, both the 2045 No-Build Alternative and 2045 Revised Build Alternative models have been refined to provide a more comprehensive local street and bicycle network. To better understand the potential impacts in the local street network and address specific design elements of the Revised Build Alternative, the following modifications have been made:

- Add the N Wheeler Avenue connection north of N Broadway
- Connect N Ramsay Way between N Larrabee Avenue and N Wheeler Avenue
- Add the U-turn movement from N Broadway and N Weidler Street
- Connect the local bicycle network

Also, bicycle and pedestrian crossing have been updated to reflect more detailed assumptions that were refined as the design has progressed at each intersection. Detailed bicycle and
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pedestrian crossing assumptions are presented in section 6.2. The local street analysis includes evaluations for two design options: 2-way Ramsay Design Option and 2-way Wheeler Design Option. Therefore, both 2045 No-Build Alternative and 2045 Revised Build Alternative analysis results in this Revised Traffic Analysis Supplemental Technical Report provide a more refined comparison of traffic operational performance between the 2045 No-Build Alternative and the 2045 Revised Build Alternative than was presented for the 2045 No-Build Alternative and the 2045 Build Alternative in the 2019 Traffic Analysis Technical Report. Due to the updated 2045 No-Build Alternative model, the 2045 No-Build Alternative traffic analysis results may differ from those documented in the 2019 Traffic Analysis Technical Report.

### 4.1 AREA OF POTENTIAL IMPACT

The API for the traffic analysis generally corresponds to the Project Area shown in Figure 2, except along N Broadway, where the API extends west to N Larrabee Avenue. This extension is the same as shown in the Area of Potential Impact in the 2019 Traffic Analysis Technical Report.

### 4.2 FUTURE TRAFFIC VOLUMES

As described in the 2019 Traffic Analysis Technical Report, the Metro Regional Travel Demand Models, which have a detailed system of the City of Portland roadway network, were used to forecast future demand for the horizon year 2045. Metro maintains travel demand models for the base (year 2015) and future conditions (year 2040). The 2040 travel demand model integrates planned transportation projects and land use changes in the metro area to generate future volume forecasts. The 2040 travel demand model used for the 2019 Traffic Analysis Technical Report incorporated transportation projects identified in the financially constrained list in the 2014 Regional Transportation Plan (RTP). For this analysis, the 2040 travel demand model was reviewed to determine if it is consistent with the current 2018 RTP. As documented in the List of Reasonably Foreseeable Future Actions Report (Appendix A), there were no new projects in the 2018 RTP that would influence the future traffic demand in the I-5 corridor and its surrounding roadway network when compared to the 2014 RTP; therefore, the travel demand models used in the development of future traffic volumes incorporated into the 2019 Traffic Analysis Technical Report are still valid to be used for this analysis.

ODOT is in the initial planning stages for the Regional Mobility Pricing Project (RMPP), which evaluates congestion pricing on I-5 through and beyond the Rose Quarter project area. RMPP is not included in the financially constrained projected list included in the 2018 Regional Transportation Plan (RTP) and is therefore not included in Metro's regional travel demand model which was used for volume development for the I-5 Rose Quarter Improvement Project. The traffic analysis results of this report do not include the Regional Mobility Pricing Project. However, the RMPP project team has completed separately a sensitivity analysis to look at the
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cumulative impacts of RMPP and the I-5 Rose Quarter Improvement Project. The results of this analysis are summarized in Appendix B and included in this report for information only.

To develop the 2045 forecast volumes for the No-Build and Revised Build Alternatives, the volume growth from the 2015 base year and the 2040 future year was used to calculate an annual growth rate using a straight-line growth method. This growth rate was applied to the 5-year increment between 2040 and 2045 to extend the demand model for the Project's horizon year. The 2045 Revised Build Alternative model was developed by:

1. Updating the 2045 No-Build Alternative model with the widened I-5 freeway segment between the I-84 and I-405 interchanges
2. Incorporating the newly proposed roadway network adjustments (i.e., relocation of I-5 southbound ramp terminal to N Wheeler Avenue, extension of NE Hancock Street to N Flint Avenue, maintain N Flint Avenue in its current location) and updating intersection lane configurations

Comparing 2045 No-Build Alternative and 2045 Revised Build Alternative travel demand models, ODOT investigated trip changes within and outside of the Project Area to identify trip pattern changes between the No-Build and Revised Build Alternatives for 2045. Within the Project Area, the travel demand model shows trips on l-5 would be 5 to 14 percent higher under the Revised Build Alternative during peak hours when compared to the No-Build Alternative. Outside of the Project Area, trip differences were evaluated at several central city bridges. Trip differences between 2045 No-Build and 2045 Revised Build Alternative are inconsequential beyond the API limits with no substantive traffic volume changes beyond the Traffic Analysis API anticipated. The 2045 No Build and 2045 Revised Build AM and PM peak hour volume are provided in Appendix C.

Appendix D also provides an evaluation of the proposed auxiliary lanes based on 2023 APM methodology which concluded that adding auxiliary lanes to freeway segments on I-5 northbound section from the I-84 entrance ramp to the $\mathbf{N}$ Greeley Avenue exit ramp and on the I-5 southbound section from the N Greeley Avenue entrance ramp to the Morrison Bridge exit ramp would not result in system capacity increase.

### 4.3 ASSESSMENT OF IMPACTS

### 4.3.1 Traffic Operations Performance Measures, Mobility Target, and Standards

The traffic operations performance measures ( $\mathrm{v} / \mathrm{c}$, LOS, delay, $95^{\text {th }}$ percentile queue and travel times), Oregon Highway Plan (OHP) mobility target, HDM mobility standards, and the City of Portland LOS Standards for local intersections are the same as those described in the 2019 Traffic Analysis Technical Report. The mobility target and standards have not changed since 2019.

### 4.3.2 Traffic Operations Software

The traffic operations software is the same as those described in the 2019 Traffic Analysis Technical Report.

Highway Capacity Software (HCS) was used to evaluate basic freeway segments, merge, diverge, and weaving operations. HCS is a deterministic analysis tool for freeway operations by implementing the Highway Capacity Manual (HCM) methodologies for basic weaving, merging, and diverging freeway segments. For the 2019 Traffic Analysis Technical Report, a traffic microsimulation software called Vissim was used to supplement the freeway analysis. Comparing the 2045 Revised Build Alternative to the Build Alternative, the locations of the merge and diverge ramp junctions and the lengths of weaving segments between entrance ramps and exit ramps are relatively the same as well as the peak hour volumes along the mainline segments and the on-and exit ramps. As a result, the prior Vissim freeway mainline analysis methodologies and results presented in the 2019 Traffic Analysis Technical Report including lane-by-lane speed were determined to still be valid. Thus, Vissim modeling of the freeway operations for the 2045 Revised Build Alternative was not updated as part of this Revised Traffic Analysis Supplemental Technical Report.

Vissim modeling, however, was updated to analyze local street traffic operations including ramp terminal intersections and reporting delays; $95^{\text {th }}$ percentile queues; and bus, streetcar, and bicycle travel times. Vissim can model and quantify performance of individual pedestrians, bicycles, automobiles, trucks, buses, and streetcars and provide performance measure results that account for modal interactions, up and/or downstream congestion, and capacity limitations that can result from queues extending beyond the storage provided at each intersection. Therefore, Vissim quantifies overall intersection delays more realistically than typical equation based HCM methods such as Synchro. In addition, the intersection LOS is computed from a microsimulation analysis, which is not HCM compliant. As a result, the intersection LOS is reported as an "estimated LOS".
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Synchro software was used to supplement Vissim modeling to report the intersection v/c ratio, delay and LOS as measurements of performance. Synchro is a deterministic analysis and signal optimization tool that uses the general characteristics of an intersection to evaluate how it would operate based on the HCM methodologies. Ramp terminal intersection v/c ratios are used to compare to the OHP traffic mobility targets for the 2045 No-Build Alternative and to compare to the Highway Design Manual (HDM) design standards for the 2045 Revised Build Alternative. The intersections not associated with the highway ramp terminals are subject to City of Portland standards of LOS D for signalized intersections and LOS E for unsignalized intersections (City of Portland n.d.). As part of the adoption of the Central City 2035 Plan, the Central City, which includes the 13 intersections analyzed in this report, has been designated as a Multimodal Mixed-Use Area (MMA). This designation provides flexibility for determining effects of land use actions by lifting mobility standards requirements at ODOT facilities. Transportation standards such as safety and multimodal access still apply.

### 5.0 AFFECTED ENVIRONMENT

The affected environment is the same as that evaluated in the 2019 Traffic Analysis Technical Report.

### 6.0 ENVIRONMENTAL CONSEQUENCES

### 6.1 NO-BUILD ALTERNATIVE

6.1.1 Direct Impacts

The No-Build Alternative would have the same direct impacts in all freeway segments as described in the 2019 Traffic Analysis Technical Report. The 2045 No-Build Alternative freeway operations are summarized in Table 5 and Table 6 in Section 6.2.2.1 and show that the I-5 northbound weave segment between the I--84 entrance ramp and the NE Weidler Street exit ramp would exceed the OHP mobility target of a v/c ratio of 0.99 in the second AM and PM peak hours (7:00-8:00 AM and 4:00-5:00 PM) and also would exceed the OHP mobility target of a v/c ratio of 1.1 in the first AM peak hour (8:00-9:00 AM). The I-5 southbound weave between the NE Weidler Street entrance ramp and the I-84 exit ramp would exceed the OHP mobility target of a $\mathrm{v} / \mathrm{c}$ ratio of 0.99 in the second AM peak hour (7:00-8:00 AM). Minimum stopping sight distance is provided within these weaving sections in both the northbound and southbound directions.

As described under section 4.0, the local street analysis for the 2045 No-Build Alternative has been updated with revised bicycle volumes and a more refined bicycle and local street network. Therefore, the local street 2045 No-Build Alternative analysis results differ from those
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presented in the 2019 Traffic Analysis Technical Report. Table 1 and Table 2 show the updated 2045 No-Build Alternative Synchro analysis results and Table 3 and Table 4 present the updated 2045 No-Build Vissim analysis results.

Synchro analysis results show that all intersections will operate at a LOS D or better in both the AM and PM peak hours with the exception of the N Broadway/ N Vancouver Avenue/ I-5 southbound exit ramp intersection which would operate at LOS F in the AM peak hour. The $\mathrm{v} / \mathrm{c}$ ratio at this intersection exceeds the OHP mobility target of 0.85 for ramp terminal intersections for both the AM and PM peak hours. The NE Weidler Street/ NE Victoria Avenue/ I-5 northbound exit ramp intersection will operate at LOS E in the AM peak hour. Detailed HCM reports from Synchro are provided in Appendix E.

Table 1 Synchro Analysis Results: 2045 No-Build Alternative 8:00 AM - 9:00 AM
$\left.\begin{array}{lllcc}\hline \text { ID } & \text { Intersection } & \text { v/c } & \text { Delay (sec) } & \text { LOS } \\ \hline 1 & \text { N Broadway \& N Vancouver Ave } \\ \text { (existing l-5 SB exit ramp) }\end{array}\right)$

Note: Red $=v / c$ exceeds OHP mobility target for ramp terminals or LOS below D for signalized local intersections.

Table 2 Synchro Analysis Results: 2045 No-Build Alternative 5:00 PM - 6:00 PM

| ID | Intersection | v/c | Delay (sec) | LOS |
| :---: | :---: | :---: | :---: | :---: |
| 1 | N Broadway \& N Vancouver Ave (existing l-5 SB exit ramp) | 0.92 | 44.2 | D |
| 2 | N/NE Broadway \& N Williams Ave | 0.57 | 13.5 | B |
| 3 | NE Broadway \& NE Victoria Ave | 0.53 | 9.1 | A |
| 4 | NE Broadway \& NE $2^{\text {nd }}$ Ave | 0.40 | 10.0 | A |
| 5 | NE Weidler St \& NE $2^{\text {nd }}$ Ave | 0.41 | 11.7 | B |
| 6 | I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | 0.60 | 19.7 | B |
| 7 | N/NE Weidler St \& N Williams Ave | 0.46 | 4.3 | A |
| 8 | N Weidler St \& N Vancouver Ave | 0.63 | 13.3 | B |
| 9 | N Broadway \& N Benton Ave | 0.50 | 20.6 | C |
| 10 | $N$ Broadway \& N Larrabee Ave | 0.66 | 19.4 | B |
| 11 | N Wheeler Ave/ N Williams Ave/ N Ramsay Way \& I-5 SB Ramps | 0.40 | 12.2 | B |
| 12 | N Williams Ave \& N/NE Hancock St | 0.21 | 14.8 | B |
| 13 | N Vancouver Ave \& NE Hancock St | - | - | - |
| 14 | N Williams Ave \& N/NE Multnomah St | 0.36 | 11.0 | B |

Note: Red $=v / c$ exceeds OHP mobility target for ramp terminals or LOS below D for signalized local intersections.
As shown below, the Vissim analysis results indicate that all intersections would operate at a LOS D or better in the AM peak hour except for the NE Weidler Street/ NE Victoria Avenue/ I-5 northbound exit ramp intersection, which would operate at LOS E. During the PM peak hour, all intersections are expected to operate at a LOS D or better except for the I-5 southbound and I-5 northbound exit ramp intersections, which would operate at LOS F and LOS E, respectively.

Vissim can model and quantify performance of individual pedestrians, bicycles, automobiles, trucks, buses, and streetcars and provide performance measure results that account for modal interactions, up and/or downstream congestion, and capacity limitations that can result from queues extending beyond the storage provided at each intersection. Therefore, Vissim quantifies overall intersection delays more realistically than typical deterministic equation based HCM methods such as Synchro. Detailed Vissim intersection results for the first and second AM and PM peak hours for all movements are provided in Appendix F.
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Table 3 Vissim Analysis Results: 2045 No-Build Alternative 8:00 AM - 9:00 AM

| ID | Intersection | Delay (sec) | LOS* |
| :---: | :---: | :---: | :---: |
| 1 | N Broadway \& N Vancouver Ave (existing l-5 SB exit ramp) | 43.8 | D |
| 2 | N/NE Broadway \& N Williams Ave | 16.3 | B |
| 3 | NE Broadway \& NE Victoria Ave | 38.9 | D |
| 4 | NE Broadway \& NE $2^{\text {nd }}$ Ave | 27.7 | C |
| 5 | NE Weidler St \& NE $2^{\text {nd }}$ Ave | 7.1 | A |
| 6 | I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | 66.1 | E |
| 7 | N/NE Weidler St \& $N$ Williams Ave | 3.6 | A |
| 8 | $N$ Weidler St \& N Vancouver Ave | 12.9 | B |
| 9 | $N$ Broadway \& N Benton Ave | 14.2 | B |
| 10 | $N$ Broadway \& N Larrabee Ave | 12.1 | B |
| 11 | N Wheeler Ave/ N Williams Ave/ N Ramsay Way \& I-5 SB Ramps | 37.2 | D |
| 12 | N Williams Ave \& N/NE Hancock St | 11.2 | B |
| 13 | N Vancouver Ave \& NE Hancock St | N/A | N/A |
| 14 | N Williams Ave \& N/NE Multnomah St | 10.4 | B |

Note: *LOS is non HCM compliant
Table 4 Vissim Analysis Results: 2045 No-Build Alternative 5:00 PM - 6:00 PM

| ID | Intersection | Delay (sec) | LOS* |
| :--- | :--- | :---: | :---: |
| 1 | N Broadway \& N Vancouver Ave <br> (existing l-5 SB exit ramp) | 87.6 | F |
| 2 | N/NE Broadway \& N Williams Ave | 15.4 | B |
| 3 | NE Broadway \& NE Victoria Ave | 28.1 | C |
| 4 | NE Broadway \& NE 2 ${ }^{\text {nd }}$ Ave | 11.4 | B |
| 5 | NE Weidler St \& NE 2 ${ }^{\text {nd }}$ Ave | 9.2 | A |
| 6 | I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | 75.4 | E |
| 7 | N/NE Weidler St \& N Williams Ave | 17.8 | B |
| 8 | N Weidler St \& N Vancouver Ave | 28.1 | C |
| 9 | N Broadway \& N Benton Ave | 17.9 | B |
| 10 | N Broadway \& N Larrabee Ave | 43.4 | D |
| 11 | N Wheeler Ave/ N Williams Ave/ | 28.5 | C |
| 12 | N Ramsay Way \& I-5 SB Ramps | 10.9 | B |
| 13 | N Vancouver Ave \& NE Hancock St | N/A | N/A |
| 14 | N Williams Ave \& N/NE Multnomah St | 11.5 | B |

Note: Red $=$ LOS below $D$ for signalized local intersections. *LOS is non HCM compliant

### 6.1.2 Indirect Impacts

The No-Build Alternative would have the same indirect impacts as described in the 2019 Traffic Analysis Technical Report.

### 6.2 REVISED BUILD ALTERNATIVE <br> 6.2.1 Short-term Construction Impacts

The short-term impacts of the Revised Build Alternative would be similar to those described in the 2019 Traffic Analysis Technical Report with two exceptions, the overall construction and transportation disruptions occurring in phases for up to 4-8 years, which is greater than the previous assumption of up to 4 years and the closure of $N$ Williams Avenue. This increase in duration is based on the construction of a larger single continuous highway cover, which would require additional construction stages and phases. N Williams Avenue between N Wheeler Avenue and NE Weidler Street would be closed for the majority of the highway cover construction. The complete closure of N Williams Avenue during construction of the new highway cover and the relocation the southbound exit ramp on $N$ Williams Avenue would have a greater impact on transit, cyclists, pedestrians, and vehicles traveling on this section of N Williams Avenue. Construction impacts on N Russell Street, NE Multnomah Street, and NE Lloyd Boulevard are the same as those described in the 2019 Traffic Analysis Technical Report.

For each construction phase, the project would develop a traffic management plan to identify lane and road closures and develop detour plans, as necessary. Also, for each phase of the project, maintenance of traffic strategies would be developed to ensure safe accommodation of pedestrians, cyclists, transit, and vehicle users while providing a safe construction work zone. Detours plans are anticipated for pedestrians, bicycles, vehicles, and buses as ramp and local streets closures would be needed in order to construct highway ramp improvements, the highway cover structure, and reconstruct sections of local roads. The Project would coordinate with TriMet, City of Portland, and Portland Streetcar to identify traffic management strategies that minimize durations of disruptions of transit service and minimize out-of-direction pedestrian and bicycle detours.

As described above in the Project Area Changes section, an existing parking lot south of N Interstate Avenue and the Broadway Bridge may be used for contractor staging during construction of the Project. The parking lot will be used primarily for storage of staging equipment and materials for multiple construction activities including those required during night operations. This yard would also serve as the main location to store materials that are procured early, such as drilled shaft permanent casings, pipe piles, and sign bridges. Furthermore, this yard could provide needed space for fabrication of concrete form work,
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welding of miscellaneous materials for the job, equipment maintenance and repair. The lot would also be used to house temporary job site trailers and used for contractor parking for multiple staff and subcontractors.

Access to the contractor staging site would be through existing truck routes including Interstate Avenue, N Broadway and N Weidler Street which could provide adequate access to the entire project site including connections to l-5 ramps. The temporary truck trips are consistent with the type of commercial and industrial uses that currently operate within the area and the volume of trips that would be generated by the construction activities will be fairly consistent with the prior uses of the site. The site has been used for similar construction and staging operations and is assumed to be used as part of the construction operations for the duration of the project.

### 6.2.2 Direct Impacts

### 6.2.2.1 Future Freeway Traffic Operations

This section describes 2045 Revised Build Alternative freeway traffic operations based on the HCS analysis results for the two AM peak hours (7:00-9:00 AM) and PM peak hours (4:00-6:00 PM). The inside shoulder width is reduced in the Revised Build Alternative in segments on I-5 between I-84 and I-405 when compared to the Build Alternative with the median lateral clearance varying from 4 feet to 8 feet. Freeway capacity calculations were performed using HCM methodologies. According to the "HCM $6^{\text {th }}$ Edition: A Guide for Multimodal Mobility Analysis", median clearances of $\mathbf{2}$ feet or more on the left side of the travel lanes generally have little impact on traffic. Therefore, no capacity adjustments to reflect the reduced leftside lateral clearance from the left travel lane edge are available in the analysis. As a result, the freeway mainline capacity was assumed to be the same with the proposed median shoulder width reduction accounted for under the Revised Build Alternative.

In the 2045 Revised Build Alternative, the I-5 northbound weave segment between the I-84 entrance ramp and Weidler exit ramp and the I-5 southbound weave segment between the Weidler entrance ramp and I-84 exit ramp are expected to operate over the HDM design standard of a v/c ratio of 0.75 in the 7:00-9:00 AM and 4:00-6:00 PM peak hours. The HDM design standard is more stringent than the 2045 No-Build Alternative mobility target of a v/c ratio of 0.99 in the second AM and PM peak hours and a v/c ratio of 1.1 in the AM and PM peak hours because it is designated for design purposes. Although the 2045 Revised Build Alternative $\mathrm{v} / \mathrm{c}$ ratios exceed HDM design standards, it is expected to substantially improve highway operations compared to the 2045 No-Build Alternative. The HCS analysis results comparing the 2045 No-Build and Revised Build Alternatives in the second AM and PM peak hours (7-8 AM and 4-5 PM) and in the first AM and PM peak hours (8-9 AM and 5-6 PM) are presented in Table 5
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and Table 6, respectively. The v/c ratios that exceed OHP mobility targets in the 2045 No-Build Alternative and HDM mobility standards in the 2045 Revised Build Alternative are highlighted.

Table 5 HCS Analysis Results: 2045 No-Build Alternative and 2045 Revised Build Alternative Second (7:00-8:00) AM and (4:00-5:00) PM Peak Hour

| Direction | Location | Analysis Type | 2045 No-Build Alternative |  |  | 2045 Revised Build Alternative |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | v/c | Volume Density (pc/mi/ln) | LOS | v/c | Volume Density (pc/mi/ln) | LOS |
| I-5 NB | I-84 entrance ramp to <br> Weidler exit ramp | Weaving | $\begin{gathered} 1.16 \\ (1.02) \end{gathered}$ | (*) | F <br> (F) | $\begin{gathered} 0.89 \\ (0.78) \end{gathered}$ | $\begin{gathered} 41.1 \\ (34.2) \end{gathered}$ | E <br> (D) |
|  | Weidler exit ramp to Broadway entrance ramp | Basic Section | $\begin{gathered} 0.91 \\ (0.79) \end{gathered}$ | $\begin{gathered} 42.5 \\ (36.6) \end{gathered}$ | E <br> (E) | $\begin{gathered} 0.72 \\ (0.64) \end{gathered}$ | $\begin{gathered} 33.5 \\ (29.6) \end{gathered}$ | D <br> (D) |
|  | Broadway entrance ramp to l-405 exit ramp | Weaving | $\begin{gathered} 0.92 \\ (0.78) \end{gathered}$ | $\begin{gathered} 36.9 \\ (31.6) \end{gathered}$ | E <br> (D) | $\begin{gathered} 0.72 \\ (0.63) \end{gathered}$ | $\begin{gathered} 30.6 \\ (26.9) \end{gathered}$ | D <br> (C) |
|  | Greeley <br> Exit ramp | Diverge | $\begin{gathered} 0.75 \\ (0.72) \end{gathered}$ | $\begin{gathered} 32.4 \\ (30.6) \end{gathered}$ | D <br> (D) | $\begin{gathered} 0.53 \\ (0.50) \end{gathered}$ | $\begin{gathered} 21.8 \\ (20.7) \end{gathered}$ | C <br> (C) |
| I-5 SB | I-84 entrance ramp to <br> Weidler exit ramp | Weaving | $\begin{gathered} 0.73 \\ (0.64) \end{gathered}$ | $\begin{gathered} 32.1 \\ (25.5) \end{gathered}$ | D <br> (C) | $\begin{gathered} 0.70 \\ (0.62) \end{gathered}$ | $\begin{gathered} 34.5 \\ (28.7) \end{gathered}$ | D <br> (D) |
|  | Weidler exit ramp to Broadway entrance ramp | Basic Section | $\begin{gathered} 0.94 \\ (0.70) \end{gathered}$ | $\begin{gathered} 44.1 \\ (32.8) \end{gathered}$ | E <br> (D) | $\begin{gathered} 0.70 \\ (0.56) \end{gathered}$ | $\begin{gathered} 33.0 \\ (26.3) \end{gathered}$ | D <br> (D) |
|  | Broadway entrance ramp to l-405 exit ramp | Weaving | $\frac{1.03}{(0.81)}$ | (34.7) | F <br> (D) | $\begin{gathered} 0.95 \\ (0.79) \end{gathered}$ | $\begin{gathered} 42.3 \\ (30.9) \end{gathered}$ | E <br> (D) |
|  | Greeley <br> Exit ramp | Diverge | $\begin{gathered} 0.81 \\ (0.61) \end{gathered}$ | $\begin{gathered} 33.3 \\ (24.9) \end{gathered}$ | D <br> (C) | $\begin{gathered} 0.58 \\ (0.46) \end{gathered}$ | $\begin{gathered} 23.7 \\ (18.8) \end{gathered}$ | C <br> (C) |

Notes: HCS = Highway Capacity Software; HDM = Highway Design Manual; LOS = Level of Service;
OHP= Oregon Highway Plan; pc/mi/In = passenger car per mile per lane; v/c=volume-to-capacity ratio LOS is based on the calculated volume density and not based on v/c ratio shown.
Orange $=v / c$ ratio exceeds OHP mobility target of 0.99 for the 2045 No-Build second peak hour.
Red $=v / c$ ratio exceeds HDM mobility target of 0.75 for the Revised Build peak hour.

* = Volume density not reported (demand exceeds capacity).

Table 6 HCS Analysis Results: 2045 No-Build and Revised Build Alternative First (8:00-9:00) AM and (5:00-6:00) PM Peak Hour

| Direction | Location | Analysis Type | 2045 No-Build Alternative |  |  | 2045 Revised Build Alternative |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | v/c | Volume Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) | LOS | v/c | Volume <br> Density (pc/mi/ln) | LOS |
| I-5 NB | I-84 entrance ramp to Weidler exit ramp | Weaving | $\frac{1.16}{(1.02)}$ | (*) | F <br> (F) | $\begin{gathered} 0.89 \\ (0.81) \end{gathered}$ | $\begin{gathered} 41.1 \\ (36.1) \end{gathered}$ | E <br> (E) |
|  | Weidler exit ramp to Broadway entrance ramp | Basic Section | $\begin{gathered} 0.91 \\ (0.82) \end{gathered}$ | $\begin{gathered} 42.5 \\ (38.1) \end{gathered}$ | E <br> (E) | $\begin{gathered} 0.72 \\ (0.66) \end{gathered}$ | $\begin{gathered} 33.5 \\ (30.8) \end{gathered}$ | D <br> (D) |
|  | Broadway entrance ramp to l-405 exit ramp | Weaving | $\begin{gathered} 0.92 \\ (0.82) \end{gathered}$ | $\begin{gathered} 36.9 \\ (33.3) \end{gathered}$ | E <br> (D) | $\begin{gathered} 0.72 \\ (0.66) \end{gathered}$ | $\begin{gathered} 30.6 \\ (28.2) \end{gathered}$ | D <br> (D) |
|  | Greeley exit ramp | Diverge | $\begin{gathered} 0.75 \\ (0.75) \end{gathered}$ | $\begin{gathered} 32.4 \\ (31.9) \end{gathered}$ | D <br> (D) | $\begin{gathered} 0.53 \\ (0.53) \end{gathered}$ | $\begin{gathered} 21.8 \\ (21.5) \end{gathered}$ | C <br> (C) |
| I-5 SB | I-84 entrance ramp to Weidler exit ramp | Weaving | $\begin{gathered} 0.73 \\ (0.67) \end{gathered}$ | $\begin{gathered} 32.1 \\ (26.8) \end{gathered}$ | D <br> (C) | $\begin{gathered} 0.70 \\ (0.65) \end{gathered}$ | $\begin{gathered} 34.5 \\ (30.4) \end{gathered}$ | (D) |
|  | Weidler exit ramp to Broadway entrance ramp | Basic Section | $\begin{gathered} 0.94 \\ (0.73) \end{gathered}$ | $\begin{gathered} 44.1 \\ (34.1) \end{gathered}$ | $\mathrm{E}$ <br> (D) | $\begin{gathered} 0.70 \\ (0.59) \end{gathered}$ | $\begin{gathered} 33.0 \\ (27.5) \end{gathered}$ | D <br> (D) |
|  | Broadway entrance ramp to l-405 exit ramp | Weaving | $\begin{gathered} 1.03 \\ (0.84) \end{gathered}$ | (36.7) | F <br> (E) | $\begin{gathered} 0.95 \\ (0.82) \end{gathered}$ | $\begin{gathered} 42.3 \\ (32.9) \end{gathered}$ | E <br> (D) |
|  | Greeley exit ramp | Diverge | $\begin{gathered} 0.81 \\ (0.64) \end{gathered}$ | $\begin{gathered} 33.3 \\ (26.0) \end{gathered}$ | D <br> (C) | $\begin{gathered} 0.58 \\ (0.48) \end{gathered}$ | $\begin{gathered} 23.7 \\ (19.7) \end{gathered}$ | C <br> (C) |

Notes: HCS = Highway Capacity Software; HDM = Highway Design Manual; LOS = Level of Service; OHP
= Oregon Highway Plan; pc/mi/ln = passenger car per mile per lane; v/c = volume-to-capacity ratio LOS is based on the calculated volume density and not based on v/c ratio shown.
Orange $=v / c$ ratio exceeds OHP mobility target of 1.1 for the 2045 No-Build peak hour.
Red $=v / c$ ratio exceeds HDM mobility target of 0.75 for the Revised Build peak hour.

* = Volume density not reported (demand exceeds capacity).

Comparing to the Build Alternative, the freeway operations improvements in the 2045 Revised Build Alternative are similar as the locations of the merge and diverge ramp junctions and the lengths of weaving segments between entrance ramps and exit ramps are relatively the same and the peak hour volumes along the mainline segments and the on-and exit ramps are similar.

### 6.2.2.2 Future Local Street Traffic Operations

This section describes the 2045 No-Build Alternative and 2045 Revised Build Alternative traffic operations for the local street intersections using Synchro and Vissim. Comparison to the Build Alternative is not provided as only the 2045 No-Build and Revised Build models have been
refined with updates in the bicycle volume forecast, detailed bicycle and pedestrian crossing assumptions and more refined local street network.

Synchro is a deterministic analysis and signal optimization tool that was used to obtain intersection v/c ratio and LOS results to compare to ODOT HDM mobility standards due to the limitations of providing $\mathrm{v} / \mathrm{c}$ ratios from microsimulation. Vissim was used to model the operations of motor vehicles, transit, pedestrians, ${ }^{3}$ and bicycles and evaluate demand served, delay, travel time, and queuing. Vissim quantifies overall intersection delays more realistically than typical equation based HCM methods such as Synchro by accounting for modal interactions, up and/or downstream congestion, and capacity limitations that can result from queues extending beyond the storage provided at each intersection.

Compared to the 2045 No-Build Alternative, the 2045 Revised Build Alternative would include higher traffic volume demand as well as bicycle and pedestrian improvements that would include protected bicycle and ped phases at locations with exclusive turning lanes and Leading Pedestrian Intervals (LPIs) at selected locations with permissive pedestrian phases. Also, the local street network in the 2045 Revised Build Alternative would accommodate physically separated and raised bicycle facilities along N/NE Broadway and N/NE Weidler Street, as well as along $N$ Williams Avenue.

The analysis of the 2045 Revised Build Alternative for both the 2-way Ramsay Design Option and the 2-way Wheeler Design Option is based on the following key bicycle/pedestrian crossing assumptions at locations with conflicting bicycle/pedestrian and vehicular turning movements:

- Protected bicycle crossings
» EB/WB at N Broadway and N Larrabee Avenue (included in 2045 No-Build)
» EB at $N$ Weidler Street and $N$ Vancouver Avenue
» WB at N/NE Broadway and N Williams Avenue (included in 2045 No-Build)
" NB at N Williams Avenue and N/NE Hancock Street
» SB at $N$ Broadway and $N$ Vancouver Avenue
- Protected pedestrian crossings
» N Broadway and N Larrabee Avenue (north and south legs, included in 2045 No-Build)
" N Weidler Street and N Vancouver Avenue (south leg)

[^2]" NE Broadway and NE Victoria Avenue (west leg)
" N/NE Broadway and N Williams Avenue (north leg)
» N Broadway and N Vancouver Avenue (south and west legs)

- Permitted pedestrian crossings with LPI
» N Broadway and N Larrabee Avenue (east leg)
" N Broadway Street and N Benton Avenue (all legs)
" N Weidler Street and N Vancouver Avenue (east leg)
» N/NE Weidler Street and N Williams Avenue (north and east leg)
» NE Weidler Street and I-5 northbound exit ramp (north leg)
" NE Broadway and NE Victoria Avenue (north leg)
» NE Broadway and N Williams Avenue (west leg)
> N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way (south leg)
- Pedestrian crossings are provided at all legs of the study intersections.


## Synchro Analysis Results

Synchro software was used for the analysis of the local street intersection operations to supplement the Vissim analysis. The Synchro analysis results are presented in Table 7 and Table 8 for the AM (8:00-9:00 AM) and PM (5:00-6:00 PM) peak hours, with locations that exceed $\mathrm{v} / \mathrm{c}$ mobility standards for ramp terminal intersections and LOS operational targets for local streets highlighted. As part of the adoption of the Central City 2035 Plan, the Central City, which includes the intersections in these tables, has been designated as a Multimodal Mixed-Use Area (MMA). This designation provides flexibility for determining effects of land use actions by lifting mobility standards requirements at ODOT facilities. Transportation standards such as safety and multimodal access still apply. Detailed HCM reports from Synchro are provided in Appendix E.

Table 7 Synchro Analysis Results: Future Conditions 8:00 AM - 9:00 AM

| ID | Intersection | 2045 No-Build Alternative |  |  | 2045 Revised Build Alternative 2-way Ramsay |  |  | 2045 Revised Build Alternative 2-way Wheeler |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | Delay (sec) | LOS | v/c | Delay (sec) | LOS | v/c | Delay (sec) | LOS |
| $1$ | N Broadway \& N Vancouver Ave (existing l-5 SB exit ramp) | 1.07 | 84.2 | F | 0.62 | 17.8 | B | 0.76 | 31.7 | C |
| 2 | N/NE Broadway \& N Williams Ave | 0.65 | 12.3 | B | 0.71 | 45.8 | D | 0.72 | 45.1 | D |
| 3 | NE Broadway \& NE Victoria Ave | 0.64 | 12.0 | B | 0.67 | 32.0 | C | 0.67 | 32.0 | C |
| 4 | NE Broadway \& NE 2nd Ave | 0.49 | 10.0 | B | 0.47 | 9.7 | A | 0.47 | 9.7 | A |
| $5$ | NE Weidler St \& NE 2nd Ave | 0.40 | 8.6 | A | 0.48 | 4.4 | A | 0.48 | 4.4 | A |
| $6$ | I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | 0.65 | 64.5 | E | 0.86 | 22.1 | C | 0.86 | 22.4 | C |
| 7 | N/NE Weidler St \& N Williams Ave | 0.32 | 3.7 | A | 0.12 | 45.8 | D | 0.12 | 51.2 | D |
| 8 |  <br> N Vancouver Ave | 0.49 | 9.3 | A | 0.55 | 16.8 | B | 0.66 | 25.8 | C |
| 9 | N Broadway \& N Benton Ave | 0.42 | 11.5 | B | 0.48 | 46.6 | D | 0.53 | 47.2 | D |
| 10 | N Broadway \& N Larrabee Ave | 0.59 | 9.7 | A | 0.69 | 28.0 | C | 0.61 | 22.2 | C |
| 11 | N Wheeler Ave/ N Williams Ave/ N Ramsay Way \& I-5 SB Ramps | 0.45 | 9.9 | A | 0.78 | 59.5 | E | 0.82 | 70.6 | E |
| 12 | N Williams Ave \& N/NE Hancock St | 0.33 | 14.3 | B | 0.43 | 17.0 | B | 0.43 | 16.3 | B |
| 13 | N Vancouver Ave \& NE Hancock St | - | - | - | 0.11 | 12.3 | B | 0.11 | 11.8 | B |
| 14 | N Williams Ave \& N/NE Multnomah St | 0.24 | 10.4 | B | 0.36 | 11.2 | B | 0.36 | 11.2 | B |

Note: Red $=v / c$ exceeds OHP in the No-Build Alternative or HDM mobility target in the Revised Build Alternative for ramp terminals or LOS below $D$ for signalized local intersections.

Table 8 Synchro Analysis Results: Future Conditions 5:00 PM - 6:00 PM

| ID | Intersection | 2045 No-Build Alternative |  |  | 2045 Revised Build Alternative 2-Way Ramsay |  |  | 2045 Revised Build Alternative 2-Way Wheeler |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | Delay (sec) | LOS | v/c | Delay (sec) | LOS | v/c | Delay (sec) | LOS |
| 1 | N Broadway \& N Vancouver Ave (existing l-5 SB exit ramp) | 0.92 | 44.2 | D | 0.40 | 14.8 | B | 0.63 | 32.8 | C |
| 2 | N/NE Broadway \& N Williams Ave | 0.57 | 13.5 | B | 0.66 | 37.2 | D | 0.67 | 32.6 | C |
| 3 | NE Broadway \& NE Victoria Ave | 0.53 | 9.1 | A | 0.55 | 21.3 | C | 0.55 | 21.5 | C |
| 4 | NE Broadway \& NE 2nd Ave | 0.40 | 10.0 | A | 0.32 | 10.0 | A | 0.32 | 9.7 | A |
|  | NE Weidler St \& NE 2nd Ave | 0.41 | 11.7 | B | 0.52 | 3.8 | A | 0.52 | 4.5 | A |
| 6 | I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | 0.60 | 19.7 | B | 0.71 | 16.2 | B | 0.71 | 14.9 | B |
|  |  <br> N Williams Ave | 0.46 | 4.3 | A | 0.26 | 24.4 | C | 0.26 | 22.9 | C |
| 8 |  <br> N Vancouver Ave | 0.63 | 13.3 | B | 0.56 | 17.3 | B | 0.64 | 18.6 | B |
| 9 |  <br> N Benton Ave | 0.50 | 20.6 | C | 0.55 | 30.9 | C | 0.53 | 33.9 | C |
| 10 | N Broadway \& N Larrabee Ave | 0.66 | 19.4 | B | 0.78 | 35.4 | D | 0.55 | 16.3 | B |
| 11 | N Wheeler Ave/ <br> N Williams Ave/ <br>  <br> I-5 SB Ramps | 0.40 | 12.2 | B | 0.84 | 57.9 | E | 0.88 | 68.9 | E |
| 12 | N Williams Ave \& N/NE Hancock St | 0.21 | 14.8 | B | 0.45 | 27.5 | C | 0.45 | 25.5 | C |
| 13 | N Vancouver Ave \& N/NE Hancock St | - | - | - | 0.09 | 11.2 | B | 0.09 | 10.8 | B |
| 14 | N Williams Ave \& N/NE Multnomah St | 0.36 | 11.0 | B | 0.36 | 11.1 | B | 0.36 | 11.1 | B |

Note: Red $=v / c$ exceeds OHP in the No-Build Alternative or HDM mobility target in the Revised Build Alternative for ramp terminals or LOS below $D$ for signalized local intersections.

As shown in Table 7 and Table 8, the I-5 southbound ramp terminal intersection at N Broadway/ N Vancouver Avenue would exceed the OHP mobility target in the 2045 No-Build Alternative, with a v/c of 1.07 in the AM peak hour and 0.92 in the PM peak hour. When relocated in the 2045 Revised Build Alternative, the N Wheeler/ N Williams/ N Ramsay Way and I-5 southbound
entrance and exit ramp terminal intersection would exceed the HDM mobility target (v/c of 0.75 or lower) in both design options, with a v/c of 0.78 to 0.88 during the AM and PM peak hours. With the addition of the southbound flyover traffic to the NE Weidler Street/ NE Victoria Avenue intersection, the I-5 northbound ramp terminal intersection is expected to exceed the HDM mobility target in the AM peak hour in both design options, with a v/c of 0.86 .

In the 2045 Revised Build Alternative, all study intersections would operate at LOS D or better in both the AM and PM peak hours in both design options except for the N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way and I-5 southbound entrance and exit ramp terminal intersection, which will operate at LOS E.

It should be noted that there are limitations with modeling separate bicycle and pedestrian only phases in Synchro, and that the analysis does not consider surrounding congestion or the full impacts of signal progression and queue spillback between intersections. Vissim analysis results below considered effects of queuing and congestion of adjacent intersections.

## Vissim Analysis Results

This section describes 2045 Revised Build Alternative local street traffic operations using delay and LOS results from the Vissim analysis for the AM (7:00-9:00 AM) and PM (4:00-6:00 PM) peak periods, with results provided for the peak and shoulder hours. This section also describes $95^{\text {th }}$ Percentile queue lengths for the I-5 northbound and southbound exit ramps, eastbound queues on $N$ Broadway from N Larrabee Avenue, and westbound queues on NE Broadway from NE Victoria Avenue. The Vissim analysis results are presented in Table 9, Table 10, Table 11, and Table 12. Detailed output showing volume, delay, and queue lengths for all movements at intersections are included in Appendix F.

In the 2045 Revised Build Alternative, the results of the Vissim analysis indicate that during the AM and PM peak hours, all intersections are expected to operate at LOS D or better in both design options. In comparison, there are multiple intersections in the 2045 No-Build Alternative that would operate at LOS E or F during the AM and PM peak hours. While most intersections in the 2045 Revised Build Alternative would operate at LOS D or better, intersection delays at some locations, particularly in the PM peak would be higher than the 2045 No-Build Alternative. This is primarily due to the proposed improvements on the I-5 mainline in the 2045 Revised Build Alternative that result in a higher volume of served vehicles on the local street network and the relocation of the I-5 southbound exit ramp, which re-routes vehicular movements compared to the $\mathbf{2 0 4 5}$ No-Build Alternative.

|  |  |  |
| :--- | :--- | :--- | :--- |
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Although overall vehicular intersection delay is expected to be higher at some locations in the 2045 Revised Build Alternative compared to the 2045 No-Build Alternative, the 2045 Revised Build condition would be better at balancing pedestrian safety and the delays of all modes with the addition of separate dedicated signal phases for bicycles, protected phases for pedestrians, and the use of Leading Pedestrian Intervals (LPIs) for permissive pedestrian crossings. More details are available in the Safety and Active Transportation Reports.

The Vissim analysis indicates that the l-5 northbound exit ramp intersection at NE Weidler Street/ NE Victoria Avenue would operate at LOS E in the 2045 No-Build Alternative in both the AM (8:00-9:00 AM) and PM (5:00-6:00 PM) peak hours. In comparison, under the 2045 Revised Build Alternative this intersection would operate at LOS C or better during both peak hours in both design options.

In the 2045 No-Build Alternative, the I-5 southbound exit ramp intersection at N Broadway/ N Vancouver Avenue would operate at LOS F in the PM (5:00-6:00 PM) peak hour. When relocated in the 2045 Revised Build Alternative, the I-5 southbound exit ramp intersection at N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way would operate at LOS D in both design options. When comparing operations for the I-5 southbound exit ramp approach in the PM peak hour, the exit ramp itself is operating at LOS F in the 2045 No-Build Alternative at the N Broadway/ N Vancouver Avenue intersection and LOS D in the 2045 Revised Build Alternative at the $\mathbf{N}$ Wheeler Avenue/ N Williams Avenue/ N Ramsay Way intersection. The flyover portion of the l-5 southbound exit ramp to NE Weidler Street is operating at LOS C.

Table 9 Vissim Analysis Results: Future Conditions 7:00 AM - 8:00 AM

| ID | Intersection | 2045 No-Build Alternative |  | 2045 Revised Build Alternative 2-Way Ramsay |  | 2045 Revised Build Alternative 2-Way Wheeler |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay (sec) | LOS* | Delay (sec) | LOS* | Delay (sec) | LOS* |
| 1 | N Broadway \& N Vancouver Ave (existing I-5 SB exit ramp) | 42.0 | D | 6.7 | A | 10.9 | B |
| 2 | N/NE Broadway \& N Williams Ave | 14.8 | B | 10.0 | B | 10.2 | B |
|  | NE Broadway \& NE Victoria Ave | 30.5 | C | 18.3 | B | 18.2 | B |
|  | NE Broadway \& NE 2nd Ave | 16.7 | B | 7.8 | A | 7.5 | A |
|  | NE Weidler St \& NE 2nd Ave | 6.6 | A | 5.3 | A | 5.4 | A |
| 6 | I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | 48.5 | D | 17.8 | B | 18.0 | B |
| 7 | N/NE Weidler St \& N Williams Ave | 3.6 | A | 3.3 | A | 3.5 | A |
| 8 |  <br> N Vancouver Ave | 10.9 | B | 18.1 | B | 15.4 | B |
| 9 | N Broadway \& N Benton Ave | 12.7 | B | 9.7 | A | 10.1 | B |
| 10 | N Broadway \& N Larrabee Ave | 10.5 | B | 19.3 | B | 15.4 | B |
| 11 | N Wheeler Ave/ N Williams Ave/ N Ramsay Way \& I-5 SB Ramps | 28.2 | C | 26.6 | C | 34.3 | C |
| 12 | N Williams Ave \& N/NE Hancock St | 11.4 | B | 15.5 | B | 15.5 | B |
| 13 | N Vancouver Ave \& NE Hancock St | - | - | 3.3 | A | 3.4 | A |
| 14 | N Williams Ave \& N/NE Multnomah St | 10.4 | B | 11.7 | B | 11.5 | B |

*LOS is non HCM compliant

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Table 10 Vissim Analysis Results: Future Conditions 8:00 AM - 9:00 AM

| ID | Intersection | 2045 No-Build Alternative |  | 2045 Revised Build Alternative 2-Way Ramsay |  | 2045 Revised Build Alternative 2-Way Wheeler |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay (sec) | LOS* | Delay (sec) | LOS* | Delay (sec) | LOS* |
| 1 |  <br> N Vancouver Ave <br> (existing l-5 SB exit ramp) | 43.8 | D | 7.9 | A | 15.1 | B |
| 2 | N/NE Broadway \& N Williams Ave | 16.3 | B | 9.9 | A | 11.1 | B |
| 3 | NE Broadway \& NE Victoria Ave | 38.9 | D | 23.5 | C | 24.8 | C |
| 4 | NE Broadway \& NE 2nd Ave | 27.7 | C | 10.6 | B | 11.0 | B |
| 5 | NE Weidler St \& NE 2nd Ave | 7.1 | A | 5.9 | A | 5.9 | A |
| 6 |  <br> NE Victoria Ave | 66.1 | E | 17.1 | B | 17.7 | B |
| 7 | N/NE Weidler St \& N Williams Ave | 3.6 | A | 3.8 | A | 4.3 | A |
| 8 | N Weidler St \& N Vancouver Ave | 12.9 | B | 19.5 | B | 17.3 | B |
| 9 | N Broadway \& N Benton Ave | 14.2 | B | 11.2 | B | 11.3 | B |
| 10 |  <br> N Larrabee Ave | 12.1 | B | 20.7 | C | 17.2 | B |
| 11 | N Wheeler Ave/ N Williams Ave/ N Ramsay Way \& I-5 SB Ramps | 37.2 | D | 30.1 | C | 38.0 | D |
| 12 | N Williams Ave \& N/NE Hancock St. | 11.2 | B | 16.9 | B | 16.6 | B |
| 13 | N Vancouver Ave \& NE Hancock St | - | - | 4.4 | A | 4.2 | A |
| 14 | N Williams Ave \& N/NE Multnomah St | 10.7 | B | 11.7 | B | 12.0 | B |

*LOS is non HCM compliant

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Table 11 Vissim Analysis Results: Future Conditions 4:00 PM - 5:00 PM

| ID | INTERSECTION | 2045 No-Build Alternative |  | 2045 Revised Build Alternative 2-Way Ramsay |  | 2045 Revised Build Alternative 2-Way Wheeler |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay <br> (sec) | LOS* | Delay <br> (sec) | LOS* | Delay <br> (sec) | LOS* |
| 1 |  <br> N Vancouver Ave (existing I-5 SB exit ramp) | 70.0 | E | 7.1 | A | 18.0 | B |
| 2 | N/NE Broadway \& N Williams Ave | 13.4 | B | 11.2 | B | 11.5 | B |
| 3 | NE Broadway \& NE Victoria Ave | 23.1 | C | 26.6 | C | 27.2 | C |
| 4 | NE Broadway \& NE 2nd Ave | 10.2 | B | 11.0 | B | 9.3 | A |
| 5 | NE Weidler St \& NE 2nd Ave | 9.8 | A | 10.7 | B | 10.9 | B |
| 6 | I-5 NB exit ramp at NE Weidler St \& NEVictoria Ave | 52.4 | D | 22.7 | C | 23.6 | C |
| 7 | N/NE Weidler St \& N Williams Ave | 13.8 | B | 3.4 | A | 3.4 | A |
| 8 |  <br> N Vancouver Ave | 22.3 | C | 14.3 | B | 18.6 | B |
| 9 |  <br> N Benton Ave | 13.4 | B | 12.2 | B | 12.6 | B |
| 10 |  <br> N Larrabee Ave | 28.7 | C | 26.7 | C | 21.2 | C |
| 11 | N Wheeler Ave/ N Williams Ave/ N Ramsay Way \& I-5 SB Ramps | 22.4 | C | 41.8 | D | 41.4 | D |
| 12 | N Williams Ave \& N/NE Hancock St | 10.8 | B | 28.5 | C | 27.8 | C |
| 13 |  <br> NE Hancock St | --- | --- | 2.8 | A | 3.0 | A |
| 14 | N Williams Ave \& N/NE Multnomah St | 11.6 | B | 11.7 | B | 11.7 | B |

Red $=$ LOS exceeds the City's operational target for local streets. *LOS is non HCM compliant

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Table 12 Vissim Analysis Results: Future Conditions 5:00 PM - 6:00 PM

| ID | Intersection | 2045 No-Build Alternative |  | 2045 Revised Build Alternative <br> 2-Way Ramsay |  | 2045 Revised Build Alternative 2-Way Wheeler |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay (sec) | LOS* | Delay (sec) | LOS* | Delay (sec) | LOS* |
| 1 |  <br> N Vancouver Ave <br> (existing I-5 SB exit ramp) | 87.6 | F | 6.8 | A | 17.3 | B |
| 2 | N/NE Broadway \& N Williams Ave | 15.4 | B | 11.4 | B | 11.7 | B |
| 3 | NE Broadway \& NE Victoria Ave | 28.1 | C | 34.3 | C | 33.4 | C |
| 4 | NE Broadway \& NE 2nd Ave | 11.4 | B | 17.8 | B | 16.8 | B |
| 5 | NE Weidler St \& NE 2nd Ave | 9.2 | A | 10.8 | B | 10.8 | B |
| 6 | I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | 75.4 | E | 23.4 | C | 23.9 | C |
| 7 | N/NE Weidler St \& N Williams Ave | 17.8 | B | 3.6 | A | 3.9 | A |
| 8 | N Weidler St \& N Vancouver Ave | 28.1 | C | 15.3 | B | 15.5 | B |
| 9 |  <br> N Benton Ave | 17.9 | B | 14.8 | B | 13.4 | B |
| 10 |  <br> N Larrabee Ave | 43.4 | D | 33.7 | C | 22.4 | C |
| 11 | N Wheeler Ave/ N Williams Ave/ N Ramsay Way \& I-5 SB Ramps | 28.5 | C | 43.4 | D | 43.7 | D |
| 12 | N Williams Ave \& N/NE Hancock St | 10.9 | B | 33.0 | C | 32.5 | C |
| 13 | N Vancouver Ave \& NE Hancock St | - | - | 2.9 | A | 3.1 | A |
| 14 | N Williams Ave \& N/NE Multnomah St | 11.5 | B | 11.8 | B | 11.7 | B |

Red $=$ LOS exceeds the City's operational target for local streets. *LOS is non HCM compliant

## Future Conditions $95^{\text {th }}$ Percentile Queue Length, feet

This section reports $95^{\text {th }}$ percentile queues at the I-5 southbound and northbound exit ramps, the eastbound approach of N Weidler at N Larrabee Avenue, and the westbound approach of NE Broadway/ NE Victoria Avenue based on the calculated $95^{\text {th }}$ percentile queue lengths. The methodology for calculating the $95^{\text {th }}$ percentile queue length has been updated for improved accuracy. Vissim queue counters were used to record the maximum queue length for each signal cycle length interval. The $95^{\text {th }}$ percentile queue length was calculated for each of the 10 simulation runs based on these "cycle length maximum queues". The resulting values were then averaged. The $95^{\text {th }}$ percentile queue lengths are shown in Table 13 for the AM peak period and Table 14 for the PM peak period.

Table 13 Future Conditions AM Peak Period 95th Percentile Queue Length, feet

| Location | 2045 No-Build Alternative |  |  | 2045 Revised Build Alternative 2-Way Ramsay |  |  | 2045 Revised Build Alternative 2-Way Wheeler |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Decel Length | Storage Length | Queue <br> Length | Decel Length | Storage Length | Queue <br> Length | Decel Length | Storage Length | Queue <br> Length |
| I-5 SB exit ramp at N Broadway \& N Vancouver Ave (2045 No-Build) | 410 | 590* | 250 | - | - | - | - | - | - |
| I-5 SB exit ramp at NE Wheeler Ave \& N Ramsay Way (Revised Build) | - | - | - | 415 | 1,440* | 430 | 415 | 1,440* | 590 |
| I-5 SB exit ramp at NE Weidler St \& NE Victoria Ave (Revised Build) | - | - | - | 415 | 2,250* | 275 | 415 | 2,250* | 275 |
| I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | 440 | 320* | >760*** | 510 | 490* | 430 | 510 | 490* | 455 |
| N Weidler St at N Larrabee Ave (EB approach) | - | 2,000** | 195 | - | 2,000** | 255 | - | 2,000** | 245 |
| NE Broadway at NE Victoria Ave (WB approach) | - | 1,000** | 1070 | - | 1,000** | 680 | - | 1,000** | 685 |
| *Storage Length on the exit ramps represent the full length of the ramp excluding the deceleration length <br> **Distance to NW Lovejoy Street and MLK Boulevard. <br> ***Queue exceeds the length of the ramp and mixes with l-5 mainline queues |  |  |  |  |  |  |  |  |  |

Table 14 Future Conditions PM Peak Period 95th Percentile Queue Length, feet

| Location | 2045 No-Build Alternative |  |  | 2045 Revised Build <br> Alternative <br> 2-Way Ramsay |  |  | 2045 Revised Build Alternative 2-Way Wheeler |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Decel Length | Storage Length | Queue Length | Decel Length | Storage Length | Queue Length | Decel Length | Storage Length | Queue Length |
| I-5 SB exit ramp at N Broadway \& N Vancouver Ave (2045 No-Build) | 410 | 590* | >1,000*** | - | - | - | - | - | - |
| I-5 SB exit ramp at NE Wheeler Ave \& N Ramsay Way (Revised Build) | - | - | - | 415 | 1,440* | 675 | 415 | 1,440* | 630 |
| I-5 SB exit ramp at NE Weidler St \& NE Victoria Ave (Revised Build) | - | - | - | 415 | 2,250* | 640 | 415 | 2,250* | 675 |
| I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | 440 | 320* | >760*** | 510 | 490* | 380 | 510 | 490* | 470 |
| N Weidler St at N Larrabee Ave (EB approach) | - | 2,000** | 1,520 | - | 2,000** | 815 | - | 2,000** | 620 |
| NE Broadway at NE Victoria Ave (WB approach) | - | 1,000** | 280 | - | 1,000** | 865 | - | 1,000** | 845 |
| *Storage Length on the <br> **Distance to NW Lovej <br> ***Queue exceeds the | exit ramps Street a ngth of th | epresent the d MLK Boule ramp and m | length of the ard. <br> xes with l-5 m | mp excludi <br> nline que | ing the decelera es. | tion leng |  |  |  |

In the updated 2045 No-Build Alternative, queuing on the southbound I-5 exit ramp exceeds the available storage in the PM peak hour, while queuing on the northbound I-5 exit ramp exceeds the available storage in both peak hours. It should be noted that when queues exceed the length of the ramp it becomes difficult to differentiate ramp queuing from mainline queuing, but queue spillback from the ramps does contribute to additional mainline congestion. The northbound I-5 exit ramp is a single lane exit in the 2045 No-Build Alternative and only has a single right-turn lane to eastbound NE Weidler Street. While this movement is considered "free-flow", vehicles must yield to bicycles and pedestrians which contributes to queuing that blocks the northbound through movement.

Queuing on the southbound I-5 exit ramp in the 2045 No-Build Alternative is the result of queue spillback on N Vancouver Avenue between N Broadway and NE Weidler Street as well as limited green time available at the ramp terminal intersection. Queuing on eastbound N Weidler Street is approximately 450 feet east of the NW Lovejoy Street and NW Broadway
intersection during the PM peak hour and queuing on westbound N Broadway during the AM peak hour extends to NE Martin Luther King Jr. Boulevard.

In the 2045 Revised Build Alternative, queues on the northbound and southbound I-5 exit ramps would not exceed the available storage or encroach into the deceleration area in the AM and PM peak hours in both design options. The northbound I-5 exit ramp is a two-lane exit in the 2045 Revised Build Alternative and includes a signalized dual right-turn lane to eastbound NE Weidler Street, which improves exit ramp queuing. The right-most right turn lane accommodates I-5 southbound traffic coming from the flyover, and the left-most right turn lane accommodates I-5 northbound traffic. The relocation of the southbound I-5 exit ramp also improves queuing in the 2045 Revised Build Alternative in both design options. In addition, both design options will provide adequate safe stopping distance for the current design speeds. The project team will explore a wide range of safety and operational enhancement treatments to manage potential traffic queues on the exit ramps through design refinement including, but not limited to, upstream queue detection for exit ramps intended to limit the potential for queuing to impact the mainline.

Eastbound queues on N Weidler Street in the PM peak hour would be less than in the 2045 No-Build Alternative. Westbound queues on N Broadway would also be reduced during the AM peak hour but would approach NE Martin Luther King Jr. Boulevard during the PM peak hour in both design options. There are additional signal phases at the NE Broadway/ NE Victoria Avenue intersection in the Revised Build Alternative that provide for protected pedestrian crossing on the west leg of the intersection. The reduced green time for westbound N Broadway results in increased queuing (approximately 600 additional feet of queuing) on westbound N Broadway in the PM peak hour.

### 6.2.2.3 Future Local Street Bicycle Conditions

## Bicycle Analysis (delay)

Bicycle delays through the signalized intersections were analyzed in Vissim for all dedicated bicycle lanes and are shown in Table 15 and Table 16 for the AM and PM peak hours. As shown below, the updated 2045 No-Build and 2045 Revised Build Alternatives are serving a similar volume of bicycles in both the AM and PM peak hours (Appendix G) but with considerably more delay in 2045 No-Build Alternative for key movements.

In the AM peak hour, southbound bicycles on N Vancouver Avenue are expected to experience over 2 minutes of delay in the 2045 No-Build Alternative due to the minimal amount of green time allowed for $N$ Vancouver Avenue. In comparison, southbound bicycles in the 2045 Revised Build Alternative would experience approximately 25 seconds of delay in both design options
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due to the removal of the l-5 southbound exit ramp and the additional green time allotted to N Vancouver Avenue.

It should be noted that southbound to westbound bicycles in the 2045 No-Build Alternative would continue using $\mathbf{N}$ Flint Avenue due to existing turn restrictions at $\mathbf{N}$ Vancouver Avenue and $\mathbf{N}$ Broadway that prohibit southbound right-turn movements across the existing l-5 southbound exit ramp. In the 2045 Revised Build Alternative bicycles could travel southbound on $\mathbf{N}$ Vancouver Avenue and turn right to westbound in both design options, but due to increased westbound bicycle/vehicular conflicts resulting in increased delays for $\mathbf{N}$ Flint Avenue traffic during the AM peak period, a portion of the southbound bicycles (approximately 250 bicycles in the AM peak period) were routed down N Vancouver Avenue resulting in an even bicycle trip distribution between $\mathbf{N}$ Flint Avenue and $\mathbf{N}$ Vancouver Avenue that helped to balance the southbound auto delays on N Vancouver Avenue and N Flint Avenue as cyclists and drivers will take the path of least resistance.

In the PM peak hour, northbound bicycles on N Williams Avenue are expected to experience 90 seconds of delay crossing NE Weidler Street and 2 minutes of delay crossing $N$ Broadway in the 2045 No-Build Alternative compared to approximately 30 seconds at both locations in both of the 2045 Revised Build Alternative design options. The reconfiguration of the intersection of N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way and I-5 southbound entrance ramp terminal intersection between the two alternatives would add additional signal phases that would result in greater delays for northbound bicycles in the PM peak hour in the 2045 Revised Build Alternative compared to the 2045 No-Build Alternative (approximately 60 seconds vs 30 seconds). It should be noted that the Clackamas Crossing in the 2045 Revised Build Alternative provides an alternate route for cyclists that originates east of I-5, reducing the number of northbound bicycles on N Williams Avenue compared to the 2045 No-Build Alternative ( $\mathbf{1 0}$ bicycles in the AM peak hour and 110 bicycles in the PM peak hour).

Refinements to signal timing and signal progression within the project area may reduce bicycle delays and will be further evaluated during design. Bicycle storage design and operations refinements will also be considered during the design phase.
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| Table 15 Future Conditions Bicycle Delay- 8:00 AM - 9:00 AM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | Intersection | Movement | 2045 No-Build Alternative |  | 2045 Revised Build Alternative 2-way Ramsay |  | 2045 Revised Build Alternative 2-way Wheeler |  |
|  |  |  | Volume <br> Served | Delay (sec) | Volume <br> Served | Delay (sec) | Volume <br> Served | $\begin{gathered} \text { Delay } \\ (\mathrm{sec}) \end{gathered}$ |
| 1 | N Broadway \& | WB Bicycle | 294 | 15.0 | 298 | 0.4 | 297 | 0.3 |
|  | (existing I-5 SB exit ramp) | SB Bicycle | 604 | 125.2 | 840 | 24.2 | 844 | 23.7 |
| 2 | N/NE Broadway \& | WB Bicycle | 306 | 44.3 | 309 | 40.8 | 308 | 52.4 |
|  | N Williams Ave | NB Bicycle | 94 | 12.7 | 100 | 8.6 | 101 | 10.7 |
| 3 | NE Broadway \& NE Victoria Ave | WB Bicycle | 307 | 9.1 | 309 | 16.1 | 309 | 15.8 |
| 4 | NE Broadway \& NE 2nd Ave | WB Bicycle | 306 | 23.6 | 306 | 7.3 | 306 | 7.3 |
| 5 | NE Weidler St \& NE 2nd Ave | EB Bicycle | 96 | 12.0 | 99 | 0.1 | 100 | 0.1 |
| 6 | l-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | EB Bicycle | 99 | 15.6 | 100 | 1.2 | 100 | 0.8 |
| 7 | N/NE Weidler St \& | EB Bicycle | 99 | 3.5 | 100 | 0.2 | 100 | 0.3 |
|  | N Williams Ave | NB Bicycle | 93 | 31.6 | 100 | 22.5 | 101 | 21.2 |
| 8 | N Weidler St \& | EB Bicycle | 147 | 29.2 | 147 | 32.1 | 148 | 34.2 |
|  | N Vancouver Ave | SB Bicycle | 569 | 44.1 | 598 | 30.8 | 599 | 25.8 |
| 9 | N Broadway \& | WB Bicycle | 1407 | 16.3 | 1419 | 12.5 | 1418 | 12.6 |
|  | $N$ Benton Ave | EB Bicycle | 147 | 1.3 | 152 | 0.3 | 152 | 0.6 |
| 10 | N Broadway \& | WB Bicycle | 1390 | 54.0 | 1427 | 24.4 | 1427 | 25.1 |
|  | N Larrabee Ave | EB Bicycle | 147 | 21.4 | 181 | 24.1 | 181 | 22.9 |
| 11 | N Wheeler Ave/ N Williams Ave/ | NB Bicycle | 47 | 29.3 | $40^{1}$ | 43.4 | $40^{1}$ | 42.8 |
|  | N Ramsay Way \& I-5 SB Ramps | SB Bicycle | 523 | 93.8 | 604 | 19.8 | 604 | 25.5 |

${ }^{1}$ Note: Revised Build Alternative reroutes 10 northbound bicycles from N Williams Avenue to the Clackamas Crossing during the AM peak.

| Table 16 Future Conditions Bicycle Delay -5:00 PM - 6:00 PM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | Intersection | Movement | 2045 No-Build <br> Alternative |  | 2045 Revised Build Alternative 2-way Ramsay |  | 2045 Revised Build <br> Alternative 2-way Wheeler |  |
|  |  |  | Volume Served | $\begin{gathered} \text { Delay } \\ (\mathrm{sec}) \end{gathered}$ | Volume Served | $\begin{gathered} \text { Delay } \\ \text { (sec) } \end{gathered}$ | Volume Served | $\begin{gathered} \text { Delay } \\ \text { (sec) } \end{gathered}$ |
| 1 | N Broadway \& | WB Bicycle | 68 | 18.7 | 68 | 0.0 | 69 | 0.1 |
|  | (existing l-5 SB exit ramp) | SB Bicycle | 58 | 35.4 | 60 | 23.8 | 61 | 25.2 |
| 2 | N/NE Broadway \& N Williams Ave | WB Bicycle | 100 | 52.7 | 101 | 52.9 | 100 | 57.1 |
|  |  | NB Bicycle | 1316 | 122.5 | 1421 | 30.2 | 1419 | 29.9 |
| 3 | NE Broadway \& NE Victoria Ave | WB Bicycle | 100 | 13.0 | 101 | 12.5 | 100 | 13.0 |
| 4 | NE Broadway \& NE 2nd Ave | WB Bicycle | 100 | 14.6 | 100 | 13.0 | 100 | 12.6 |
| 5 | NE Weidler St \& NE 2nd Ave | EB Bicycle | 96 | 14.7 | 96 | 0.9 | 98 | 1.0 |
| 6 | I-5 NB exit ramp at NE Weidler St \& NE Victoria Ave | EB Bicycle | 97 | 13.4 | 97 | 20.4 | 100 | 21.6 |
| 7 |  <br> N Williams Ave | EB Bicycle | 97 | 6.1 | 98 | 0.2 | 100 | 0.3 |
|  |  | NB Bicycle | 1383 | 89.8 | 1430 | 33.5 | 1433 | 33.9 |
| 8 |  <br> N Vancouver Ave | EB Bicycle | 810 | 45.3 | 821 | 32.8 | 822 | 33.0 |
|  |  | SB Bicycle | 47 | 17.5 | 49 | 43.3 | 50 | 32.7 |
| 9 | N Broadway \& N Benton Ave | WB Bicycle | 129 | 14.1 | 125 | 17.1 | 126 | 16.5 |
|  |  | EB Bicycle | 803 | 1.5 | 828 | 0.7 | 829 | 0.9 |
| 10 | N Broadway \& N Larrabee Ave | WB Bicycle | 129 | 17.7 | 125 | 20.9 | 126 | 20.3 |
|  |  | EB Bicycle | 813 | 61.4 | 862 | 34.8 | 862 | 33.1 |
| 11 | N Wheeler Ave/ N Williams Ave/ N Ramsay Way \& I-5 SB Ramps | NB Bicycle | 725 | 31.8 | $617^{1}$ | 61.7 | $608{ }^{1}$ | 57.7 |
|  |  | SB Bicycle | 46 | 13.8 | 49 | 32.5 | 49 | 34.7 |

${ }^{1}$ Note: Revised Build Alternative reroutes 110 northbound bicycles from $N$ Williams Avenue to the Clackamas Crossing during the PM peak.

## Bicycle Travel Time

Bicycle travel times going westbound and eastbound on N/NE Broadway and N/NE Weidler Street from west of $N$ Larrabee Avenue to east of NE 2nd Avenue were also evaluated using the Vissim simulated travel times for both the 2045 No-Build Alternative and 2045 Revised Build Alternative design options. The bicycle travel time segments are shown in Figure 7 and summarized in Table 17 and Table 18 for the AM and PM peak hours.

Figure 7 Bicycle Travel Time Routes


As shown below in Table 17 and Table 18 , bicycle travel times for the 2045 Revised Build Alternative are consistently shorter in both design options compared to the 2045 No-Build Alternative. Westbound travel times are up to $\mathbf{2 0}$ seconds slower in the 2-way Wheeler Design Option compared to the 2-way Ramsay Design Option due to the modified signal phasing at the $\mathbf{N}$ Broadway and N Vancouver Avenue intersection. In the 2-way Wheeler Design Option an additional signal phase is required to accommodate a left turn movement from northbound N Vancouver Avenue to westbound N Broadway. This results in less green time for westbound bicycle and vehicular traffic.

Table 17 AM Future Conditions Bicycle Travel Time, minutes

| Direction | 7-8 AM |  |  | 8-9 AM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $2045$ <br> No-Build | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler | $2045$ <br> No-Build | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build <br> Alternative 2-way Wheeler |
| Bicycle Westbound | 4.5 | 3.9 | 4.0 | 5.0 | 4.0 | 4.3 |
| Bicycle Eastbound | 3.6 | 3.2 | 3.2 | 3.6 | 3.2 | 3.2 |

Table 18 PM Future Conditions Bicycle Travel Time, minutes

| Direction | 4-5 PM |  |  | 5-6 PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $2045$ <br> No-Build | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build <br> Alternative 2-way Wheeler | $2045$ No-Build | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler |
| Bicycle Westbound | 4.2 | 4.1 | 4.1 | 4.5 | 4.3 | 4.4 |
| Bicycle <br> Eastbound | 4.2 | 3.6 | 3.5 | 4.9 | 3.6 | 3.6 |

### 6.2.2.4 Future Local Street Transit Conditions

## Bus Travel Time

Bus service travel times from the Vissim simulation results were used to assess bus operations under future conditions for the AM and PM peak periods. Three bus lines traverse the local intersections within the Project API and travel times were captured for the routes shown in Figure 8. Bus 4 and Bus 44 travel on $N$ Williams Avenue and $N$ Vancouver Avenue between NE Multnomah Street and NE Hancock Street and Bus 17 travels on N/NE Broadway from NE Grand Avenue to the Broadway Bridge west of N Larrabee Avenue.

Figure 8 Bus and Streetcar Travel Time Routes


As shown below in Table 19, northbound, southbound, and westbound bus service travel times are expected to be similar to or shorter in the 2045 Revised Build Alternative AM peak hours compared to the 2045 No-Build Alternative for both design options. With the removal of the I-5 southbound exit ramp at the N Broadway and N Vancouver Avenue intersection, there would be less congestion on $N$ Vancouver Avenue between N Broadway and NE Weidler Street and more green time would be provided for southbound traffic on $N$ Vancouver Avenue,
resulting in less queuing and delay compared to the 2045 No-Build Alternative condition. Eastbound bus service travel times are approximately 20 to $\mathbf{3 0}$ seconds longer compared to the 2045 No-Build Alternative.

During the PM peak period (see Table 20), southbound bus service travel times are approximately 20 seconds longer in the 2-way Ramsay Design Option and 50 seconds longer in the 2-way Wheeler Design Option compared to the 2045 No-Build Alternative. The relocation of the I-5 southbound exit ramp to the N Wheeler Avenue/ N Williams Avenue/ $\mathbf{N}$ Ramsay Way intersection adds an additional signal phase that reduces the green time for southbound traffic, affecting the overall travel time in both design options. The southbound bus travel time experiences an additional delay in the 2-way Wheeler Design Option due to the additional signal phase for the northbound left-turn movement at $\mathbf{N}$ Broadway/ N Vancouver Avenue, which reduces the green time available for southbound N Vancouver Avenue. The 2-way Wheeler Design Option also removes the southbound bus only lane between N Broadway and NE Weidler Street.

Northbound bus service travel times in the PM peak period are less than $\mathbf{2 0}$ seconds longer in duration compared to the 2045 No-Build Alternative. As previously noted, the 2045 Revised Build Alternative would include an additional traffic signal at the N Williams Avenue/ N/NE Hancock Street intersection that would affect northbound routes. The current design assumption is that a traffic signal is needed at this location to accommodate a diagonal bicycle crossing. Options for transitions to tie into existing bicycle facilities north of $N$ Broadway will be further evaluated during design. Eastbound and westbound bus routes for the 2045 Revised Build Alternative design options are up to 1 minute shorter compared to the 2045 No-Build Alternative in the PM peak period.

Refinements to signal timing and signal progression within the project area may shorten bus service travel times and will be further evaluated during design. The addition of transit signal priority, bus only lanes, bus queue jumps, and bus stop consolidation will also be evaluated as potential mitigation during design.
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Table 19 AM Future Conditions Bus Travel Time, minutes

| Direction | 7-8 AM |  |  | 8-9 AM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} 2045 \\ \text { No-Build } \end{gathered}$ | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler | $\begin{gathered} 2045 \\ \text { No-Build } \end{gathered}$ | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler |
| Bus 4 and 44 NB | 3.5 | 2.7 | 2.7 | 3.5 | 2.8 | 2.8 |
| Bus 4 and 44 SB | 3.4 | 3.3 | 3.5 | 4.0 | 3.4 | 3.5 |
| Bus 17 WB | 4.3 | 3.4 | 3.4 | 5.1 | 3.7 | 3.8 |
| Bus 17 EB | 3.0 | 3.1 | 3.2 | 3.3 | 3.6 | 3.8 |

Table 20 PM Future Conditions Bus Travel Time, minutes

| Direction | 4-5 PM |  |  | 5-6 PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $2045$ <br> No-Build | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler | $2045$ <br> No-Build | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler |
| Bus 4 and 44 NB | 3.6 | 3.6 | 3.5 | 3.7 | 4.0 | 3.7 |
| Bus 4 and 44 SB | 2.8 | 3.1 | 3.6 | 2.9 | 3.1 | 3.7 |
| Bus 17 WB | 4.7 | 4.0 | 4.1 | 4.9 | 4.0 | 4.1 |
| Bus 17 EB | 3.9 | 3.8 | 3.7 | 4.6 | 4.5 | 3.9 |

## Streetcar Travel Time

Streetcar service travel times from the Vissim simulation results were used to assess Streetcar operations under future conditions for the AM and PM peak periods. The travel time routes for both the westbound and eastbound streetcar are reported between NE Grand Avenue and the Broadway Bridge west of N Larrabee Avenue (see Figure 8). As shown below in Table 21 and Table 22, westbound Streetcar travel times in the 2045 Revised Build Alternative are expected to be shorter compared to 2045 No-Build, particularly during the AM and PM peak hours. Both design options have similar travel times with improvements of 30 seconds to 1 minute compared to the 2045 No-Build Alternative.

Eastbound Streetcar travel times are also similar between design options and would generally be within 20 to 25 seconds of the 2045 No-Build travel times during the AM peak period and 1 to 2 minutes shorter during the PM peak period. Refinements to signal timing within the project area could shorten eastbound Streetcar service travel times during the AM peak period and will be further evaluated during design.

Table 21 AM Future Conditions Streetcar Travel Time, minutes

|  | 7-8 AM |  |  | 8-9 AM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | $\begin{gathered} 2045 \\ \text { No-Build } \end{gathered}$ | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler | $\begin{gathered} 2045 \\ \text { No-Build } \end{gathered}$ | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler |
| Westbound Streetcar | 4.1 | 3.5 | 3.5 | 4.3 | 3.6 | 3.7 |
| Eastbound Streetcar | 3.3 | 3.7 | 3.7 | 3.2 | 3.6 | 3.6 |

Table 22 PM Future Conditions Streetcar Travel Time, minutes

|  | 4-5 PM |  |  | 5-6 PM |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Direction | $2045$ <br> No-Build | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler | $\begin{gathered} 2045 \\ \text { No-Build } \end{gathered}$ | 2045 Revised Build Alternative 2-way Ramsay | 2045 Revised Build Alternative 2-way Wheeler |
| Westbound Streetcar | 4.4 | 3.9 | 3.9 | 5.0 | 4.0 | 4.0 |
| Eastbound <br> Streetcar | 4.7 | 3.8 | 3.7 | 5.7 | 3.8 | 3.8 |

### 6.2.3 Indirect Impacts

There would be no additional indirect impacts under the 2045 Revised Build Alternative than those disclosed in the 2019 Traffic Analysis Technical Report. Similar to the Build Alternative, the 2045 Revised Build Alternative would have indirect impacts for event access to the Moda Center due to the relocation of the existing l-5 southbound exit ramp terminal. Potential mitigations in the traffic operations including wayfinding signage to guide traffic from the proposed $N$ Wheeler Avenue/ $\mathbf{N}$ Williams Avenue/ $N$ Ramsay Way southbound exit ramp to access the Moda Center and traffic signal adjustments would be necessary. During the design phase, traffic analysis of the ingress conditions would be performed to identify specific mitigation and develop event traffic management plan to accommodate the additional traffic volumes during both event ingress and egress conditions. Also, as described in the 2019 Traffic
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Analysis Technical Report, the Clackamas Crossing would provide an additional route for bicycles and pedestrians to cross I-5 using a separated facility with less exposure to motor vehicles and that can avoid crossing the complex intersections of ramp terminals. The Clackamas Crossing in the Revised Build Alternative provides additional grade separated connections compared to that described in the 2019 Traffic Analysis including a connection parallel to $\mathbf{N}$ Williams Avenue from the crossing to the southeast corner of the intersection of N Williams Avenue and N/NE Weidler Street and a direct connection from the crossing to the Garden Garage.

### 6.2.4 Cumulative Impacts

The cumulative impact analysis considered the Project's impacts combined with other past, present, and reasonably foreseeable future actions that would result in the environmental impacts in the Project Area. The travel demand model for this project is based on the 2014 Metro Regional Transportation Plan (RTP) and changes from the 2014 and 2018 RTP have been evaluated and reviewed. There are no changes in the projects considered for the RFFA list and therefore there are no updates on the trip generation, travel demand, or modeling used in the traffic analysis of the Project. Therefore, the cumulative impacts of the 2045 Revised Build Alternative would be the same as those reported in the 2019 Traffic Analysis Technical Report.

### 6.3 CONCLUSION

The traffic analysis presented in this supplemental report include the following results for the Revised Build Alternative:

- Traffic operations would improve at all highway segments including the four weaving segments between I-84 and I-405 in both the AM (7:00 AM to 9:00 AM) and PM (4:00 PM to 6:00 PM) analysis periods when compared to the 2045 No-Build Alternative.
- The I-5 southbound exit ramp terminal intersection at $\mathbf{N}$ Wheeler Avenue / N Williams Avenue/ N Ramsay Way intersection is expected to exceed the Highway Design Manual (HDM) mobility target (v/c of 0.75 or lower) in both the AM and PM peak hours in both design options. The I-5 northbound exit ramp terminal intersection at NE Weidler Street/ NE Victoria Avenue is expected to exceed the HDM mobility target (v/c of 0.75 or lower) during the AM peak hour in both design options.
- As part of the adoption of the Central City 2035 Plan, the Central City, which includes the I-5 ramp terminal intersections, has been designated as a Multimodal Mixed-Use Area (MMA). This designation provides flexibility for determining significant effects of land use actions by lifting mobility standards requirements at ODOT facilities. Transportation standards such as safety and multimodal access still apply. Although both ramp terminal

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intersections exceed the HDM mobility target, the Revised Build Alternative reduces exit ramp queuing and provides bicycle and pedestrian crossing improvements.

- All intersections would operate at acceptable LOS D or better using Synchro analysis results except for the N Wheeler Avenue/ N Williams Avenue/ N Ramsay Way and I-5 southbound entrance and exit ramp terminal intersection, which will operate at LOS E.

All intersections would operate at LOS D or better in the AM and PM peak hours using Vissim analysis results.
$95^{\text {th }}$ percentile queue lengths on the l-5 northbound and southbound exit ramps would be reduced in the 2045 Revised Build Alternative compared to the 2045 No-Build Alternative and would not exceed the proposed ramp storage length approaching both ramp terminals.

- Eastbound queuing on N Weidler Street in the PM peak hour would be less than in the 2045 No-Build Alternative and westbound queuing on N Broadway would be less during the AM peak hour but would approach Martin Luther King Jr. Boulevard during the PM peak hour, which is approximately 600 feet longer compared to the 2045 No-Build Alternative.

Bicycle delays in the eastbound and westbound direction would generally be shorter compared to those in the No-Build Alternative. Bicycle delays in the northbound and southbound direction would generally be shorter compared to those in the No-Build Alternative except for southbound bicycles at the $\mathbf{N}$ Weidler Street and $\mathbf{N}$ Vancouver Avenue intersection and northbound bicycles at the $\mathbf{N}$ Wheeler Avenue/ $\mathbf{N}$ Williams Avenue/ N Ramsay Way and I-5 southbound entrance ramp terminal intersection in the PM peak hour ( $\mathbf{1 5}$ to $\mathbf{3 0}$ seconds longer).

- Bicycle travel times in both the eastbound and westbound direction would be shorter compared to those in the No-Build Alternative. Westbound travel times would be up to 20 seconds slower in the 2-way Wheeler Design Option compared to the 2-way Ramsay Design Option.
- Bus travel times would be shorter in the northbound, southbound, and westbound routes during the AM peak period compared to the No-Build and would be longer in the eastbound routes by 20 to $\mathbf{3 0}$ seconds. During the PM peak period, Revised Build Alternative bus travel times would be similar to or shorter in the westbound, eastbound, and northbound direction and would be longer in the southbound direction compared to the No-Build Alternative. The 2-way Wheeler Design Option is approximately 30 seconds longer in the southbound direction compared to the 2-way Ramsay Design Option.
- Streetcar travel times in the westbound direction would be between 30 seconds and 1 minute shorter compared to the No-Build Alternative and would be 20 to 25 seconds
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longer in the eastbound direction during the AM peak period compared to No-Build Alternative.


### 7.0 AVOIDANCE, MINIMIZATION, AND MITIGATION MEASURES

Mitigation measures would be the same as reported in the 2019 Traffic Analysis Technical Report.
8.0 PREPARERS

| NAME | DISCIPLINE | EDUCATION | YEARS OF <br> EXPERIENCE |
| :--- | :--- | :---: | :---: |
| Jeremy Jackson | Traffic Engineer | B.S. in Civil Engineering | $\mathbf{1 8}$ |
| Mingwei Shen | Traffic Engineer | B.S. in Civil Engineering | $\mathbf{5}$ |
| Simon Eng | Traffic Engineer | B.S. in Civil Engineering | $\mathbf{3 5}$ |

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## Appendix A: List of Reasonably Foreseeable Future Actions

# REASONABLY FORESEEABLE FUTURE ACTIONS COMPARISON 

Date: Tuesday June 15, 2022 [REVISED SEPTEMBER 1, 2023]
Project: K19071 I-5 Rose Quarter Improvement Project
To: Steve Drahota
From: Brian Bauman

Subject: Reasonably Foreseeable Future Actions Comparison

### 1.0 INTRODUCTION

Reasonably Foreseeable Future Actions (RFFAs) having the potential to contribute to a cumulative effect with the Build Alternative for the I-5 Rose Quarter Improvement Project (Project) were identified in 2019 technical reports supporting the Project's Environmental Assessment (EA) and the Finding of No Significant Impact (FONSI) and Revised EA. The purpose of this memo is to review the RFFAs documented in the 2019 technical reports and update them based on changes in plans for future development in the Project vicinity. The updated RFFAs presented herein are used in the assessment of cumulative environmental effects of the Project's Revised Build Alternative presented in the I-5 Rose Quarter Improvement Project Supplemental EA.

### 2.0 RFFA ASSESSMENT

As part of the cumulative impacts analysis included in the 2019 technical reports, ODOT considered planned and programmed projects in the Project Area and surrounding areas that are likely to be implemented by 2045 to be reasonably foreseeable. Future (2045) traffic conditions were interpolated from Metro's regional travel demand model which is built on population and employment growth forecasts adopted by the Metro Council and the financially constrained project list included in the 2014 Regional Transportation Plan (RTP). This updated RFFA assessment compares projects included in the most recent 2018 RTP that may contribute to a cumulative effect with the Project with the RFFAs documented in the 2019 technical reports.

### 2.1 LAND USE ASSUMPTIONS - LAND USE AND ASSUMPTIONS FOR RFFAS

The RFFAs included in the 2019 technical reports include City-owned parcels proposed for redevelopment (East/West parking garages, Benton surface parking lot, Phase II Entertainment Lot); improvements to the Veterans Memorial Coliseum, Moda Center, Annex lot plus building; and private redevelopment (Vulcan/Thunderbird site west of $N$ Interstate and the Weston-owned site at N Larrabee and $N$ Broadway). In addition to these actions, public entities such as the Portland Water Bureau, TriMet, Metro/Oregon Convention Center, Portland Public Schools, and Multnomah County plan to undertake improvement projects within the area before 2045.

Both the 2014 and 2018 RTPs support the implementation of the 2040 Growth Concept, which is the region's adopted land use and transportation strategy for managing growth and building healthy, equitable communities and a strong economy. The RFFAs listed above were included in both the 2014 RTP and the 2018 RTP and are the only projects that may have an impact on traffic within the I-5 Rose Quarter Improvement Project Area. Additional assumptions can be found in Appendix M Attachment 3 (Page 77) of the 2018 RTP dated December 6 ${ }^{\text {th }}, 2018$.

For the 2019 Traffic Analysis Technical Report and the 2023 Revised Traffic Analysis Supplemental Technical Report, the Project team utilized the regionally adopted population and employment numbers associated with Metroscope and the Regional Travel Demand Model as the baseline for travel demand development in conjunction with Metro. Additionally, the adopted I-5 Rose Quarter Project in the RTP was coordinated with the updates to the Comprehensive Plan and Zoning designations in the NNE quadrant plan covering the project study area. It should be noted that the comprehensive plan and zoning designations in the study area were designated primarily General Commercial (GC) which allows for the maximum density. While there have been changes or additional detail to proposed developments in the Project Area, these do not change the underlying assumptions of build-out of those parcels in accordance with the applicable comprehensive plan designations.

Since the FONSI and Revised EA were released in 2020, the Portland Public School's Long Range Facility Plan lists Harriet Tubman Middle School (HTMS) as under consideration for relocation (PPS 2021) and funding for the relocation is provided to the Oregon Department of Administrative Services in Oregon House Bill 5202, Section 323 which was signed by Governor Brown on April 4, 2022. The relocation of HTMS is a new RFFA for purposes of cumulative analyses for the Supplemental EA. The middle school occupies approximately 2.2 acres zoned Commercial Mixed Use and 0.13 acres zoned
Reasonably Foreseeable Future
Actions Comparison

Open Space. After the school use of the existing building relocates, re-use of the land and building could include several potential outcomes, and it is not possible to predict how the land will be used. In the event the buildings are demolished, and the site is redeveloped under the current zoning, the 2.2-acre Commercial Mixed Use 3 portion could support a large-scale mixed-use building with 6-7 stories including retail, office, residential, institutional, and limited industrial uses. There is a minimum residential density requirement of 1 unit per 1,000 square feet of site area, which would translate to a minimum of approximately 95 residential units.

### 2.2 TRANSPORTATION ASSUMPTIONS FREEWAY VOLUMES AND 2019 ASSUMPTIONS

The Columbia River Crossing Project is included in the 2014 RTP financially constrained project list and is in Metro's 2014 regional travel demand model (RTDM). The Columbia River Crossing Project remained in the financially constrained list in the 2018 RTP (See Table 4 in Appendix M of the 2018 RTP dated December $6^{\text {th }}$, 2018, on Page 13). Tolling was assumed as a part of the Columbia River Crossing Project (Appendix 3.4 of the 2014 RTP Technical Appendix on Page 337 and Appendix M of the 2018 RTP on Page 13). No other major projects have been completed or incorporated into the RTP that would substantially affect travel volumes, therefore there are no changes to the RFFAs in the Revised Traffic Analysis Supplemental Technical Report.

Projects under the Oregon Toll Program were not on the 2014 or 2018 RTP financially constrained list and, therefore, were not included as part of the future modeling scenarios in the 2019 Traffic Analysis Technical Report. Tolling is currently in an environmental review process for l-205 at the Abernethy Bridge (I-205 Toll Project), as well as in a planning phase for I-5 and other portions of I-205 (Regional Mobility Pricing Project; RMPP). Volume development for the traffic analysis for the Supplemental EA was conducted from November 2021 to December 2021. Metro added the I-205 Toll Project (which, at that time included tolls at the Abernethy and Tualatin River bridges) to the RTP financially constrained list in May 2022; i.e., after volume development for the Supplemental EA was complete. Regional modeling performed for the I-205 Toll Project in 2021 determined that daily volume changes resulting from the l-205 Toll Project alternatives would be negligible (less than $2 \%$ in volume) on l-5

|  | I-5 ROSE |  |
| :--- | :--- | :--- |
| Reasonably Foreseeable Future |  |  |
| Actions Comparison | 3 | QUARTER |
| MPROVEMENT PROJECT |  |  |

at the Marquam Bridge (i.e., south of the l-5 Rose Quarter Improvement Project). ${ }^{1}$. Therefore, the RFFAs for the l-5 Rose Quarter Improvement Project were not updated to include the I-205 Toll Project and ODOT determined there would not be analytical value to performing sensitivity tests related to the effects of the I-205 Toll Project on the I-5 Rose Quarter Improvement Project.

The RMPP is not on the 2018 RTP financially constrained list and therefore was not considered as an RFFA in the Supplemental EA. Due to public interest, ODOT had its consultant team conduct a sensitivity analysis of the potential influence of the RMPP on I-5 in the Project area. The results of that analysis are contained in Appendix D of the 2023 Revised Traffic Analysis Supplemental Technical Report. Because the RMPP is in the early stages of planning, and assumptions used in the sensitivity analysis are likely to change as the RMPP project elements become more defined in subsequent phases, the results have many limitations.

### 2.3 TRANSPORTATION ASSUMPTIONS - LOCAL STREET VOLUMES AND 2019 ASSUMPTIONS

As a part of the multi-modal traffic modelling work, the 2019 Traffic Analysis Technical Report included additional network refinement and operational detail based on input from the City of Portland, including elements of the Central City in Motion project. The primary change was lane reallocations on Broadway. These changes were incorporated in the 2018 RTP, and thus the change is consistent with that plan. The Broadway MultiModal Corridor project is project \#11646 in the 2018 RTP. No other projects have been completed or incorporated into the RTP that would affect travel volumes, therefore there are no changes to the RFFAs in the Traffic Analysis Supplemental Technical Report.

### 3.0 FINDINGS

The RFFAs identified for the 2019 technical reports to support the cumulative impacts analysis of the Project Build Alternative were reviewed to determine if updates were needed to assess traffic and cumulative impacts of the Revised Build Alternative. The 2014 and 2018 RTPs were also reviewed and compared. No projects were added to or removed from the RFFA list that would affect traffic impacts, volumes, or performance in

[^3]the project area. The relocation of HTMS may impact future use of the existing site; however, neither the relocations nor the RFFAs have resulted in updates that would result in any changes to trip generation, travel demand or to modeling used in the evaluation of the Project.

## Appendix B: Regional Mobility Pricing Project / Rose Quarter Regional Travel Demand Model Sensitivity Test Results Summary

# Regional Mobility Pricing Project 

## Memorandum

| Date | July 21, 2022 |
| :---: | :---: |
| To | I-5 Rose Quarter Improvement Project Team |
| From | Regional Mobility Pricing Project Team |
| Subject | RMPP/RQ Regional Travel Demand Model Sensitivity Test Results Summary |

## 1 Purpose

This memo provides a summary of regional travel demand model (RTDM) results in the vicinity of the l-5 Rose Quarter Improvement Project (RQ Project) for different future model scenarios in 2045. Specifically, this review looked at the impacts that the RQ Project and the Regional Mobility Pricing Project (RMPP) could have on each other. This sensitivity analysis also was prepared to further address issues identified by the RQ Project team in response to stakeholder questions received during the 2019 Environmental Assessment public comment period for the RQ Project.

The Portland Metro RTDM was used to provide high level traffic analysis and comparisons to better understand the relationship between the two projects. The RQ Project would include construction of additional auxiliary lanes and shoulders on I-5 between I-84 and I-405. The RMPP would apply pricing (tolls) on all lanes of I-5 and I-205 to manage traffic congestion.

## 2 Methodology/Assumptions

Four model scenarios were evaluated in 2045 and compared to assess potential changes in conditions with and without RMPP and with and without the RQ Project improvements. Table 1 shows major projects that were included for each scenario. Scenarios with RQ Project improvements are called No Build while scenarios without RMPP are called No Action.

The RMPP (Action) scenarios include preliminary modeling toll rate assumptions developed for the Initial Congestion Pricing Concept (ICPC). The ICPC scenario was developed to address congestion in 2045 baseline (No Action) conditions. These assume construction of the RQ Project and other (constrained) projects in the Regional Transportation Plan that have been identified as reasonably likely to be funded by 2045. The RMPP toll rate assumptions will be updated/refined as the project is developed further.

The ICPC toll rate assumptions are assumed to be variable by time of day based on an hourly schedule, not dynamically priced as a function of congestion. No adjustments or modifications were made to the toll rate assumptions to account for RQ Project Build/No Build status. The toll rate assumptions were held constant between the two model scenarios that include the RMPP.

Table 1. Scenarios Compared in 2045

|  | Baseline Scenarios for RMPP |  | Additional Scenarios for <br> Sensitivity Test |  |
| :---: | :---: | :---: | :---: | :---: |
|  | RMPP No Action <br> w/ RQ Build | RMPP ICPC <br> w/ RQ Build | RMPP No Action <br> w/ RQ No Build | RMPP ICPC <br> w/ RQ No Build |
| I-205 Toll Project | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| I-205 Improvements Project | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| IBR Program Toll | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| IBR Program Improvements | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Rose Quarter Improvement <br> Project | $\checkmark$ | $\checkmark$ | $\mathbf{x}$ | $\mathbf{x}$ |
| RMPP Initial Congestion Pricing <br> Concept | $\mathbf{x}$ | $\checkmark$ | $\mathbf{x}$ | $\checkmark$ |

## 3 Limitations

Specific results from the RTDM scenarios are expected to differ from the RQ Project technical analysis, as different methodologies, assumptions, and tools are applied in each project. RMPP project results are also expected to change as more detailed and refined analysis will be performed during later project phases.

Regional travel demand models do not supersede or replace the need for more refined traffic operations analysis currently being conducted by the RQ project team. The RTDM forecasts are generally not appropriate for directly predicting future traffic conditions at specific locations. They are best used to support planning decision-making by providing relative comparisons between scenarios and high-level indicators of potential changes in key performance measures.

The RMPP's ICPC was not designed to eliminate traffic congestion in the Rose Quarter but was designed to manage demand and congestion along the I-5 and I-205 corridors in the Portland metro area, assuming the RQ Project improvements have been constructed on I-5. Either updating the project objectives or the baseline assumptions could change the assumed/applied toll rates of the RMPP.

The analysis presented is limited to consideration of results on the I-5 mainline and does not include evaluation of potential changes in traffic conditions on other nearby roadways in the area around the RQ Project.

## 4 Results

Tables 2 and 3 show the peak hour model volumes on I-5 between I-405 and I-84 for each of the four scenarios. All model scenarios reflect average weekday conditions in 2045 . While the number of trips on I-5 increases under a RQ Project build scenario for all four conditions analyzed (two in the AM and two in
the PM), the model network changes indicate that most of these trips are rerouting from other roadways that are alternatives to $l-5$. This reflects the model reacting to changed conditions to increase the efficiency of the network by transferring trips to l-5 and away from a more congested alternatives such as I-405 and/or surface streets near I-5.

Table 2. 2045 Average Weekday Traffic Volumes on I-5 between I-405 and Broadway/Weidler Interchange

| 8-9 AM | RMPP No Action |  | RMPP ICPC |  |
| :---: | :---: | :---: | :---: | :---: |
|  | RQ No Build | RQ Build | RQ No Build | RQ Build |
| NB | 4,948 | 5,634 | 3,938 | 4,179 |
| SB | 4,605 | 5,190 | 3,356 | 3,931 |


| 5-6 PM | RMPP No Action |  | RMPP ICPC |  |
| :---: | :---: | :---: | :---: | :---: |
|  | RQ No Build | RQ Build | RQ No Build | RQ Build |
| NB | 4,487 | 5,121 | 3,425 | 3,327 |
| SB | 5,624 | 5,710 | 4,370 | 4,071 |

Source: Metro Regional Travel Demand Model
Table 3. 2045 Average Weekday Traffic Volumes on I-5 between I-84 and Broadway/Weidler Interchange

| 8-9 AM | RMPP No Action |  | RMPP ICPC |  |
| :---: | :---: | :---: | :---: | :---: |
|  | RQ No Build | RQ Build | RQ No Build | RQ Build |
| NB | 4,711 | 5,437 | 4,150 | 4,519 |
| SB | 4,328 | 4,884 | 3,531 | 3,900 |


| 5-6 PM | RMPP No Action |  | RMPP ICPC |  |
| :---: | :---: | :---: | :---: | :---: |
|  | RQ No Build | RQ Build | RQ No Build | RQ Build |
| NB | 4,839 | 5,534 | 4,160 | 4,129 |
| SB | 5,046 | 5,547 | 4,297 | 4,236 |

Source: Metro Regional Travel Demand Model

Both the RQ Project build and the RMPP ICPC would be expected to result in changes in traffic volumes, circulation patterns, and traffic operations on I-5 and other roadways near the RQ Project area. RQ Project improvements are expected to increase the driver's ability to safely navigate the roadway near the junctions of $\mathrm{I}-5, \mathrm{I}-405$, and $\mathrm{I}-84$. The RMPP is expected to manage demand to help prevent traffic flow breakdowns with their associated social, economic, and environmental costs. Both of these projects support improved traffic flow and reduced congestion on I-5. While additional analysis would be needed to fully understand the expected changes in traffic operations, looking at relative differences in speeds from the RTDM can provide insights for these projects.

Table 4 and 5 below show the RTDM forecast vehicle speeds during peak hours on I-5 between I-405 and I-84 for each of the four scenarios. All model scenarios reflect average weekday conditions in 2045. It should be noted that small differences in speeds (less than a few miles per hour) are negligible and should not be viewed as a substantive difference between scenarios.

Table 4. 2045 Average Weekday Traffic Speed (in mph) on I-5 between I-405 and Broadway/Weidler Interchange

| 8-9 AM | RMPP No Action |  | RMPP ICPC |  |
| :---: | :---: | :---: | :---: | :---: |
|  | RQ No Build | RQ Build | RQ No Build | RQ Build |
| NB | 22 | 33 | 39 | 44 |
| SB | 39 | 37 | 45 | 44 |
| 5-6 PM | RMPP No Action |  | RMPP ICPC |  |
|  | RQ No Build | RQ Build | RQ No Build | RQ Build |
| NB | 31 | 39 | 43 | 46 |
| SB | 31 | 35 | 42 | 45 |

Source: Metro Regional Travel Demand Model

Table 5. 2045 Average Weekday Traffic Speed (in mph) on I-5 between I-84 and Broadway/Weidler Interchange

| 8-9 AM | RMPP No Action |  | RMPP ICPC |  |
| :---: | :---: | :---: | :---: | :---: |
|  | RQ No Build | RQ Build | RQ No Build | RQ Build |
| NB | 14 | 32 | 27 | 41 |
| SB | 38 | 39 | 44 | 44 |


| 5-6 PM | RMPP No Action |  | RMPP ICPC |  |
| :---: | :---: | :---: | :---: | :---: |
|  | RQ No Build | RQ Build | RQ No Build | RQ Build |
| NB | 14 | 33 | 27 | 44 |
| SB | 33 | 36 | 41 | 44 |

Source: Metro Regional Travel Demand Model
The RQ Project would not construct any improvements to I-5 southbound between I-405 and Broadway/Weidler interchange; the added auxiliary lane and shoulder in the southbound direction begins south of the southbound Broadway exit. RTDM traffic speed results in this section show limited changes when comparing RQ No-Build and RQ Build in the RMPP ICPC. A more detailed traffic operations analysis is needed to incorporate additional operational factors such as downstream queuing impacts. However, some trends can be identified.

In general, most freeway facilities tend to operate with maximum vehicle flow when average speeds are between 40 mph and 50 mph . Speeds below 40 mph usually indicate a freeway with congestion that negatively impacts its ability to efficiently move vehicles and that can lead to major flow breakdowns. To achieve speeds above 50 mph , the freeway is not likely to be carrying all traffic that it could. The analysis indicates that speeds between 40 mph and 50 mph are achieved on all roadway segments only where both the RMPP and the RQ Project improvements are in place.

Table 6 shows the number of hours per day that congestion can be expected to be experienced on I-5 for each of four scenarios and shows the complementary effect with both strategies in place. All model scenarios reflect average weekday conditions in 2045.

RMPP/RQ Regional Travel Demand Model Sensitivity Test Results Summary / July 21, 2022

Table 6. 2045 Daily Number of Hours with Congestion on I-5 between I-84 and I-405

|  | RMPP No Action |  | RMPP ICPC |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | RQ No Build | RQ Build | RQ No Build | RQ Build |  |
| Between I-405 and <br> Broadway/Weidler Interchange | NB | 13 | 6 | 7 | 0 |
| Between I-84 and <br> Broadway/Weidler Interchange | SB | 6 | 8 | 0 | 0 |
|  | NB | 15 | 13 | 12 | 0 |

Note: Congestion defined when the ratio of hourly model volume to roadway capacity exceeds 0.8. Source: Metro Regional Travel Demand Model

## 5 Summary of Findings

The following observations were made based on comparing the RTDM results for 2045 scenarios:

- Both the RQ Project and RMPP Initial Congestion Pricing Concept (ICPC) were needed to reduce congestion below the congestion threshold ( $0.80 \mathrm{~V} / \mathrm{C}$ ) for all hours and directions of travel.
- RMPP ICPC could reduce peak hour volumes/demand on I-5 by approximately 1,000 vehicles per hour or more in each direction near the Rose Quarter.
- The RQ Project and RMPP ICPC are each expected to reduce the duration and severity of congestion on I-5 near the Rose Quarter.
- RMPP ICPC is comparatively more effective at improving speeds to above 40 mph .
- RMPP ICPC toll rate assumptions would need to be refined if RQ Project improvements are not constructed. Otherwise, severe congestion would remain on northbound I-5 near I-84.
- For a more refined operational analysis, post-processing of the RTDM results is necessary.


## Appendix C: 2045 No Build and 2045 Build AM and PM Peak Hour Traffic Volumes

Revised Traffic Analysis Supplemental
Technical Report


Figure 1 - No-Build 2045 AM Peak Hour Volumes






## Appendix D: Auxiliary Lane Analysis

## Auxiliary Lane Analysis

This Appendix provides the results of the Auxiliary Lanes analysis for the I-5 Rose Quarter Project. The 2023 Analysis Procedure Manual ${ }^{4}$ has been updated to include a new traffic analysis methodology for evaluating auxiliary lanes to determine whether the freeway weaving lanes function as an auxiliary lane or as a regular through lane that would add system capacity. The methodology utilizes the volume ratio (VR), which is defined as the ratio between the weaving flows (i.e., sum of the freeway to exit ramp and freeway to entrance ramp flows) and total demand flow in the weaving section. The volume ratio needs to be computed and compared with the maximum weaving lengths in Exhibit 10A-2 of the Highway Capacity Manual (HCM) to determine if the given weaving segment length is less than the indicated distances. If it is, then the weaving lane would function as an auxiliary lane. If the given weaving segment length is greater than the maximum operational weaving length, the auxiliary lane would result in system capacity increase.

| Exhibit 10A-2: Maximum (Operational) Weaving Length (mi) ${ }^{1}$ |  |  |
| :---: | :---: | :---: |
| VR | SINGLE LANE ENTRANCE/ EXIT RAMPS | DUAL LANE ENTRANCE AND/OR EXIT RAMP ${ }^{\mathbf{2}}$ |
| 0.1 | 0.7 | 0.4 |
| 0.2 | 0.9 | 0.6 |
| 0.3 | 1.1 | 0.8 |
| 0.4 | 1.3 | 0.9 |
| 0.5 | 1.5 | 1.2 |
| 0.6 | $1.7^{\text {a }}$ | 1.4 |
| 0.7 | n/a | 1.6 |

${ }^{1}$ Maximum weaving length calculations based on HCM 7th Edition Equation 13-4.
${ }^{2}$ The dual entrance/exit ramps are full lanes and not widened for ramp metering.
${ }^{a}$ Value obtained from HCM 7th Edition Exhibit 13-11, which is based on Equation 13-4.

[^4]$$
V R=\frac{\left(v_{F R}+v_{R F}\right)}{\left(v_{F F}+v_{R F}+v_{F R}+v_{R R}\right)}
$$

Where:
$V_{F R}=$ Freeway to exit ramp flow
$V_{\text {RF }}=$ Exit ramp to freeway flow
$V_{\text {FF }}=$ Freeway through flow
$V_{R R}=$ Entrance ramp to exit ramp flow (optional)
This new methodology was applied to evaluate the freeway sections in the Revised Build Alternative including the I-5 northbound auxiliary lane from the I-84 entrance ramp to the N Greeley Avenue exit ramp and the I-5 southbound auxiliary lane from the $N$ Greeley Avenue entrance ramp to the Morrison Bridge exit ramp.

The analysis shows that both the I-5 northbound section from the I-84 entrance ramp to the N Greeley Avenue exit ramp and the l-5 southbound section from the N Greeley Ave entrance ramp to the Morrison Bridge exit ramp are expected to operate as an auxiliary lane and would not result in system capacity increase.

There are two nested weaving lanes within each of the northbound and southbound full auxiliary lanes. These nested weaving lanes are:

1. I-5 northbound from I-84 entrance ramp to NE Weidler Street exit ramp,
2. I-5 northbound from N Broadway entrance ramp to $\mathrm{l}-405$ exit ramp,
3. I-5 southbound from I-405 entrance ramp to N Broadway exit ramp, and
4. I-5 southbound from NE Wheeler Street entrance ramp to I-84 exit ramp

These nested auxiliary lanes were each evaluated individually. It was determined that all four nested auxiliary lanes would operate as auxiliary lanes and would not result in system capacity increase.

## Appendix D - Table 1-I-5 NB Aux. Lane from I-84 entrance ramp to Greeley Ave exit ramp 2045 AM and PM Peak Hour Volumes

$V_{\text {fR }}=$ Sum of upstream freeway volume to Weider, $1-405$ and Greeley exit ramps
$V_{\text {VF }}=1-84$ ramp to freeway north of Greeley exit ramp + Broadway ramp to freeway north of Greeley exit ramp - i.e. entrance ramp traffic continuing to NB $1-5$
$V_{\text {RR }}=1-84$ ramp to $1-405$ and Greeley exit ramps + Broadway ramp to Greeley exit ramp. Excluded $1-84$ to Weidler and Broadway to $1-405$ ramp to ramp volumes because they can use their respective nested and would not need to use the full aux. lane between Greeley and Morrison
I-5 NB Aux. Lane from I-84 entrance ramp to Greeley Ave exit ramp - 2045 AM Peak Hour Volumes

|  | Upstream freeway volume to: | Weidler exit ramp | $1-405$ exit ramp | Greeley exit ramp |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{FR}}=$ | 2,390 | 1020 | 750 | 620 |
|  |  | I-84 entrance ramp to freeway north of Greeley exit ramp | Broadway entrance ramp to freeway north of Greeley exit ramp |  |
| $\mathrm{V}_{\mathrm{gF}}=$ | 935 | 595 | 340 |  |
| $\mathrm{V}_{\mathrm{FF}}=940$ |  |  |  |  |
|  |  | $1-84$ entrance ramp to $1-405$ exit ramp | I-84 entrance ramp to Greeley exit ramp | Broadway entrance ramp to Greeley exit ramp |
| $\mathrm{V}_{\mathrm{RR}}=$ | 1,420 | 805 | 395 | 220 |



$\mathrm{VR}=\frac{\left(v_{F R}+v_{R F}\right)}{\left(v_{F F}+v_{F R}+v_{R F}+v_{R R}\right)}$
$V_{\text {RR }}$ Freeway to exit ramp flow
$V_{\text {ER }}$ Entrance ramp to freeway flow
$V_{\mathrm{FR}}$ Freeway through flow
$V_{\text {FR }}$ Entrance ramp to exit ramp flow (optional)



|  | Upstream freeway volume to: | Broadway exit ramp | $1-84$ exit ramp | Morrison exit ramp |
| :---: | :---: | :---: | :---: | :---: |
| $v_{\text {fR }}=$ | 1,760 | 435 | 765 | 560 |
|  |  | Greeley entrance ramp to freeway south of Morrison | I-405 entrance ramp to freeway south of Morrison | Wheeler entrance ramp to freeway south of Morrison |
| $\mathrm{v}_{\mathrm{ff}}=$ | 1,205 | 320 | 465 | 420 |


|  |  | Greeley entrance ramp to Broadway exit ramp | Greeley entrance ramp to $1-84$ exit ramp | Greeley entrance ramp to Morrison exit ramp | $1-405$ entrance ramp to -84 exit ramp | I-405 entrance ramp to Morrison exit ramp | $\begin{aligned} & \text { Wheeler to } \\ & \text { Morrison exit } \\ & \text { ramp } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{RR}}=$ | 1,535 | 195 | 150 | 200 | 425 | 295 | 270 |
| $\mathrm{v}_{\text {fr }}$ | $\mathrm{V}_{\mathrm{RF}}$ | $\mathrm{V}_{\text {FF }}$ | $\mathrm{V}_{\text {RR }}$ | VR | Maximum (Operational) Weaving Length (miles) | Weaving section distance (miles) | Is it a through lane? |
| 1,760 | 1,205 | 870 | 1,535 | 0.55 | 1.60 | 1.42 | No |



|  |  | Greeley entrance ramp to Broadway exit ramp |  | Greeley entrance ramp to 1-84 exit ramp | Greeley entrance ramp to Morrison exit ramp | 1-405 entrancer |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {VR }}=$ | 1,630 | 195 |  | 125 | 170 |  |
| ver | $\mathrm{v}_{\mathrm{RF}}$ | $\mathrm{V}_{\text {FF }}$ |  | $\mathrm{V}_{\text {Rr }}$ | VR | Maximum ( $\mathrm{O}_{\text {P }}$ |
| 1,690 | 985 | 585 |  | 1,630 | 0.55 |  |
| $\mathrm{V}_{\mathrm{fF}}$ |  | $\mathrm{VR}=\frac{\left(v_{F R}+v_{R F}\right)}{\left(v_{F F}+v_{F R}+v_{R F}+v_{R R}\right)}$ |  | Exhibit 10A-2: Maximum (Operational) Weaving Length (mi) ${ }^{2}$ |  |  |
|  |  | vR | Single lane entrance/ exit ramps 0.7 | Dual lane entrance and/or exit ramp ${ }^{2}$ |  |
|  |  | 0.1 |  | 0.40.6 |  |
|  |  | 0.2 <br> 0.3 <br> 0. | 0.7 0.9 |  |  |
|  |  | $\mathrm{V}_{\text {FR }}$$\mathrm{V}_{\text {FR }}$ Eneeway to extrance ramp ramp flow$\mathrm{V}_{\text {FReeway }}$ Freeway through flow | 0.4 | 1.3 | 0.90.91.2 |  |
|  |  | 0.5 | 1.5 |  |  |  |  |
|  |  | 0.6 | $\frac{\mathrm{n}}{} \mathrm{l}$ length colculations based on HCM 7 th Ed | 1.4 |  |
|  |  | $V_{\text {FR }}$ Freeway through flow |  | ${ }^{1}$ Maximum weaving length calculations based on HCM 7th Edition Equation 13-4 ${ }^{2}$ The dual entrance/exit ramps are full lanes and not widened for ramp metering. ${ }^{\circ}$ Value/obtained from HCM 7th Edition Exhibit 13-11, which is based on Equation 13-4. |  |  |  |
| $\mathrm{V}_{\text {RR }}$ |  |  | $\mathrm{V}_{\text {FR }}$ Entrance ramp to exit ramp flow (optional) |  |  |  |  |  |  |

Appendix D Figure 1-I-5 NB Freeway and Ramp Volume Distributions Obtained from 2045 Build Freeway Vissim Models


Appendix D Figure 2 - I-5 SB Freeway and Ramp Volume Distributions Obtained from 2045 Build Freeway Vissim Models


## Appendix D - Table 3 - Analysis of the nested weaving lanes - 2045 AM Peak Hour Volumes

| Northbound | Sta | 2045 AM Peak Hour Volume | From ramp | To ramp | VR (from HCS files) | Maximum (Operational) Weaving Length | Weaving section distance | Is it a through lane? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 -84 entrance ramp x2 | 38083 | 2,605 | $1-84$ entrance ramp x2* | Weidler exit ramp $\times 2{ }^{*}$ | 0.46 | 1.08 | 0.19 | No |
| 1-5 through |  | 5,935 |  |  |  |  |  |  |
| Weidler exit ramp $\times 2$ | 37058 | 1,830 |  |  |  |  |  |  |
| 1-5 through |  | 4,105 |  |  |  |  |  |  |
| Broadway entrance ramp | 34553 | 710 | Broadway entrance ramp $\times 1{ }^{*}$ | $1-405$ exit ramp x2* | 0.39 | 0.89 | 0.21 | No |
| 1-5 through |  | 4,815 |  |  |  |  |  |  |
| 1-405 exit ramp $\times 2$ | 33523 | 1,705 |  |  |  |  |  |  |
| 1-5 through |  | 3,110 |  |  |  |  |  |  |
| Greeley exit ramp | 32746 | 1,235 |  |  |  |  |  |  |


| Southbound | Sta | 2045 AM Peak Hour Volume | From ramp | To ramp | VR | Max weaving distance | Weaving section distance | Is it a through lane? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Greeley entrance ramp | 32080 | 865 |  |  |  |  |  |  |
| 1-5 through |  | 3,495 |  |  |  |  |  |  |
| 1-405 entrance ramp | 32950 | 1,440 | 1-405 entrance ramp x1* | Broadway exit ramp x2* | 0.36 | 0.86 | 0.34 | No |
| 1-5 through |  | 4,935 |  |  |  |  |  |  |
| Broadway exit ramp x2 | 34669 | 885 |  |  |  |  |  |  |
| 1-5 through |  | 4,050 |  |  |  |  |  |  |
| Wheeler entrance ramp | 37183 | 1,070 | Wheeler entrance ramp x1* | 1-84 exit ramp x1* | 0.40 | 1.30 | 0.20 | No |
| 1-5 through |  | 5,120 |  |  |  |  |  |  |
| 1-84 exit ramp | 38223 | 1,720 |  |  |  |  |  |  |
| $1-5$ through |  | 3,400 |  |  |  |  |  |  |
| Morrison exit ramp | 39485 | 1,325 |  |  |  |  |  |  |

Morrison exit ramp $\qquad$
Nested Weaving Lanes
lenath between the gore points
Volumes are 2045 peak hour volumes, consistent with those used for HCM analysis in the SEA

| Exhibit 10A-2: Maximum (Operational) Weaving Length (mi) ${ }^{1}$ |  |  |
| :---: | :---: | :---: |
| VR | Single lane entrance/ <br> exit ramps | Dual lane entrance and/or exit ramp ${ }^{2}$ |
| 0.1 | 0.7 | 0.4 |
| 0.2 | 0.9 | 0.6 |
| 0.3 | 1.1 | 0.8 |
| 0.4 | 1.3 | 0.9 |
| 0.5 | 1.5 | 1.2 |
| 0.6 | $\mathrm{n} / \mathrm{a}$ | 1.4 |
| 0.7 | 1.6 |  |

Maximum weaving length calculations based on HCM 7th Edition Equation 13-4.
The dual entrancel exit ramps are full anes and not widened for ramp metering.

| Appendix D - Table 4 - Analysis of the nested weaving lanes - 2045 PM Peak Hour Volumes |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Northbound | Sta | 2045 PM Peak Hour Volume | From ramp | To ramp | VR (from HCS files) | Maximum (Operational) Weaving Length | Weaving section distance | Is it a through lane? |
| 1-84 entrance ramp $\times 2$ | 38083 | 2,355 | $1-84$ entrance ramp x2* | Weidler exit ramp x2* | 0.46 | 1.08 | 0.19 | No |
| 1-5 through |  | 5,480 |  |  |  |  |  |  |
| Weidler exit ramp $\times 2$ | 37058 | 1,595 |  |  |  |  |  |  |
| 1-5 through |  | 3,885 |  |  |  |  |  |  |
| \| Broadway entrance ramp | 34553 | 700 | Broadway entrance ramp x1* | 1-405 exit ramp x2* | 0.36 | 0.86 | 0.21 | No |
| 1-5 through |  | 4,585 |  |  |  |  |  |  |
| 1-405 exit ramp $\times 2$ | 33523 | 1,425 |  |  |  |  |  |  |
| 1-5 through |  | 3,160 |  |  |  |  |  |  |
| Greeley exit ramp | 32746 | 855 |  |  |  |  |  |  |


| Southbound | Sta | 2045 PM Peak Hour Volume | From ramp | To ramp | VR | Maximum (Operational) Weaving Length | Weaving section distance | Is it a through lane? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Greeley entrance ramp | 32080 | 700 |  |  |  |  |  |  |
| 1-5 through |  | 2,975 |  |  |  |  |  |  |
| 1-405 entrance ramp | 32950 | 1,585 | 1-405 entrance ramp x1* | Broadway exit ramp x2* | 0.42 | 0.96 | 0.34 | No |
| $1-5$ through |  | 4,560 |  |  |  |  |  |  |
| Broadway exit ramp x2 | 34669 | 1,130 |  |  |  |  |  |  |
| 1-5 through |  | 3,430 |  |  |  |  |  |  |
| Wheeler entrance ramp | 37183 | 980 | Wheeler entrance ramp x1* | $1-84$ exit ramp $\mathbf{1}^{*}$ | 0.41 | 1.32 | 0.20 | No |
| 1-5 through |  | 4,410 |  |  |  |  |  |  |
| $1-84$ exit ramp | 38223 | 1,530 |  |  |  |  |  |  |
| 1-5 through |  | 2,880 |  |  |  |  |  |  |
| Morrison exit ramp | 39485 | 1,310 |  |  |  |  |  |  |

Nested Weaving Lanes
gore point
*olumes are 2045 peak hour volumes, consistent with those used for HCM analysis in the SEA

| Exhibit 10A-2: Maximum (Operational) Weaving Length (mi) $^{1}$ |  |  |
| :---: | :---: | :---: |
| VR | Single lane entrance/ <br> exit ramps | Dual lane entrance and/or exit ramp ${ }^{2}$ |
| 0.1 | 0.7 | 0.4 |
| 0.2 | 0.9 | 0.6 |
| 0.3 | 1.1 | 0.8 |
| 0.4 | 1.3 | 0.9 |
| 0.5 | 1.5 | 1.2 |
| 0.6 | $\mathrm{n} / \mathrm{a}$ | 1.4 |
| 0.7 |  | 1.6 |

${ }^{2}$ The dual entrance/exit ramps are full lanes and not widened for ramp metering.
${ }^{\text {a }}$ Value obtained from HCM 7th Edition Exhibit 13-11, which is based on Equation 13-4

QUARTER

## Appendix E: Synchro Model Intersection Results - 2045 AM and PM Peak Hour No Build

|  | $\mathrm{E}-1$ | IMPROVEMENT PROJECT |
| :--- | :--- | :--- | :--- |



c Critical Lane Group

|  | $\dagger$ |  |  |  | 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBT | SBT | SER | SER2 |  |  |
| Lane Configurations | \％ | ¢ $\uparrow$ | 个4 | 「「「 | 「 |  |  |
| Trafic Volume（vph） | 505 | 750 | 255 | 855 | 310 |  |  |
| Future Volume（vph） | 505 | 750 | 255 | 855 | 310 |  |  |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Total Lost time（s） | 4.0 | 4.0 | 3.5 | 4.5 | 4.9 |  |  |
| Lane Util．Factor | ＊0．52 | ＊0．52 | 0.95 | ＊0．95 | 1.00 |  |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Flpb，ped／bikes | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Frt | 1.00 | 1.00 | 1.00 | 1.00 | 0.85 |  |  |
| Flt Protected | 0.95 | 0.99 | 1.00 | 1.00 | 1.00 |  |  |
| Satd．Flow（prot） | 881 | 1825 | 3406 | 3406 | 1524 |  |  |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 1.00 | 1.00 |  |  |
| Satd．Flow（perm） | 881 | 1825 | 3406 | 3406 | 1524 |  |  |
| Peak－hour factor，PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Adj．Flow（vph） | 532 | 789 | 268 | 900 | 326 |  |  |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 |  |  |
| Lane Group Flow（vph） | 335 | 986 | 268 | 900 | 326 |  |  |
| Confl．Peds．（\＃／hr） | 6 |  |  |  |  |  |  |
| Bus Blockages（\＃／hr） | 0 | 5 | 0 | 0 | 0 |  |  |
| Turn Type | Perm | NA | NA | Prot | Perm |  |  |
| Protected Phases |  | 6 | 4 | 3 |  |  |  |
| Permitted Phases | 6 |  |  |  | 3 |  |  |
| Actuated Green，G（s） | 27.7 | 27.7 | 9.2 | 19.1 | 19.1 |  |  |
| Effective Green， $\mathrm{g}(\mathrm{s})$ | 28.4 | 28.4 | 10.1 | 19.5 | 19.1 |  |  |
| Actuated g／C Ratio | 0.41 | 0.41 | 0.14 | 0.28 | 0.27 |  |  |
| Clearance Time（s） | 4.7 | 4.7 | 4.4 | 4.9 | 4.9 |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |  |
| Lane Grp Cap（vph） | 357 | 740 | 491 | 948 | 415 |  |  |
| v／s Ratio Prot |  |  | c0．08 | c0．26 |  |  |  |
| v／s Ratio Perm | 0.38 | 0.54 |  |  | 0.21 |  |  |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.94 | 1.33 | 0.55 | 0.95 | 0.79 |  |  |
| Uniform Delay，d1 | 20.0 | 20.8 | 27.8 | 24.8 | 23.6 |  |  |
| Progression Factor | 0.54 | 0.58 | 1.00 | 1.00 | 1.00 |  |  |
| Incremental Delay，d2 | 29.4 | 156.9 | 1.2 | 18.0 | 9.4 |  |  |
| Delay（s） | 40.2 | 168.9 | 29.1 | 42.8 | 33.0 |  |  |
| Level of Service | D | F | C | D | C |  |  |
| Approach Delay（s） |  | 136.3 | 29.1 |  |  |  |  |
| Approach LOS |  | F | C |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 84.2 |  | HCM 2000 Level of Service | F |  |
| HCM 2000 Volume to Capacity ratio |  |  | 1.07 |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 70.0 |  | Sum of lost time（s） | 12.0 |  |
| Intersection Capacity Utilization |  |  | 71．0\％ |  | CU Level of Service | C |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |

C Critical Lane Group


|  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | ---: |

c Critical Lane Group


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|  | $\stackrel{ }{ }$ |  |  | 7 |  | 4 | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | \$ |  |  |  |  |
| Traffic Volume (veh/h) | 10 | 10 | 0 | 0 | 0 | 180 | 10 | 455 | 10 | 0 | 0 | 0 |
| Future Volume (Veh/h) | 10 | 10 | 0 | 0 | 0 | 180 | 10 | 455 | 10 | 0 | 0 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 11 | 11 | 0 | 0 | 0 | 189 | 11 | 479 | 11 | 0 | 0 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  | 498 |  |  |  |  |
| pX, platoon unblocked | 0.99 | 0.99 |  | 0.99 | 0.99 | 0.99 |  |  |  | 0.99 |  |  |
| vC , conflicting volume | 696 | 512 | 0 | 512 | 506 | 484 | 0 |  |  | 490 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 687 | 501 | 0 | 501 | 496 | 473 | 0 |  |  | 479 |  |  |
| tC , single (s) | 7.2 | 6.6 | 6.3 | 7.2 | 6.6 | 6.3 | 4.2 |  |  | 4.2 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.6 | 4.1 | 3.4 | 3.6 | 4.1 | 3.4 | 2.3 |  |  | 2.3 |  |  |
| p0 queue free \% | 95 | 98 | 100 | 100 | 100 | 67 | 99 |  |  | 100 |  |  |
| cM capacity (veh/h) | 235 | 458 | 1073 | 458 | 461 | 576 | 1597 |  |  | 1051 |  |  |
| Direction, Lane\# | EB 1 | WB 1 | NB 1 |  |  |  |  |  |  |  |  |  |
| Volume Total | 22 | 189 | 501 |  |  |  |  |  |  |  |  |  |
| Volume Left | 11 | 0 | 11 |  |  |  |  |  |  |  |  |  |
| Volume Right | 0 | 189 | 11 |  |  |  |  |  |  |  |  |  |
| cSH | 311 | 576 | 1597 |  |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.07 | 0.33 | 0.01 |  |  |  |  |  |  |  |  |  |
| Queue Length 95th (ft) | 6 | 36 | 1 |  |  |  |  |  |  |  |  |  |
| Control Delay (s) | 17.5 | 14.3 | 0.2 |  |  |  |  |  |  |  |  |  |
| Lane LOS | C | B | A |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 17.5 | 14.3 | 0.2 |  |  |  |  |  |  |  |  |  |
| Approach LOS | C | B |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 4.5 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 42.9\% |  | Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |



C Critical Lane Group


C Critical Lane Group


c Critical Lane Group

|  | 7 |  |  |  | $\pm$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBT | SBT | SER | SER2 |  |  |
| Lane Configurations | \％ | $\uparrow \uparrow$ | 个个 | 「「「 | 「 |  |  |
| Traffic Volume（vph） | 405 | 515 | 355 | 930 | 410 |  |  |
| Future Volume（vph） | 405 | 515 | 355 | 930 | 410 |  |  |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Total Lost time（s） | 4.0 | 4.0 | 3.5 | 4.5 | 4.9 |  |  |
| Lane Util．Factor | ＊0．52 | ＊0．52 | 0.95 | ＊0．95 | 1.00 |  |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Flpb，ped／bikes | 0.98 | 0.99 | 1.00 | 1.00 | 1.00 |  |  |
| Frt | 1.00 | 1.00 | 1.00 | 1.00 | 0.85 |  |  |
| Flt Protected | 0.95 | 0.99 | 1.00 | 1.00 | 1.00 |  |  |
| Satd．Flow（prot） | 890 | 1868 | 3505 | 3505 | 1568 |  |  |
| Flt Permitted | 0.95 | 0.99 | 1.00 | 1.00 | 1.00 |  |  |
| Satd．Flow（perm） | 890 | 1868 | 3505 | 3505 | 1568 |  |  |
| Peak－hour factor，PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |  |  |
| Adj．Flow（vph） | 426 | 542 | 374 | 979 | 432 |  |  |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 |  |  |
| Lane Group Flow（vph） | 268 | 700 | 374 | 979 | 432 |  |  |
| Confl．Peds．（\＃hr） | 26 |  |  |  |  |  |  |
| Bus Blockages（\＃／hr） | 0 | 5 | 0 | 0 | 0 |  |  |
| Turn Type | Perm | NA | NA | Prot | Perm |  |  |
| Protected Phases |  | 6 | 4 | 3 |  |  |  |
| Permitted Phases | 6 |  |  |  | 3 |  |  |
| Actuated Green，G（s） | 27.3 | 27.3 | 9.6 | 19.1 | 19.1 |  |  |
| Effective Green， g （s） | 28.0 | 28.0 | 10.5 | 19.5 | 19.1 |  |  |
| Actuated g／C Ratio | 0.40 | 0.40 | 0.15 | 0.28 | 0.27 |  |  |
| Clearance Time（s） | 4.7 | 4.7 | 4.4 | 4.9 | 4.9 |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |  |
| Lane Grp Cap（vph） | 356 | 747 | 525 | 976 | 427 |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  | c0．11 | c0． 28 |  |  |  |
| v／s Ratio Perm | 0.30 | 0.37 |  |  | 0.28 |  |  |
| v／c Ratio | 0.75 | 0.94 | 0.71 | 1.00 | 1.01 |  |  |
| Uniform Delay，d1 | 18.0 | 20.2 | 28.3 | 25.2 | 25.4 |  |  |
| Progression Factor | 0.32 | 0.35 | 1.00 | 1.00 | 1.00 |  |  |
| Incremental Delay，d2 | 12.6 | 19.4 | 8.0 | 29.6 | 46.5 |  |  |
| Delay（s） | 18.3 | 26.4 | 36.3 | 54.8 | 72.0 |  |  |
| Level of Service | B | C | D | D | E |  |  |
| Approach Delay（s） |  | 24.2 | 36.3 |  |  |  |  |
| Approach LOS |  | C | D |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 44.2 |  | HCM 2000 Level of Service | D |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.92 |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 70.0 |  | Sum of lost time（s） | 12.0 |  |
| Intersection Capacity Utilization |  |  | 70．1\％ |  | ICU Level of Service | C |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |




C Critical Lane Group

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C Critical Lane Group

|  | $\stackrel{ }{ }$ |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |  |  |
| Traffic Volume (veh/h) | 5 | 0 | 0 | 0 | - | 95 | 5 | 620 | 25 | 0 | 0 | 0 |
| Future Volume (Veh/h) | 5 | 0 | 0 | 0 | 0 | 95 | 5 | 620 | 25 | 0 | 0 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 5 | 0 | 0 | 0 | 0 | 100 | 5 | 653 | 26 | 0 | 0 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  | 498 |  |  |  |  |
| pX, platoon unblocked | 0.88 | 0.88 |  | 0.88 | 0.88 | 0.88 |  |  |  | 0.88 |  |  |
| vC , conflicting volume | 776 | 689 | 0 | 676 | 676 | 666 | 0 |  |  | 679 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 682 | 583 | 0 | 569 | 569 | 557 | 0 |  |  | 572 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 98 | 100 | 100 | 100 | 100 | 79 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 252 | 373 | 1082 | 381 | 380 | 467 | 1617 |  |  | 881 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 |  |  |  |  |  |  |  |  |  |
| Volume Total | 5 | 100 | 684 |  |  |  |  |  |  |  |  |  |
| Volume Left | 5 | 0 | 5 |  |  |  |  |  |  |  |  |  |
| Volume Right | 0 | 100 | 26 |  |  |  |  |  |  |  |  |  |
| cSH | 252 | 467 | 1617 |  |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.02 | 0.21 | 0.00 |  |  |  |  |  |  |  |  |  |
| Queue Length 95th (ft) | 2 | 20 | 0 |  |  |  |  |  |  |  |  |  |
| Control Delay (s) | 19.6 | 14.8 | 0.1 |  |  |  |  |  |  |  |  |  |
| Lane LOS | C | B | A |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 19.6 | 14.8 | 0.1 |  |  |  |  |  |  |  |  |  |
| Approach LOS | C | B |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 47.0\% |  | U Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


c Critical Lane Group


C Critical Lane Group

## Synchro Model Intersection Results - 2045 AM and PM Peak Hour Revised Build



c Critical Lane Group

|  | 4 | $\rightarrow$ |  | $\checkmark$ |  | 4 | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  | ${ }^{7} 1$ | 44 |  |  |  |  |  | 4 | 「 |
| Traffic Volume (vph) | 0 | 0 | 0 | 575 | 970 | 0 | 0 | 0 | 0 | 0 | 300 | 45 |
| Future Volume (vph) | 0 | 0 | 0 | 575 | 970 | 0 | 0 | 0 | 0 | 0 | 300 | 45 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  |  |  | 4.0 | 4.0 |  |  |  |  |  | 4.0 | 4.0 |
| Lane Util. Factor |  |  |  | 0.97 | 0.95 |  |  |  |  |  | 1.00 | 1.00 |
| Frt |  |  |  | 1.00 | 1.00 |  |  |  |  |  | 1.00 | 0.85 |
| Flt Protected |  |  |  | 0.95 | 1.00 |  |  |  |  |  | 1.00 | 1.00 |
| Satd. Flow (prot) |  |  |  | 3303 | 3372 |  |  |  |  |  | 1792 | 1524 |
| Flt Permitted |  |  |  | 0.95 | 1.00 |  |  |  |  |  | 1.00 | 1.00 |
| Satd. Flow (perm) |  |  |  | 3303 | 3372 |  |  |  |  |  | 1792 | 1524 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 605 | 1021 | 0 | 0 | 0 | 0 | 0 | 316 | 47 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 605 | 1021 | 0 | 0 | 0 | 0 | 0 | 316 | 47 |
| Bus Blockages (\#/hr) |  | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type |  | Prot |  |  | NA |  |  |  |  |  | NA | custom |
| Protected Phases |  |  |  | 6 | 2 |  |  |  |  |  | 4 | 8 |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Green, G (s) |  |  |  | 33.7 | 40.5 |  |  |  |  |  | 20.5 | 4.5 |
| Effective Green, g (s) |  |  |  | 34.2 | 41.0 |  |  |  |  |  | 21.0 | 5.0 |
| Actuated g/C Ratio |  |  |  | 0.49 | 0.59 |  |  |  |  |  | 0.30 | 0.07 |
| Clearance Time (s) |  |  |  | 4.5 | 4.5 |  |  |  |  |  | 4.5 | 4.5 |
| Vehicle Extension (s) |  |  |  | 3.0 | 3.0 |  |  |  |  |  | 3.0 | 3.0 |
| Lane Grp Cap (vph) v/s Ratio Prot |  |  |  | 1613 | 1975 |  |  |  |  |  | 537 | 108 |
|  |  |  |  | 0.18 | c0.30 |  |  |  |  |  | c0.18 | 0.03 |
| v/s Ratio Perm |  |  |  |  |  |  |  |  |  |  |  |  |
| v/c Ratio |  |  |  | 0.38 | 0.52 |  |  |  |  |  | 0.59 | 0.44 |
| Uniform Delay, d1 |  |  |  | 11.2 | 8.6 |  |  |  |  |  | 20.8 | 31.1 |
| Progression Factor |  |  |  | 1.49 | 1.76 |  |  |  |  |  | 1.00 | 1.00 |
| Incremental Delay, d2 |  |  |  | 0.6 | 0.8 |  |  |  |  |  | 1.7 | 2.8 |
| Delay (s) |  |  |  | 17.3 | 15.9 |  |  |  |  |  | 22.5 | 33.9 |
| Level of Service |  |  |  | B | B |  |  |  |  |  | C | C |
| Approach Delay (s) |  | 0.0 |  |  | 16.4 |  |  | 0.0 |  |  | 24.0 |  |
| Approach LOS |  | A |  |  | B |  |  | A |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 17.8 |  | HCM 2000 | Level of | ervice |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.62 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 70.0 |  | Sum of los | time (s) |  |  | 15.5 |  |  |  |
| Intersection Capacity Utilization |  |  | 49.3\% |  | ICU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |



c Critical Lane Group


Analysis Period (min)
15
C Critical Lane Group

c Critical Lane Group



c Critical Lane Group

|  | 4 | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |  |  |
| Traffic Volume (vph) | 10 | 0 | 0 | 0 | 60 | 125 | 0 | 380 | 10 | 0 | 0 | 0 |
| Future Volume (vph) | 10 | 0 | 0 | 0 | 60 | 125 | 0 | 380 | 10 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |  |  |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Frt |  | 1.00 |  |  | 0.91 |  |  | 1.00 |  |  |  |  |
| Flt Protected |  | 0.95 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Satd. Flow (prot) |  | 1703 |  |  | 1629 |  |  | 1786 |  |  |  |  |
| Flt Permitted |  | 0.51 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Satd. Flow (perm) |  | 916 |  |  | 1629 |  |  | 1786 |  |  |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 11 | 0 | 0 | 0 | 63 | 132 | 0 | 400 | 11 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 11 | 0 | 0 | 195 | 0 | 0 | 411 | 0 | 0 | 0 | 0 |
| Turn Type | Perm | NA |  |  | NA |  |  | NA |  |  |  |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  |  |  |
| Permitted Phases | 2 |  |  |  |  |  | 4 |  |  |  |  |  |
| Actuated Green, G (s) |  | 13.7 |  |  | 13.7 |  |  | 29.6 |  |  |  |  |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 14.2 |  |  | 14.2 |  |  | 30.1 |  |  |  |  |
| Actuated g/C Ratio |  | 0.20 |  |  | 0.20 |  |  | 0.43 |  |  |  |  |
| Clearance Time (s) |  | 4.5 |  |  | 4.5 |  |  | 4.5 |  |  |  |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  |  | 3.0 |  |  |  |  |
| Lane Grp Cap (vph) |  | 185 |  |  | 330 |  |  | 767 |  |  |  |  |
| v/s Ratio Prot |  |  |  |  | c0.12 |  |  | c0.23 |  |  |  |  |
| v/s Ratio Perm |  | 0.01 |  |  |  |  |  |  |  |  |  |  |
| v/c Ratio |  | 0.06 |  |  | 0.59 |  |  | 0.54 |  |  |  |  |
| Uniform Delay, d1 |  | 22.5 |  |  | 25.3 |  |  | 14.8 |  |  |  |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 0.77 |  |  |  |  |
| Incremental Delay, d2 |  | 0.1 |  |  | 2.8 |  |  | 0.2 |  |  |  |  |
| Delay (s) |  | 22.6 |  |  | 28.1 |  |  | 11.6 |  |  |  |  |
| Level of Service |  | C |  |  | C |  |  | B |  |  |  |  |
| Approach Delay (s) |  | 22.6 |  |  | 28.1 |  |  | 11.6 |  |  | 0.0 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 17.0 |  | HCM 2000 | Level of S | ervice |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.43 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 70.0 |  | Sum of lost | time (s) |  |  | 12.5 |  |  |  |
| Intersection Capacity Utilization |  |  | 38.1\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group



| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 59.5 | HCM 2000 Level of Service | E |
| HCM 2000 Volume to Capacity ratio | 0.78 |  | 26.0 |
| Actuated Cycle Length (s) | 90.7 | Sum of lost time (s) | C |
| Intersection Capacity Utilization | $66.0 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |


c Critical Lane Group


c Critical Lane Group




C Critical Lane Group

c Critical Lane Group




|  | $\rangle$ |  |  | $\dagger$ |  |  | 4 | $\dagger$ | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | А中解 |  |  |  |  |  | F |  |  | $\uparrow$ |  |
| Traffic Volume (vph) | 140 | 1715 | 165 | 0 | 0 | 0 | 0 | 30 | 15 | 15 | 20 | 0 |
| Future Volume (vph) | 140 | 1715 | 165 | 0 | 0 | 0 | 0 | 30 | 15 | 15 | 20 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  |  |  |  | 4.0 |  |  | 4.0 |  |
| Lane Util. Factor |  | 0.91 |  |  |  |  |  | 1.00 |  |  | 1.00 |  |
| Frpb, ped/bikes |  | 0.99 |  |  |  |  |  | 0.99 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  |  |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.99 |  |  |  |  |  | 0.95 |  |  | 1.00 |  |
| Flt Protected |  | 1.00 |  |  |  |  |  | 1.00 |  |  | 0.98 |  |
| Satd. Flow (prot) |  | 4881 |  |  |  |  |  | 1751 |  |  | 1801 |  |
| Flt Permitted |  | 1.00 |  |  |  |  |  | 1.00 |  |  | 0.84 |  |
| Satd. Flow (perm) |  | 4881 |  |  |  |  |  | 1751 |  |  | 1541 |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 147 | 1805 | 174 | 0 | 0 | 0 | 0 | 32 | 16 | 16 | 21 | 0 |
| RTOR Reduction (vph) | 0 | 8 | 0 | 0 | 0 | 0 | 0 | , | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 2118 | 0 | 0 | 0 | 0 | 0 | 39 | 0 | 0 | 37 | 0 |
| Confl. Peds. (\#/hr) | 58 |  | 152 |  |  |  |  |  | 2 | 2 |  |  |
| Confl. Bikes (\#/hr) |  |  | 100 |  |  |  |  |  |  |  |  |  |
| Turn Type | Perm | NA |  |  |  |  |  | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  |  |  |  | 4 |  |  | 4 |  |
| Permitted Phases | 2 |  |  |  |  |  |  |  |  | 4 |  |  |
| Actuated Green, G (s) |  | 55.0 |  |  |  |  |  | 6.0 |  |  | 6.0 |  |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 55.5 |  |  |  |  |  | 6.5 |  |  | 6.5 |  |
| Actuated g/C Ratio |  | 0.79 |  |  |  |  |  | 0.09 |  |  | 0.09 |  |
| Clearance Time (s) |  | 4.5 |  |  |  |  |  | 4.5 |  |  | 4.5 |  |
| Vehicle Extension (s) |  | 0.5 |  |  |  |  |  | 0.5 |  |  | 0.5 |  |
| Lane Grp Cap (vph) |  | 3869 |  |  |  |  |  | 162 |  |  | 143 |  |
| v/s Ratio Prot |  |  |  |  |  |  |  | 0.02 |  |  |  |  |
| v/s Ratio Perm |  | 0.43 |  |  |  |  |  |  |  |  | c0.02 |  |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.55 |  |  |  |  |  | 0.24 |  |  | 0.26 |  |
| Uniform Delay, d1 |  | 2.7 |  |  |  |  |  | 29.5 |  |  | 29.5 |  |
| Progression Factor |  | 0.87 |  |  |  |  |  | 1.00 |  |  | 1.02 |  |
| Incremental Delay, d2 |  | 0.4 |  |  |  |  |  | 0.3 |  |  | 0.3 |  |
| Delay (s) |  | 2.7 |  |  |  |  |  | 29.7 |  |  | 30.5 |  |
| Level of Service |  | A |  |  |  |  |  | C |  |  | C |  |
| Approach Delay (s) |  | 2.7 |  |  | 0.0 |  |  | 29.7 |  |  | 30.5 |  |
| Approach LOS |  | A |  |  | A |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  | 3.8 |  | HCM 2000 Level of Service |  |  |  |  | A |  |  |  |
| HCM 2000 Volume to Capacity ratio |  | 0.52 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  | 70.0 |  | Sum of lost time (s) |  |  |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  | 55.4\% |  | ICU Level of Service |  |  |  |  | B |  |  |  |
| Analysis Period (min) |  | 15 |  |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

|  | 4 |  |  | 7 |  |  | 4 | $\dagger$ | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |  |  |
| Traffic Volume (vph) | 10 | 0 | 0 | 0 | 50 | 75 | 5 | 485 | 20 | 0 | 0 | 0 |
| Future Volume (vph) | 10 | 0 | 0 | 0 | 50 | 75 | 5 | 485 | 20 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |  |  |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Frt |  | 1.00 |  |  | 0.92 |  |  | 0.99 |  |  |  |  |
| Flt Protected |  | 0.95 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Satd. Flow (prot) |  | 1752 |  |  | 1696 |  |  | 1834 |  |  |  |  |
| Flt Permitted |  | 0.58 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Satd. Flow (perm) |  | 1069 |  |  | 1696 |  |  | 1834 |  |  |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 11 | 0 | 0 | 0 | 53 | 79 | 5 | 511 | 21 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 11 | 0 | 0 | 132 | 0 | 0 | 537 | 0 | 0 | 0 | 0 |
| Turn Type | Perm | NA |  |  | NA |  | Perm | NA |  |  |  |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  |  |  |
| Permitted Phases | 2 |  |  |  |  |  | 4 |  |  |  |  |  |
| Actuated Green, G (s) |  | 6.4 |  |  | 6.4 |  |  | 23.0 |  |  |  |  |
| Effective Green, g (s) |  | 6.9 |  |  | 6.9 |  |  | 23.5 |  |  |  |  |
| Actuated g/C Ratio |  | 0.10 |  |  | 0.10 |  |  | 0.34 |  |  |  |  |
| Clearance Time (s) |  | 4.5 |  |  | 4.5 |  |  | 4.5 |  |  |  |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  |  | 3.0 |  |  |  |  |
| Lane Grp Cap (vph) |  | 105 |  |  | 167 |  |  | 615 |  |  |  |  |
| v/s Ratio Prot |  |  |  |  | c0.08 |  |  |  |  |  |  |  |
| v/s Ratio Perm |  | 0.01 |  |  |  |  |  | 0.29 |  |  |  |  |
| v/c Ratio |  | 0.10 |  |  | 0.79 |  |  | 0.87 |  |  |  |  |
| Uniform Delay, d1 |  | 28.7 |  |  | 30.8 |  |  | 21.8 |  |  |  |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 0.63 |  |  |  |  |
| Incremental Delay, d2 |  | 0.4 |  |  | 22.0 |  |  | 7.5 |  |  |  |  |
| Delay (s) |  | 29.2 |  |  | 52.8 |  |  | 21.3 |  |  |  |  |
| Level of Service |  | C |  |  | D |  |  | C |  |  |  |  |
| Approach Delay (s) |  | 29.2 |  |  | 52.8 |  |  | 21.3 |  |  | 0.0 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 27.5 |  | HCM 2000 | Level of S | ervice |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.45 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 70.0 |  | Sum of lost | time (s) |  |  | 12.5 |  |  |  |
| Intersection Capacity Utilization |  |  | 42.0\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group



c Critical Lane Group


c Critical Lane Group

|  | 4 |  |  | 7 |  | 4 | 4 | $\dagger$ | $p$ |  | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  | ${ }^{7} 1$ | 中4 |  | \% |  |  |  | 4 |  |
| Traffic Volume (vph) | 0 | 0 | 0 | 605 | 970 | 0 | 180 | 0 | 0 | 0 | 300 | 0 |
| Future Volume (vph) | 0 | 0 | 0 | 605 | 970 | 0 | 180 | 0 | 0 | 0 | 300 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  |  |  | 4.0 | 4.0 |  | 4.0 |  |  |  | 4.0 |  |
| Lane Util. Factor |  |  |  | 0.97 | 0.95 |  | 1.00 |  |  |  | 1.00 |  |
| Frt |  |  |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  |
| Flt Protected |  |  |  | 0.95 | 1.00 |  | 0.95 |  |  |  | 1.00 |  |
| Satd. Flow (prot) |  |  |  | 3303 | 3372 |  | 1703 |  |  |  | 1792 |  |
| Fit Permitted |  |  |  | 0.95 | 1.00 |  | 0.95 |  |  |  | 1.00 |  |
| Satd. Flow (perm) |  |  |  | 3303 | 3372 |  | 1703 |  |  |  | 1792 |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 637 | 1021 | 0 | 189 | 0 | 0 | 0 | 316 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 637 | 1021 | 0 | 189 | 0 | 0 | 0 | 316 | 0 |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  |  |  | Prot | NA |  | Prot |  |  |  | NA |  |
| Turn Type <br> Protected Phases |  |  |  | 6 | 2 |  | 3 |  |  |  | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Green, G (s) |  |  |  | 26.7 | 33.5 |  | 10.8 |  |  |  | 12.2 |  |
| Effective Green, g (s) |  |  |  | 27.2 | 34.0 |  | 11.3 |  |  |  | 12.7 |  |
| Actuated g/C Ratio |  |  |  | 0.39 | 0.49 |  | 0.16 |  |  |  | 0.18 |  |
| Clearance Time (s) |  |  |  | 4.5 | 4.5 |  | 4.5 |  |  |  | 4.5 |  |
| Vehicle Extension (s) |  |  |  | 3.0 | 3.0 |  | 3.0 |  |  |  | 3.0 |  |
| Lane Grp Cap (vph) |  |  |  | 1283 | 1637 |  | 274 |  |  |  | 325 |  |
| Lane Grp Cap (vph) v/s Ratio Prot |  |  |  | 0.19 | c0.30 |  | c0.11 |  |  |  | c0.18 |  |
| v/s Ratio Perm |  |  |  |  |  |  |  |  |  |  |  |  |
| v/c Ratio |  |  |  | 0.50 | 0.62 |  | 0.69 |  |  |  | 0.97 |  |
| Uniform Delay, d1 |  |  |  | 16.2 | 13.3 |  | 27.7 |  |  |  | 28.5 |  |
| Progression Factor |  |  |  | 1.34 | 1.40 |  | 1.89 |  |  |  | 1.00 |  |
| Incremental Delay, d2 |  |  |  | 1.1 | 1.5 |  | 6.5 |  |  |  | 42.2 |  |
| Delay (s) |  |  |  | 22.9 | 20.0 |  | 58.9 |  |  |  | 70.7 |  |
| Level of Service |  |  |  | C | C |  | E |  |  |  | E |  |
| Approach Delay (s) 0.0 |  |  |  |  | 21.1 |  |  | 58.9 |  |  | 70.7 |  |
| Approach LOS |  | A |  | C |  |  |  | E |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 31.7 | HCM 2000 Level of Service |  |  |  |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.76 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 70.0 |  | Sum of los | ime (s) |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 62.6\% |  | CU Level | Service |  |  | B |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |




C Critical Lane Group


C Critical Lane Group

|  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



C Critical Lane Group


c Critical Lane Group

|  | 4 | $\rightarrow$ |  | 7 |  |  | 4 | $\dagger$ | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |  |  |
| Traffic Volume (vph) | 10 | 0 | 0 | 0 | 60 | 125 | 0 | 385 | 10 | 0 | 0 | 0 |
| Future Volume (vph) | 10 | 0 | 0 | 0 | 60 | 125 | 0 | 385 | 10 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |  |  |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Frt |  | 1.00 |  |  | 0.91 |  |  | 1.00 |  |  |  |  |
| Flt Protected |  | 0.95 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Satd. Flow (prot) |  | 1703 |  |  | 1629 |  |  | 1786 |  |  |  |  |
| Flt Permitted |  | 0.51 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Satd. Flow (perm) |  | 916 |  |  | 1629 |  |  | 1786 |  |  |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 11 | 0 | 0 | 0 | 63 | 132 | 0 | 405 | 11 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 11 | 0 | 0 | 195 | 0 | 0 | 416 | 0 | 0 | 0 | 0 |
| Turn Type | Perm | NA |  |  | NA |  |  | NA |  |  |  |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  |  |  |
| Permitted Phases | 2 |  |  |  |  |  | 4 |  |  |  |  |  |
| Actuated Green, G (s) |  | 13.7 |  |  | 13.7 |  |  | 29.8 |  |  |  |  |
| Effective Green, g (s) |  | 14.2 |  |  | 14.2 |  |  | 30.3 |  |  |  |  |
| Actuated g/C Ratio |  | 0.20 |  |  | 0.20 |  |  | 0.43 |  |  |  |  |
| Clearance Time (s) |  | 4.5 |  |  | 4.5 |  |  | 4.5 |  |  |  |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  |  | 3.0 |  |  |  |  |
| Lane Grp Cap (vph) |  | 185 |  |  | 330 |  |  | 773 |  |  |  |  |
| v/s Ratio Prot |  |  |  |  | c0.12 |  |  | c0.23 |  |  |  |  |
| v/s Ratio Perm |  | 0.01 |  |  |  |  |  |  |  |  |  |  |
| v/c Ratio |  | 0.06 |  |  | 0.59 |  |  | 0.54 |  |  |  |  |
| Uniform Delay, d1 |  | 22.5 |  |  | 25.3 |  |  | 14.7 |  |  |  |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 0.71 |  |  |  |  |
| Incremental Delay, d2 |  | 0.1 |  |  | 2.8 |  |  | 0.2 |  |  |  |  |
| Delay (s) |  | 22.6 |  |  | 28.1 |  |  | 10.7 |  |  |  |  |
| Level of Service |  | C |  |  | C |  |  | B |  |  |  |  |
| Approach Delay (s) |  | 22.6 |  |  | 28.1 |  |  | 10.7 |  |  | 0.0 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 16.3 |  | HCM 2000 | Level of S | ervice |  | B |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.43 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 70.0 |  | Sum of lost | time (s) |  |  | 12.5 |  |  |  |
| Intersection Capacity Utilization |  |  | 38.4\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group


| Movement | EBL | EBR | EBR2 | WBL | WBT | WBR | NBT | SET | SER |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | Tit |  |  | \$ |  | $\uparrow$ | 个4 | F |
| Traffic Volume (vph) | 0 | 80 | 20 | 130 | 0 | 230 | 0 | 995 | 150 |
| Future Volume (vph) | 0 | 80 | 20 | 130 | 0 | 230 | 0 | 995 | 150 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 | 6.0 |
| Lane Util. Factor |  | 0.88 |  |  | 1.00 |  |  | 0.95 | 1.00 |
| Frpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 | 1.00 |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  |  | 1.00 | 1.00 |
| Frt |  | 0.85 |  |  | 0.91 |  |  | 1.00 | 0.85 |
| Flt Protected |  | 1.00 |  |  | 0.98 |  |  | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 2682 |  |  | 1609 |  |  | 3406 | 1524 |
| Flt Permitted |  | 1.00 |  |  | 0.98 |  |  | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 2682 |  |  | 1609 |  |  | 3406 | 1524 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 84 | 21 | 137 | 0 | 242 | 0 | 1047 | 158 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 105 | 0 | 0 | 379 | 0 | 0 | 1047 | 158 |
| Confl. Peds. (\#/hr) |  |  | 10 |  |  |  |  |  |  |
| Turn Type | Prot | Prot |  | Split | NA |  |  | NA | Prot |
| Protected Phases | 4 | 4 |  | 6 | 6 |  | 8 | 5 | 5 |
| Permitted Phases |  |  |  |  |  |  |  |  |  |
| Actuated Green, G (s) |  | 8.9 |  |  | 16.0 |  |  | 34.0 | 34.0 |
| Effective Green, g (s) |  | 8.9 |  |  | 16.0 |  |  | 34.0 | 34.0 |
| Actuated g/C Ratio |  | 0.10 |  |  | 0.18 |  |  | 0.37 | 0.37 |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 |  |  | 1.5 |  |  | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 262 |  |  | 283 |  |  | 1273 | 570 |
| v/s Ratio Prot |  | c0.04 |  |  | c0.24 |  |  | c0.31 | 0.10 |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  |  |  |  |  |  |  |  |  |
| v/c Ratio |  | 0.40 |  |  | 1.34 |  |  | 0.82 | 0.28 |
| Uniform Delay, d1 |  | 38.5 |  |  | 37.5 |  |  | 25.7 | 19.9 |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 1.0 |  |  | 174.6 |  |  | 4.4 | 0.3 |
| Delay (s) |  | 39.5 |  |  | 212.1 |  |  | 30.1 | 20.1 |
| Level of Service |  | D |  |  | F |  |  | C | C |
| Approach Delay (s) |  |  |  |  | 212.1 |  | 0.0 | 28.8 |  |
| Approach LOS |  |  |  |  | F |  | A | C |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 70.6 | HCM 2000 Level of Service | E |
| HCM 2000 Volume to Capacity ratio | 0.82 |  | 26.0 |
| Actuated Cycle Length (s) | 90.9 | Sum of lost time (s) | C |
| Intersection Capacity Utilization | $68.0 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |


c Critical Lane Group


c Critical Lane Group

|  | 4 | $\rightarrow$ | $\cdots$ | 7 |  | 4 | 4 | 4 | $p$ |  | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  |  |  | 17 | 44 |  | ${ }^{7}$ |  |  |  | 4 |  |
| Traffic Volume (vph) | 0 | 0 | 0 | 370 | 605 | 0 | 290 | 0 | 0 | 0 | 220 | 0 |
| Future Volume (vph) | 0 | 0 | 0 | 370 | 605 | 0 | 290 | 0 | 0 | 0 | 220 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  |  |  | 4.0 | 4.0 |  | 4.0 |  |  |  | 4.0 |  |
| Lane Util. Factor |  |  |  | 0.97 | 0.95 |  | 1.00 |  |  |  | 1.00 |  |
| Frt |  |  |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  |
| Flt Protected |  |  |  | 0.95 | 1.00 |  | 0.95 |  |  |  | 1.00 |  |
| Satd. Flow (prot) |  |  |  | 3400 | 3470 |  | 1752 |  |  |  | 1845 |  |
| Flt Permitted |  |  |  | 0.95 | 1.00 |  | 0.95 |  |  |  | 1.00 |  |
| Satd. Flow (perm) |  |  |  | 3400 | 3470 |  | 1752 |  |  |  | 1845 |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 0 | 0 | 0 | 389 | 637 | 0 | 305 | 0 | 0 | 0 | 232 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 0 | 389 | 637 | 0 | 305 | 0 | 0 | 0 | 232 | 0 |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  |  |  | Prot | NA |  | Prot |  |  |  | NA |  |
| Turn Type <br> Protected Phases |  |  |  | 6 | 2 |  | 3 |  |  |  | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Green, G (s) |  |  |  | 22.9 | 33.5 |  | 11.5 |  |  |  | 11.5 |  |
| Effective Green, g (s) |  |  |  | 23.4 | 34.0 |  | 12.0 |  |  |  | 12.0 |  |
| Actuated g/C Ratio |  |  |  | 0.33 | 0.49 |  | 0.17 |  |  |  | 0.17 |  |
| Clearance Time (s) |  |  |  | 4.5 | 4.5 |  | 4.5 |  |  |  | 4.5 |  |
| Vehicle Extension (s) |  |  |  | 3.0 | 3.0 |  | 3.0 |  |  |  | 3.0 |  |
| Lane Grp Cap (vph) |  |  |  | 1136 | 1685 |  | 300 |  |  |  | 316 |  |
| v/s Ratio Prot |  |  |  | 0.11 | c0.18 |  | c0.17 |  |  |  | c0.13 |  |
| v/s Ratio Perm |  |  |  |  |  |  |  |  |  |  |  |  |
| v/c Ratio |  |  |  | 0.34 | 0.38 |  | 1.02 |  |  |  | 0.73 |  |
| Uniform Delay, d1 |  |  |  | 17.5 | 11.3 |  | 29.0 |  |  |  | 27.5 |  |
| Progression Factor |  |  |  | 0.97 | 1.05 |  | 1.43 |  |  |  | 1.00 |  |
| Incremental Delay, d2 |  |  |  | 0.8 | 0.6 |  | 50.3 |  |  |  | 8.5 |  |
| Delay (s) |  |  |  | 17.8 | 12.5 |  | 91.8 |  |  |  | 36.0 |  |
| Level of Service |  |  |  | B | B |  | F |  |  |  | D |  |
| Approach Delay (s) 0.0 |  |  |  |  | 14.5 |  |  | 91.8 |  |  | 36.0 |  |
| Approach LOS |  | A |  |  | B |  |  | F |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 32.8 |  | HCM 2000 | Level of S | ervice |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.63 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 70.0 |  | Sum of los | time (s) |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 54.4\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |




C Critical Lane Group


C Critical Lane Group

c Critical Lane Group




C Critical Lane Group

|  | 4 |  |  | 7 |  |  | 4 | $\dagger$ | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |  |  |
| Traffic Volume (vph) | 10 | 0 | 0 | 0 | 50 | 75 | 5 | 485 | 20 | 0 | 0 | 0 |
| Future Volume (vph) | 10 | 0 | 0 | 0 | 50 | 75 | 5 | 485 | 20 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  |  | 4.0 |  |  |  |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Frt |  | 1.00 |  |  | 0.92 |  |  | 0.99 |  |  |  |  |
| Flt Protected |  | 0.95 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Satd. Flow (prot) |  | 1752 |  |  | 1696 |  |  | 1834 |  |  |  |  |
| Flt Permitted |  | 0.58 |  |  | 1.00 |  |  | 1.00 |  |  |  |  |
| Satd. Flow (perm) |  | 1069 |  |  | 1696 |  |  | 1834 |  |  |  |  |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 11 | 0 | 0 | 0 | 53 | 79 | 5 | 511 | 21 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 11 | 0 | 0 | 132 | 0 | 0 | 537 | 0 | 0 | 0 | 0 |
| Turn Type | Perm | NA |  |  | NA |  | Perm | NA |  |  |  |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 4 |  |  |  |  |
| Permitted Phases | 2 |  |  |  |  |  | 4 |  |  |  |  |  |
| Actuated Green, G (s) |  | 6.4 |  |  | 6.4 |  |  | 23.0 |  |  |  |  |
| Effective Green, g (s) |  | 6.9 |  |  | 6.9 |  |  | 23.5 |  |  |  |  |
| Actuated g/C Ratio |  | 0.10 |  |  | 0.10 |  |  | 0.34 |  |  |  |  |
| Clearance Time (s) |  | 4.5 |  |  | 4.5 |  |  | 4.5 |  |  |  |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  |  | 3.0 |  |  |  |  |
| Lane Grp Cap (vph) |  | 105 |  |  | 167 |  |  | 615 |  |  |  |  |
| v/s Ratio Prot |  |  |  |  | c0.08 |  |  |  |  |  |  |  |
| v/s Ratio Perm |  | 0.01 |  |  |  |  |  | 0.29 |  |  |  |  |
| v/c Ratio |  | 0.10 |  |  | 0.79 |  |  | 0.87 |  |  |  |  |
| Uniform Delay, d1 |  | 28.7 |  |  | 30.8 |  |  | 21.8 |  |  |  |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 0.51 |  |  |  |  |
| Incremental Delay, d2 |  | 0.4 |  |  | 22.0 |  |  | 7.4 |  |  |  |  |
| Delay (s) |  | 29.2 |  |  | 52.8 |  |  | 18.7 |  |  |  |  |
| Level of Service |  | C |  |  | D |  |  | B |  |  |  |  |
| Approach Delay (s) |  | 29.2 |  |  | 52.8 |  |  | 18.7 |  |  | 0.0 |  |
| Approach LOS |  | C |  |  | D |  |  | B |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 25.5 |  | HCM 2000 | Level of S | ervice |  | C |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.45 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 70.0 |  | Sum of lost | time (s) |  |  | 12.5 |  |  |  |
| Intersection Capacity Utilization |  |  | 42.0\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group


| Movement | EBL | EBR | EBR2 | WBL | WBT | WBR | NBT | SET | SER |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 「安 |  |  | \＄ |  | $\uparrow$ | 个4 | F |
| Trafic Volume（vph） | 10 | 240 | 105 | 130 | 0 | 335 | 0 | 740 | 85 |
| Future Volume（vph） | 10 | 240 | 105 | 130 | 0 | 335 | 0 | 740 | 85 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 6.0 | 6.0 |  |  | 6.0 |  |  | 6.0 | 6.0 |
| Lane Util．Factor | 1.00 | 0.88 |  |  | 1.00 |  |  | 0.95 | 1.00 |
| Frpb，ped／bikes | 1.00 | 1.00 |  |  | 1.00 |  |  | 1.00 | 1.00 |
| Flpb，ped／bikes | 1.00 | 1.00 |  |  | 1.00 |  |  | 1.00 | 1.00 |
| Frt | 1.00 | 0.85 |  |  | 0.90 |  |  | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  |  | 0.99 |  |  | 1.00 | 1.00 |
| Satd．Flow（prot） | 1752 | 2760 |  |  | 1642 |  |  | 3505 | 1568 |
| Flt Permitted | 0.95 | 1.00 |  |  | 0.99 |  |  | 1.00 | 1.00 |
| Satd．Flow（perm） | 1752 | 2760 |  |  | 1642 |  |  | 3505 | 1568 |
| Peak－hour factor，PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj．Flow（vph） | 11 | 253 | 111 | 137 | 0 | 353 | 0 | 779 | 89 |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 11 | 364 | 0 | 0 | 490 | 0 | 0 | 779 | 89 |
| Confl．Peds．（\＃／hr） |  |  | 10 |  |  |  |  |  |  |
| Turn Type | Prot | Prot |  | Split | NA |  |  | NA | Prot |
| Protected Phases | 4 | 4 |  | 6 | 6 |  | 8 | 5 | 5 |
| Permitted Phases |  |  |  |  |  |  |  |  |  |
| Actuated Green，G（s） | 16.8 | 16.8 |  |  | 26.0 |  |  | 25.0 | 25.0 |
| Effective Green，g（s） | 16.8 | 16.8 |  |  | 26.0 |  |  | 25.0 | 25.0 |
| Actuated g／C Ratio | 0.17 | 0.17 |  |  | 0.26 |  |  | 0.25 | 0.25 |
| Clearance Time（s） | 6.0 | 6.0 |  |  | 6.0 |  |  | 6.0 | 6.0 |
| Vehicle Extension（s） | 3.0 | 3.0 |  |  | 1.5 |  |  | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 294 | 464 |  |  | 427 |  |  | 878 | 392 |
| v／s Ratio Prot | 0.01 | c0．13 |  |  | c0．30 |  |  | c0． 22 | 0.06 |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  |  |  |  |  |  |  |  |  |
| v／c Ratio | 0.04 | 0.78 |  |  | 1.15 |  |  | 0.89 | 0.23 |
| Uniform Delay，d1 | 34.7 | 39.8 |  |  | 36.9 |  |  | 36.0 | 29.7 |
| Progression Factor | 1.00 | 1.00 |  |  | 1.00 |  |  | 1.00 | 1.00 |
| Incremental Delay，d2 | 0.1 | 8.5 |  |  | 90.5 |  |  | 10.8 | 0.3 |
| Delay（s） | 34.8 | 48.2 |  |  | 127.4 |  |  | 46.8 | 30.0 |
| Level of Service | C | D |  |  | F |  |  | D | C |
| Approach Delay（s） |  |  |  |  | 127.4 |  | 0.0 | 45.1 |  |
| Approach LOS |  |  |  |  | F |  | A | D |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 68.9 | HCM 2000 Level of Service | E |
| HCM 2000 Volume to Capacity ratio | 0.88 |  | 26.0 |
| Actuated Cycle Length（s） | 99.8 | Sum of lost time（s） | D |
| Intersection Capacity Utilization | $75.4 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| C Critical Lane Group |  |  |  |


c Critical Lane Group

## Appendix F: Vissim Model Intersection Results

|  | $\mathrm{F}-1$ | IMPROVEMENT PROJECT |
| :--- | :--- | :--- | :--- |

Table F-1 Future No-Build Alternative 8-9 A M

| Intersection | Node | Approach | Movement | Movement |  |  |  |  | Intersection |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) | Max Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |
| N Williams Ave \& N/NE Hancock St | 1001 | EB | EBL | 10 | 9 | 7.2 | 68 | 12 | 675 | 597 | 11.2 |
|  | 1001 |  | EBT | 10 | 10 | 8.3 | 47 | 12 |  |  |  |
|  | 1001 | WB | WBT | 0 | 0 | 0.0 | 106 | 31 |  |  |  |
|  | 1001 |  | WBR | 180 | 179 | 11.2 | 138 | 29 |  |  |  |
|  | 1001 | NB | NBL | 10 | 6 | 2.8 | 2 | 7 |  |  |  |
|  | 1001 |  | NBT | 455 | 383 | 1.5 | 0 | 0 |  |  |  |
|  | 1001 |  | NBR | 10 | 10 | 1.5 | 0 | 0 |  |  |  |
| N/NE Broadway \& N Williams Ave | 1008 | WB | WBT | 1255 | 1175 | 13.9 | 287 | 20 | 2,475 | 2,309 | 16.3 |
|  | 1008 |  | WBR | 970 | 896 | 16.9 | 285 | 15 |  |  |  |
|  | 1008 | NB | NBL | 0 | 0 | 0.0 | 119 | 18 |  |  |  |
|  | 1008 |  | NBT | 250 | 239 | 25.5 | 137 | 27 |  |  |  |
| N Broadway \& N Vancouver Ave (I-5 SB Exit Ramp) | 1009 | SB | SBL | 855 | 600 | 81.2 | 276 | 48 | 2,675 | 2,240 | 43.8 |
|  | 1009 |  | SBT | 255 | 248 | 31.0 | 141 | 16 |  |  |  |
|  | 1009 |  | SBR | 310 | 211 | 71.3 | 223 | 54 |  |  |  |
|  | 1009 | WB | WBL | 505 | 493 | 26.9 | 278 | 27 |  |  |  |
|  | 1009 |  | WBT | 750 | 688 | 19.5 | 278 | 27 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Broadway \& N Larrabee Ave | 1010 | EB | EBT | 590 | 609 | 7.2 | 262 | 90 | 1,970 | 1,818 | 12.1 |
|  | 1010 |  | EBR | 220 | 218 | 42.3 | 508 | 105 |  |  |  |
|  | 1010 | SB | SBL | 0 | 2 | 81.5 | 19 | 10 |  |  |  |
|  | 1010 |  | SBT | 20 | 19 | 84.5 | 65 | 11 |  |  |  |
|  | 1010 | WB | WBL | 5 | 2 | 86.5 | 26 | 25 |  |  |  |
|  | 1010 |  | WBT | 970 | 811 | 0.9 | 123 | 73 |  |  |  |
|  | 1010 |  | WBR | 5 | 2 | 38.0 | 21 | 12 |  |  |  |
|  | 1010 | NB | NBL | 60 | 58 | 62.4 | 150 | 36 |  |  |  |
|  | 1010 |  | NBT | 25 | 26 | 61.6 | 80 | 15 |  |  |  |
|  | 1010 |  | NBR | 75 | 71 | 6.2 | 93 | 25 |  |  |  |
| N Weidler St \& N Vancouver Ave | 1055 | EB | EBT | 355 | 371 | 14.6 | 195 | 45 | 2,230 | 1,968 | 12.9 |
|  | 1055 |  | EBR | 260 | 260 | 11.7 | 228 | 32 |  |  |  |
|  | 1055 | SB | SBL | 875 | 627 | 5.6 | 279 | 16 |  |  |  |
|  | 1055 |  | SBT | 740 | 710 | 18.9 | 276 | 16 |  |  |  |
| N Wheeler Ave/ N Williams Ave/ N Ramsey Way \&l-5 SB Entrance Ramp | 1067 | EB | EBL | 50 | 42 | 33.8 | 160 | 49 | 1,235 | 1,221 | 37.2 |
|  | 1067 |  | EBT | 120 | 120 | 35.5 | 160 | 49 |  |  |  |
|  | 1067 |  | EBR | 60 | 56 | 46.1 | 160 | 49 |  |  |  |
|  | 1067 | SB | SBL | 915 | 906 | 39.4 | 305 | 12 |  |  |  |
|  | 1067 |  | SBT | 80 | 80 | 11.3 | 137 | 51 |  |  |  |
|  | 1067 | NB | NBT | 10 | 18 | 30.6 | 64 | 15 |  |  |  |



| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 15 | 10 | 7.0 | 57 | 13 | 2,545 | 2,029 | 66.1 |
|  | 2091 |  | EBT | 1025 | 813 | 0.8 | 57 | 13 |  |  |  |
|  | 2091 | NB | NBT | 740 | 586 | 113.8 | 3470 | 2418 |  |  |  |
|  | 2091 |  | NBR | 765 | 620 | 52.5 | 375 | 110 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 130 | 102 | 8.8 | 236 | 39 | 1,870 | 1,512 | 7.1 |
|  | 2247 |  | EBT | 1550 | 1248 | 6.1 | 236 | 39 |  |  |  |
|  | 2247 |  | EBR | 100 | 78 | 3.6 | 240 | 39 |  |  |  |
|  | 2247 | SB | SBL | 10 | 6 | 13.8 | 57 | 15 |  |  |  |
|  | 2247 |  | SBT | 10 | 11 | 30.1 | 57 | 15 |  |  |  |
|  | 2247 | NB | NBT | 55 | 57 | 24.4 | 98 | 18 |  |  |  |
|  | 2247 |  | NBR | 15 | 10 | 9.5 | 103 | 18 |  |  |  |
| NE Broadway \& NE 2nd Ave | 2248 | SB | SBT | 5 | 6 | 19.2 | 137 | 34 | 1,710 | 1,669 | 27.7 |
|  | 2248 |  | SBR | 145 | 142 | 15.0 | 139 | 32 |  |  |  |
|  | 2248 | WB | WBL | 15 | 11 | 16.5 | 539 | 14 |  |  |  |
|  | 2248 |  | WBT | 1310 | 1301 | 28.8 | 539 | 14 |  |  |  |
|  | 2248 |  | WBR | 50 | 49 | 47.7 | 539 | 14 |  |  |  |
|  | 2248 | NB | NBL | 55 | 58 | 30.2 | 196 | 43 |  |  |  |
|  | 2248 |  | NBT | 130 | 102 | 22.0 | 196 | 43 |  |  |  |



Table F-2 Future No-Build Alternative 5-6 PM

| Intersection | Node | Approach | Movement | Movement |  |  |  |  | Intersection |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) | Max <br> Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |
| N Williams Ave \& N/NE Hancock St | 1001 | EB | EBL | 5 | 4 | 6.9 | 41 | 1 | 750 | 681 | 10.9 |
|  | 1001 |  | EBT | 0 | 0 | 0.0 | 20 | 1 |  |  |  |
|  | 1001 | WB | WBT | 0 | 0 | 0.0 | 66 | 26 |  |  |  |
|  | 1001 |  | WBR | 95 | 93 | 10.9 | 103 | 24 |  |  |  |
|  | 1001 | NB | NBL | 5 | 2 | 4.2 | 0 | 0 |  |  |  |
|  | 1001 |  | NBT | 620 | 563 | 2.3 | 0 | 0 |  |  |  |
|  | 1001 |  | NBR | 25 | 19 | 2.5 | 0 | 0 |  |  |  |
| N/NE Broadway \& N Williams Ave | 1008 | WB | WBT | 900 | 881 | 11.2 | 262 | 26 | 2,320 | 2,176 | 15.4 |
|  | 1008 |  | WBR | 860 | 801 | 14.5 | 284 | 14 |  |  |  |
|  | 1008 | NB | NBL | 20 | 18 | 26.8 | 192 | 42 |  |  |  |
|  | 1008 |  | NBT | 540 | 478 | 24.0 | 225 | 55 |  |  |  |
| N Broadway \& N Vancouver Ave (I-5 SB Exit Ramp) | 1009 | SB | SBL | 930 | 669 | 125.7 | 4048 | 4228 | 2,615 | 2,206 | 73.1 |
|  | 1009 |  | SBT | 355 | 335 | 80.8 | 472 | 247 |  |  |  |
|  | 1009 |  | SBR | 410 | 304 | 85.3 | 319 | 205 |  |  |  |
|  | 1009 | WB | WBL | 405 | 400 | 39.1 | 258 | 19 |  |  |  |
|  | 1009 |  | WBT | 515 | 498 | 16.9 | 258 | 19 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume <br> Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Broadway \& N Larrabee Ave | 1010 | EB | EBT | 1135 | 1099 | 64.7 | 1782 | 959 | 2,770 | 2,587 | 43.4 |
|  | 1010 |  | EBR | 280 | 256 | 67.1 | 1086 | 734 |  |  |  |
|  | 1010 | SB | SBL | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1010 |  | SBT | 25 | 26 | 69.5 | 85 | 18 |  |  |  |
|  | 1010 | WB | WBL | 15 | 11 | 45.7 | 51 | 11 |  |  |  |
|  | 1010 |  | WBT | 905 | 791 | 1.5 | 194 | 64 |  |  |  |
|  | 1010 |  | WBR | 20 | 17 | 32.6 | 62 | 24 |  |  |  |
|  | 1010 | NB | NBL | 120 | 121 | 85.1 | 220 | 12 |  |  |  |
|  | 1010 |  | NBT | 235 | 233 | 38.7 | 210 | 11 |  |  |  |
|  | 1010 |  | NBR | 35 | 33 | 21.3 | 80 | 42 |  |  |  |
| N Weidler St \& $N$ Vancouver Ave | 1055 | EB | EBT | 845 | 818 | 38.6 | 371 | 14 | 2,785 | 2,446 | 28.1 |
|  | 1055 |  | EBR | 250 | 238 | 16.5 | 336 | 50 |  |  |  |
|  | 1055 | SB | SBL | 960 | 714 | 30.0 | 319 | 7 |  |  |  |
|  | 1055 |  | SBT | 730 | 677 | 17.5 | 316 | 7 |  |  |  |
| N Wheeler Ave/ N Williams Ave/ N Ramsey Way \&l-5 SB Entrance Ramp | 1067 | EB | EBL | 105 | 85 | 52.1 | 172 | 33 | 1,350 | 1,277 | 28.5 |
|  | 1067 |  | EBT | 240 | 233 | 26.3 | 172 | 33 |  |  |  |
|  | 1067 |  | EBR | 20 | 19 | 23.0 | 172 | 33 |  |  |  |
|  | 1067 | SB | SBL | 735 | 712 | 30.9 | 273 | 26 |  |  |  |
|  | 1067 |  | SBT | 240 | 210 | 14.2 | 199 | 43 |  |  |  |
|  | 1067 | NB | NBT | 10 | 18 | 21.9 | 69 | 12 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  |  |  | Intersection |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) | Max <br> Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |
| N/NE Weidler St \& N Williams Ave | 1068 | EB | EBL | 460 | 397 | 20.4 | 289 | 8 | 1,920 | 1,613 | 17.8 |
|  | 1068 |  | EBT | 1345 | 1126 | 13.8 | 288 | 8 |  |  |  |
|  | 1068 | NB | NBT | 100 | 90 | 55.4 | 156 | 52 |  |  |  |
|  | 1068 |  | NBR | 15 | 0 | 0.0 | 77 | 13 |  |  |  |
| N Broadway \& N Benton Ave | 1098 | EB | EBL | 95 | 94 | 50.0 | 291 | 32 | 2,265 | 2,090 | 17.9 |
|  | 1098 |  | EBT | 930 | 896 | 13.5 | 271 | 45 |  |  |  |
|  | 1098 |  | EBR | 145 | 137 | 7.0 | 276 | 45 |  |  |  |
|  | 1098 | SB | SBL | 25 | 24 | 62.4 | 151 | 28 |  |  |  |
|  | 1098 |  | SBT | 25 | 25 | 53.4 | 151 | 28 |  |  |  |
|  | 1098 |  | SBR | 30 | 31 | 25.6 | 156 | 28 |  |  |  |
|  | 1098 | WB | WBL | 50 | 45 | 90.3 | 129 | 44 |  |  |  |
|  | 1098 |  | WBT | 900 | 781 | 12.1 | 347 | 91 |  |  |  |
|  | 1098 |  | WBR | 20 | 14 | 13.1 | 350 | 91 |  |  |  |
|  | 1098 | NB | NBL | 10 | 7 | 66.7 | 45 | 23 |  |  |  |
|  | 1098 |  | NBT | 25 | 28 | 48.3 | 110 | 34 |  |  |  |
|  | 1098 |  | NBR | 10 | 7 | 70.3 | 110 | 34 |  |  |  |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 35 | 33 | 45.5 | 79 | 22 | 1,920 | 1,835 | 28.1 |
|  | 2001 | WB | WBT | 1035 | 1035 | 35.2 | 379 | 70 |  |  |  |
|  | 2001 |  | WBR | 20 | 17 | 45.0 | 379 | 70 |  |  |  |
|  | 2001 | NB | NBL | 680 | 620 | 15.8 | 282 | 15 |  |  |  |
|  | 2001 |  | NBT | 150 | 130 | 24.5 | 282 | 15 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 35 | 25 | 12.7 | 273 | 20 | 2,735 | 2,398 | 75.4 |
|  | 2091 |  | EBT | 1325 | 1107 | 6.3 | 273 | 20 |  |  |  |
|  | 2091 | NB | NBT | 795 | 721 | 125.5 | 4974 | 1063 |  |  |  |
|  | 2091 |  | NBR | 580 | 545 | 58.0 | 334 | 93 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 200 | 164 | 10.3 | 293 | 20 | 1,970 | 1,716 | 9.2 |
|  | 2247 |  | EBT | 1500 | 1317 | 8.6 | 293 | 20 |  |  |  |
|  | 2247 |  | EBR | 205 | 171 | 6.8 | 297 | 20 |  |  |  |
|  | 2247 | SB | SBL | 10 | 11 | 24.9 | 71 | 17 |  |  |  |
|  | 2247 |  | SBT | 20 | 19 | 36.1 | 71 | 17 |  |  |  |
|  | 2247 | NB | NBT | 20 | 19 | 23.4 | 55 | 14 |  |  |  |
|  | 2247 |  | NBR | 15 | 14 | 8.0 | 60 | 14 |  |  |  |
| NE Broadway \& NE 2nd Ave | 2248 | SB | SBT | 15 | 12 | 13.8 | 73 | 14 | 1,345 | 1,294 | 11.4 |
|  | 2248 |  | SBR | 70 | 68 | 7.1 | 81 | 21 |  |  |  |
|  | 2248 | WB | WBL | 20 | 19 | 7.6 | 377 | 114 |  |  |  |
|  | 2248 |  | WBT | 965 | 955 | 11.3 | 377 | 114 |  |  |  |
|  | 2248 |  | WBR | 55 | 57 | 13.6 | 377 | 114 |  |  |  |
|  | 2248 | NB | NBL | 20 | 19 | 22.4 | 184 | 42 |  |  |  |
|  | 2248 |  | NBT | 200 | 165 | 12.1 | 184 | 42 |  |  |  |



Table F-3 Future No-Build Alternative 7-8 AM



| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N/NE Weidler St \& N Williams Ave | 1068 | EB | EBL | 166 | 165 | 2.6 | 166 | 51 | 1,071 | 1,015 | 3.6 |
|  | 1068 |  | EBT | 855 | 809 | 3.0 | 165 | 51 |  |  |  |
|  | 1068 | NB | NBT | 42 | 40 | 18.7 | 63 | 13 |  |  |  |
|  | 1068 |  | NBR | 8 | 1 | 16.1 | 69 | 9 |  |  |  |
| N Broadway \& N Benton Ave | 1098 | EB | EBL | 46 | 44 | 67.9 | 191 | 54 | 1,443 | 1,422 | 12.7 |
|  | 1098 |  | EBT | 440 | 447 | 2.5 | 185 | 50 |  |  |  |
|  | 1098 |  | EBR | 66 | 65 | 2.6 | 190 | 50 |  |  |  |
|  | 1098 | SB | SBL | 8 | 8 | 56.1 | 107 | 27 |  |  |  |
|  | 1098 |  | SBT | 21 | 20 | 52.4 | 107 | 27 |  |  |  |
|  | 1098 |  | SBR | 8 | 8 | 20.6 | 112 | 27 |  |  |  |
|  | 1098 | WB | WBL | 4 | 3 | 87.3 | 31 | 19 |  |  |  |
|  | 1098 |  | WBT | 793 | 768 | 12.9 | 315 | 35 |  |  |  |
|  | 1098 |  | WBR | 33 | 35 | 17.4 | 318 | 35 |  |  |  |
|  | 1098 | NB | NBL | 12 | 11 | 57.6 | 59 | 12 |  |  |  |
|  | 1098 |  | NBT | 8 | 10 | 52.0 | 57 | 18 |  |  |  |
|  | 1098 |  | NBR | 4 | 3 | 53.3 | 57 | 18 |  |  |  |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 21 | 18 | 39.4 | 53 | 8 | 1,901 | 1,869 | 30.5 |
|  | 2001 | WB | WBT | 1237 | 1216 | 38.0 | 530 | 39 |  |  |  |
|  | 2001 |  | WBR | 17 | 15 | 36.9 | 530 | 39 |  |  |  |
|  | 2001 | NB | NBL | 589 | 586 | 14.9 | 263 | 16 |  |  |  |
|  | 2001 |  | NBT | 37 | 34 | 23.0 | 263 | 16 |  |  |  |




Table F-4 Future No-Build Alternative 4-5 PM



| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N/NE Weidler St \& N Williams Ave | 1068 | EB | EBL | 442 | 406 | 15.6 | 284 | 6 | 1,843 | 1,667 | 13.8 |
|  | 1068 |  | EBT | 1291 | 1169 | 11.4 | 283 | 6 |  |  |  |
|  | 1068 | NB | NBT | 96 | 92 | 36.1 | 99 | 14 |  |  |  |
|  | 1068 |  | NBR | 14 | 0 | 0.0 | 66 | 0 |  |  |  |
| N Broadway \& N Benton Ave | 1098 | EB | EBL | 91 | 86 | 44.5 | 266 | 40 | 2,175 | 2,103 | 13.4 |
|  | 1098 |  | EBT | 893 | 913 | 6.7 | 226 | 53 |  |  |  |
|  | 1098 |  | EBR | 139 | 140 | 5.0 | 231 | 53 |  |  |  |
|  | 1098 | SB | SBL | 24 | 20 | 55.5 | 125 | 19 |  |  |  |
|  | 1098 |  | SBT | 24 | 24 | 51.9 | 125 | 19 |  |  |  |
|  | 1098 |  | SBR | 29 | 31 | 22.6 | 130 | 19 |  |  |  |
|  | 1098 | WB | WBL | 48 | 40 | 83.3 | 116 | 15 |  |  |  |
|  | 1098 |  | WBT | 864 | 794 | 11.1 | 312 | 78 |  |  |  |
|  | 1098 |  | WBR | 19 | 16 | 13.2 | 315 | 78 |  |  |  |
|  | 1098 | NB | NBL | 10 | 9 | 63.0 | 45 | 16 |  |  |  |
|  | 1098 |  | NBT | 24 | 25 | 47.6 | 83 | 21 |  |  |  |
|  | 1098 |  | NBR | 10 | 6 | 46.6 | 83 | 21 |  |  |  |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 34 | 32 | 38.0 | 67 | 14 | 1,844 | 1,812 | 23.1 |
|  | 2001 | WB | WBT | 994 | 980 | 30.6 | 284 | 51 |  |  |  |
|  | 2001 |  | WBR | 19 | 16 | 39.7 | 284 | 51 |  |  |  |
|  | 2001 | NB | NBL | 653 | 648 | 11.0 | 287 | 10 |  |  |  |
|  | 2001 |  | NBT | 144 | 137 | 21.3 | 287 | 10 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 34 | 27 | 11.4 | 280 | 13 | 2,626 | 2,480 | 52.4 |
|  | 2091 |  | EBT | 1272 | 1137 | 6.7 | 280 | 13 |  |  |  |
|  | 2091 | NB | NBT | 763 | 764 | 83.3 | 2822 | 2199 |  |  |  |
|  | 2091 |  | NBR | 557 | 553 | 38.0 | 325 | 71 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 192 | 176 | 10.8 | 310 | 26 | 1,891 | 1,767 | 9.8 |
|  | 2247 |  | EBT | 1440 | 1342 | 9.3 | 310 | 26 |  |  |  |
|  | 2247 |  | EBR | 197 | 188 | 7.2 | 314 | 26 |  |  |  |
|  | 2247 | SB | SBL | 10 | 13 | 24.1 | 65 | 14 |  |  |  |
|  | 2247 |  | SBT | 19 | 18 | 35.2 | 65 | 14 |  |  |  |
|  | 2247 | NB | NBT | 19 | 19 | 23.8 | 58 | 13 |  |  |  |
|  | 2247 |  | NBR | 14 | 13 | 7.9 | 62 | 13 |  |  |  |
| NE Broadway \& NE 2nd Ave | 2248 | SB | SBT | 14 | 13 | 12.7 | 64 | 13 | 1,290 | 1,265 | 10.2 |
|  | 2248 |  | SBR | 67 | 63 | 6.6 | 68 | 17 |  |  |  |
|  | 2248 | WB | WBL | 19 | 18 | 9.2 | 271 | 61 |  |  |  |
|  | 2248 |  | WBT | 926 | 924 | 9.6 | 271 | 61 |  |  |  |
|  | 2248 |  | WBR | 53 | 53 | 11.5 | 271 | 61 |  |  |  |
|  | 2248 | NB | NBL | 19 | 19 | 23.6 | 180 | 33 |  |  |  |
|  | 2248 |  | NBT | 192 | 175 | 13.2 | 180 | 33 |  |  |  |



Table F-5 Future Revised Build Alternative 2-Way Ramsay 8-9 A M


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Broadway \& N Larrabee Ave | 1010 | EB | EBT | 715 | 717 | 11.7 | 335 | 101 | 2,500 | 2,356 | 20.7 |
|  | 1010 |  | EBR | 245 | 235 | 35.6 | 406 | 63 |  |  |  |
|  | 1010 | SB | SBL | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1010 |  | SBT | 30 | 29 | 81.1 | 96 | 15 |  |  |  |
|  | 1010 | WB | WBL | 5 | 4 | 49.7 | 31 | 13 |  |  |  |
|  | 1010 |  | WBT | 965 | 877 | 2.8 | 163 | 64 |  |  |  |
|  | 1010 |  | WBR | 115 | 109 | 33.2 | 210 | 50 |  |  |  |
|  | 1010 | NB | NBL | 275 | 239 | 58.3 | 221 | 12 |  |  |  |
|  | 1010 |  | NBT | 70 | 65 | 58.2 | 221 | 12 |  |  |  |
|  | 1010 |  | NBR | 80 | 83 | 68.8 | 190 | 25 |  |  |  |
| N Weidler St \& N Vancouver Ave | 1055 | EB | EBT | 590 | 599 | 5.2 | 199 | 107 | 1,760 | 1,717 | 19.5 |
|  | 1055 |  | EBR | 295 | 280 | 42.5 | 349 | 25 |  |  |  |
|  | 1055 | SB | SBL | 25 | 19 | 26.0 | 257 | 18 |  |  |  |
|  | 1055 |  | SBT | 850 | 820 | 21.9 | 257 | 18 |  |  |  |
| N Wheeler Ave/ N Williams Ave/ N Ramsey Way \& I-5 SB Ramps | 1067 | EB | EBL | 0 | 0 | 0.0 | 90 | 18 | 1,615 | 1,505 | 30.1 |
|  | 1067 |  | EBT | 80 | 75 | 32.9 | 90 | 18 |  |  |  |
|  | 1067 |  | EBR | 20 | 19 | 35.8 | 90 | 18 |  |  |  |
|  | 1067 | WB | WBL | 130 | 116 | 56.5 | 493 | 49 |  |  |  |
|  | 1067 |  | WBT | 230 | 184 | 57.3 | 493 | 49 |  |  |  |
|  | 1067 | SB | SBL | 995 | 970 | 22.7 | 299 | 19 |  |  |  |
|  | 1067 |  | SBT | 150 | 131 | 18.9 | 170 | 52 |  |  |  |
|  | 1067 | NB | NBT | 10 | 10 | 44.4 | 48 | 0 |  |  |  |

Report

| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N/NE Weidler St \& N Williams Ave | 1068 | EB | EBL | 190 | 184 | 3.4 | 141 | 48 | 625 | 625 | 3.8 |
|  | 1068 |  | EBT | 425 | 430 | 3.4 | 138 | 48 |  |  |  |
|  | 1068 | NB | NBT | 10 | 10 | 27.9 | 47 | 0 |  |  |  |
| N Broadway \& N Benton Ave | 1098 | EB | EBL | 10 | 11 | 64.7 | 50 | 14 | 2,025 | 1,922 | 11.2 |
|  | 1098 |  | EBT | 755 | 761 | 5.1 | 230 | 44 |  |  |  |
|  | 1098 |  | EBR | 30 | 27 | 5.1 | 230 | 44 |  |  |  |
|  | 1098 | SB | SBL | 10 | 6 | 51.4 | 114 | 16 |  |  |  |
|  | 1098 |  | SBT | 25 | 22 | 51.0 | 114 | 16 |  |  |  |
|  | 1098 |  | SBR | 15 | 18 | 53.4 | 114 | 16 |  |  |  |
|  | 1098 | WB | WBL | 5 | 3 | 52.5 | 30 | 16 |  |  |  |
|  | 1098 |  | WBT | 1055 | 959 | 9.1 | 403 | 73 |  |  |  |
|  | 1098 |  | WBR | 35 | 34 | 27.1 | 403 | 73 |  |  |  |
|  | 1098 | NB | NBL | 15 | 15 | 64.7 | 54 | 14 |  |  |  |
|  | 1098 |  | NBT | 20 | 20 | 54.8 | 146 | 29 |  |  |  |
|  | 1098 |  | NBR | 50 | 45 | 54.7 | 146 | 29 |  |  |  |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 30 | 28 | 11.7 | 41 | 8 | 2,520 | 2,332 | 23.5 |
|  | 2001 | WB | WBT | 1560 | 1548 | 32.3 | 532 | 36 |  |  |  |
|  | 2001 |  | WBR | 10 | 12 | 54.2 | 532 | 36 |  |  |  |
|  | 2001 | NB | NBL | 865 | 699 | 5.2 | 105 | 26 |  |  |  |
|  | 2001 |  | NBT | 55 | 46 | 5.4 | 105 | 26 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 15 | 14 | 18.9 | 185 | 20 | 2,780 | 2,348 | 17.1 |
|  | 2091 |  | EBT | 410 | 418 | 11.2 | 185 | 20 |  |  |  |
|  | 2091 | NB | NBT | 905 | 731 | 16.5 | 175 | 25 |  |  |  |
|  | 2091 |  | NBR | 1450 | 1185 | 19.5 | 551 | 58 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 100 | 90 | 7.6 | 266 | 65 | 1,945 | 1,676 | 5.9 |
|  | 2247 |  | EBT | 1750 | 1502 | 5.1 | 266 | 65 |  |  |  |
|  | 2247 |  | EBR | 10 | 7 | 4.7 | 270 | 65 |  |  |  |
|  | 2247 | SB | SBL | 25 | 22 | 15.9 | 63 | 17 |  |  |  |
|  | 2247 |  | SBT | 10 | 12 | 20.2 | 63 | 17 |  |  |  |
|  | 2247 | NB | NBT | 40 | 35 | 24.4 | 71 | 12 |  |  |  |
|  | 2247 |  | NBR | 10 | 8 | 9.5 | 77 | 12 |  |  |  |
| NE Broadway \& NE 2nd Ave | 2248 | SB | SBT | 25 | 22 | 25.9 | 150 | 17 | 1,765 | 1,728 | 10.6 |
|  | 2248 |  | SBR | 150 | 151 | 17.2 | 151 | 17 |  |  |  |
|  | 2248 | WB | WBL | 10 | 12 | 4.2 | 381 | 113 |  |  |  |
|  | 2248 |  | WBT | 1385 | 1368 | 8.4 | 381 | 113 |  |  |  |
|  | 2248 |  | WBR | 55 | 50 | 12.7 | 384 | 113 |  |  |  |
|  | 2248 | NB | NBL | 35 | 35 | 14.9 | 148 | 45 |  |  |  |
|  | 2248 |  | NBT | 105 | 90 | 28.5 | 148 | 45 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Vancouver Ave \& N/NE Hancock St | 2249 | EB | EBT | 10 | 10 | 26.6 | 39 | 22 | 415 | 423 | 4.4 |
|  | 2249 |  | EBR | 0 | 0 | 0.0 | 39 | 22 |  |  |  |
|  | 2249 | WB | WBL | 0 | 1 | 10.3 | 99 | 10 |  |  |  |
|  | 2249 |  | WBT | 60 | 60 | 12.8 | 93 | 10 |  |  |  |
|  | 2249 | SB | SBT | 345 | 352 | 2.3 | 9 | 19 |  |  |  |
|  | 2249 |  | SBR | 0 | 0 | 0.0 | 9 | 19 |  |  |  |
| N Williams Ave \& N/NE Multnomah St | 1066 | EB | EBT | 220 | 214 | 10.2 | 151 | 19 | 810 | 767 | 11.7 |
|  | 1066 |  | EBR | 5 | 5 | 6.1 | 151 | 19 |  |  |  |
|  | 1066 | SB | SBL | 205 | 177 | 15.2 | 194 | 34 |  |  |  |
|  | 1066 |  | SBT | 25 | 30 | 15.1 | 194 | 34 |  |  |  |
|  | 1066 |  | SBR | 70 | 59 | 12.9 | 84 | 30 |  |  |  |
|  | 1066 | WB | WBL | 10 | 12 | 12.4 | 112 | 18 |  |  |  |
|  | 1066 |  | WBT | 265 | 260 | 9.3 | 112 | 18 |  |  |  |
|  | 1066 | NB | NBT | 10 | 10 | 29.3 | 48 | 0 |  |  |  |
|  | 1066 |  | NBR | 0 | 0 | 0.0 | 48 | 0 |  |  |  |



| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume <br> Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Broadway \& N Larrabee Ave | 1010 | EB | EBT | 1150 | 1155 | 34.7 | 962 | 394 | 2,645 | 2,555 | 33.7 |
|  | 1010 |  | EBR | 280 | 278 | 41.9 | 572 | 315 |  |  |  |
|  | 1010 | SB | SBL | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1010 |  | SBT | 25 | 25 | 72.3 | 75 | 23 |  |  |  |
|  | 1010 | WB | WBL | 15 | 14 | 79.5 | 58 | 15 |  |  |  |
|  | 1010 |  | WBT | 615 | 577 | 2.6 | 195 | 71 |  |  |  |
|  | 1010 |  | WBR | 85 | 76 | 36.1 | 154 | 23 |  |  |  |
|  | 1010 | NB | NBL | 380 | 340 | 55.4 | 219 | 11 |  |  |  |
|  | 1010 |  | NBT | 20 | 18 | 57.2 | 219 | 11 |  |  |  |
|  | 1010 |  | NBR | 75 | 72 | 102.6 | 166 | 50 |  |  |  |
| N Weidler St \& N Vancouver Ave | 1055 | EB | EBT | 1095 | 1100 | 5.4 | 350 | 15 | 2,015 | 1,960 | 15.3 |
|  | 1055 |  | EBR | 350 | 293 | 58.3 | 363 | 31 |  |  |  |
|  | 1055 | SB | SBL | 45 | 46 | 20.9 | 196 | 24 |  |  |  |
|  | 1055 |  | SBT | 525 | 521 | 11.6 | 196 | 24 |  |  |  |
| N Wheeler Ave/ N Williams Ave/ N Ramsey Way \& I-5 SB Ramps | 1067 | EB | EBL | 10 | 10 | 47.9 | 213 | 34 | 1,655 | 1,544 | 43.4 |
|  | 1067 |  | EBT | 240 | 229 | 46.9 | 213 | 34 |  |  |  |
|  | 1067 |  | EBR | 105 | 97 | 45.6 | 213 | 34 |  |  |  |
|  | 1067 | WB | WBL | 130 | 108 | 53.6 | 515 | 44 |  |  |  |
|  | 1067 |  | WBT | 335 | 278 | 54.8 | 515 | 44 |  |  |  |
|  | 1067 | SB | SBL | 740 | 723 | 37.2 | 284 | 9 |  |  |  |
|  | 1067 |  | SBT | 85 | 89 | 33.5 | 157 | 47 |  |  |  |
|  | 1067 | NB | NBT | 10 | 10 | 42.8 | 47 | 0 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume <br> Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N/NE Weidler St \& N Williams Ave | 1068 | EB | EBL | 360 | 361 | 5.0 | 191 | 35 | 1,160 | 1,165 | 3.6 |
|  | 1068 |  | EBT | 780 | 784 | 2.3 | 191 | 35 |  |  |  |
|  | 1068 | NB | NBT | 20 | 20 | 30.1 | 77 | 24 |  |  |  |
| N Broadway \& N Benton Ave | 1098 | EB | EBL | 15 | 11 | 51.2 | 113 | 87 | 2,160 | 2,097 | 14.8 |
|  | 1098 |  | EBT | 1170 | 1177 | 10.8 | 300 | 16 |  |  |  |
|  | 1098 |  | EBR | 40 | 38 | 18.3 | 300 | 16 |  |  |  |
|  | 1098 | SB | SBL | 25 | 24 | 57.5 | 168 | 24 |  |  |  |
|  | 1098 |  | SBT | 15 | 15 | 48.9 | 168 | 24 |  |  |  |
|  | 1098 |  | SBR | 50 | 50 | 55.0 | 168 | 24 |  |  |  |
|  | 1098 | WB | WBL | 10 | 9 | 72.1 | 46 | 13 |  |  |  |
|  | 1098 |  | WBT | 665 | 620 | 9.7 | 282 | 66 |  |  |  |
|  | 1098 |  | WBR | 70 | 64 | 15.2 | 282 | 66 |  |  |  |
|  | 1098 | NB | NBL | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1098 |  | NBT | 30 | 29 | 51.3 | 163 | 31 |  |  |  |
|  | 1098 |  | NBR | 70 | 60 | 50.5 | 163 | 31 |  |  |  |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 25 | 24 | 15.5 | 39 | 7 | 1,980 | 1,854 | 34.3 |
|  | 2001 | WB | WBT | 920 | 918 | 51.9 | 544 | 21 |  |  |  |
|  | 2001 |  | WBR | 15 | 14 | 136.5 | 544 | 21 |  |  |  |
|  | 2001 | NB | NBL | 860 | 761 | 17.2 | 265 | 17 |  |  |  |
|  | 2001 |  | NBT | 160 | 137 | 3.4 | 265 | 17 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 45 | 39 | 13.4 | 182 | 32 | 3,040 | 2,759 | 23.4 |
|  | 2091 |  | EBT | 735 | 746 | 7.5 | 182 | 32 |  |  |  |
|  | 2091 | NB | NBT | 975 | 858 | 31.8 | 636 | 287 |  |  |  |
|  | 2091 |  | NBR | 1285 | 1116 | 28.0 | 722 | 232 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 140 | 141 | 14.7 | 423 | 43 | 2,100 | 1,936 | 10.8 |
|  | 2247 |  | EBT | 1715 | 1566 | 9.9 | 423 | 43 |  |  |  |
|  | 2247 |  | EBR | 165 | 153 | 11.3 | 426 | 43 |  |  |  |
|  | 2247 | SB | SBL | 15 | 15 | 13.5 | 74 | 19 |  |  |  |
|  | 2247 |  | SBT | 20 | 18 | 30.9 | 74 | 19 |  |  |  |
|  | 2247 | NB | NBT | 30 | 29 | 22.9 | 64 | 11 |  |  |  |
|  | 2247 |  | NBR | 15 | 14 | 11.0 | 70 | 11 |  |  |  |
| NE Broadway \& NE 2nd Ave | 2248 | SB | SBT | 15 | 15 | 19.1 | 115 | 52 | 1,135 | 1,125 | 17.8 |
|  | 2248 |  | SBR | 95 | 94 | 15.9 | 117 | 52 |  |  |  |
|  | 2248 | WB | WBL | 20 | 18 | 5.9 | 363 | 125 |  |  |  |
|  | 2248 |  | WBT | 810 | 802 | 18.6 | 363 | 125 |  |  |  |
|  | 2248 |  | WBR | 25 | 26 | 35.1 | 366 | 125 |  |  |  |
|  | 2248 | NB | NBL | 30 | 29 | 13.8 | 161 | 19 |  |  |  |
|  | 2248 |  | NBT | 140 | 142 | 13.1 | 161 | 19 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Vancouver Ave \& N/NE Hancock St | 2249 | EB | EBT | 10 | 10 | 14.8 | 25 | 2 | 325 | 333 | 2.9 |
|  | 2249 |  | EBR | 0 | 0 | 0.0 | 25 | 2 |  |  |  |
|  | 2249 | WB | WBL | 5 | 2 | 9.2 | 83 | 10 |  |  |  |
|  | 2249 |  | WBT | 50 | 49 | 8.0 | 77 | 10 |  |  |  |
|  | 2249 | SB | SBT | 260 | 273 | 1.5 | 0 | 0 |  |  |  |
|  | 2249 |  | SBR | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
| N Williams Ave \& N/NE Multnomah St | 1066 | EB | EBT | 250 | 248 | 10.2 | 168 | 24 | 1,045 | 1,005 |  |
|  | 1066 |  | EBR | 5 | 5 | 10.7 | 168 | 24 |  |  |  |
|  | 1066 | SB | SBL | 210 | 191 | 15.3 | 178 | 28 |  |  |  |
|  | 1066 |  | SBT | 15 | 14 | 15.3 | 178 | 28 |  |  |  |
|  | 1066 |  | SBR | 105 | 90 | 14.6 | 102 | 27 |  |  | 11.8 |
|  | 1066 | WB | WBL | 0 | 0 | 0.0 | 127 | 14 |  |  |  |
|  | 1066 |  | WBT | 450 | 447 | 10.0 | 127 | 14 |  |  |  |
|  | 1066 | NB | NBT | 10 | 10 | 29.3 | 48 | 0 |  |  |  |
|  | 1066 |  | NBR | 0 | 0 | 0.0 | 48 | 0 |  |  |  |

Table F-7 Future Revised Build Alternative 2-W ay Ramsay 7-8 A M

| Intersection | Node | Approach | Movement | Movement |  |  |  |  |  | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |
| N Williams Ave \& N/NE Hancock St | 1001 | EB | EBL | 8 | 8 | 23.3 | 63 | 22 | 485 | 488 | 15.5 |
|  | 1001 | WB | WBT | 50 | 49 | 29.4 | 167 | 19 |  |  |  |
|  | 1001 |  | WBR | 104 | 102 | 31.5 | 167 | 19 |  |  |  |
|  | 1001 | NB | NBL | 0 | 0 | 0.0 | 242 | 34 |  |  |  |
|  | 1001 |  | NBT | 315 | 324 | 8.2 | 242 | 34 |  |  |  |
|  | 1001 |  | NBR | 8 | 7 | 9.9 | 242 | 34 |  |  |  |
| N/NE <br> Broadway \& N Williams Ave | 1008 | WB | WBT | 1274 | 1255 | 6.5 | 229 | 34 | 2,195 | 2,170 | 10.0 |
|  | 1008 |  | WBR | 764 | 755 | 12.2 | 285 | 20 |  |  |  |
|  | 1008 | NB | NBL | 8 | 5 | 31.7 | 156 | 45 |  |  |  |
|  | 1008 |  | NBT | 149 | 155 | 27.1 | 156 | 45 |  |  |  |
| N <br> Broadway \& N Vancouver Ave | 1009 | SB | SBT | 249 | 249 | 25.2 | 252 | 21 | 1,568 | 1,547 | 6.7 |
|  | 1009 |  | SBR | 37 | 40 | 41.0 | 97 | 15 |  |  |  |
|  | 1009 | WB | WBL | 477 | 474 | 3.1 | 128 | 25 |  |  |  |
|  | 1009 |  | WBT | 805 | 786 | 1.3 | 130 | 52 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  |  |  | Intersection |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |
| N Broadway \& N Larrabee Ave | 1010 | EB | EBT | 593 | 603 | 9.4 | 242 | 40 | 2,073 | 2,063 | 19.3 |
|  | 1010 |  | EBR | 203 | 206 | 33.8 | 285 | 51 |  |  |  |
|  | 1010 | SB | SBL | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1010 |  | SBT | 25 | 20 | 82.5 | 66 | 15 |  |  |  |
|  | 1010 | WB | WBL | 4 | 3 | 25.3 | 26 | 11 |  |  |  |
|  | 1010 |  | WBT | 801 | 794 | 2.0 | 128 | 53 |  |  |  |
|  | 1010 |  | WBR | 95 | 93 | 32.9 | 158 | 31 |  |  |  |
|  | 1010 | NB | NBL | 228 | 218 | 58.8 | 230 | 19 |  |  |  |
|  | 1010 |  | NBT | 58 | 58 | 60.3 | 230 | 19 |  |  |  |
|  | 1010 |  | NBR | 66 | 68 | 67.7 | 181 | 36 |  |  |  |
| N Weidler St \& N Vancouver Ave | 1055 | EB | EBT | 490 | 499 | 4.4 | 169 | 33 | 1,462 | 1,477 | 18.1 |
|  | 1055 |  | EBR | 245 | 247 | 34.6 | 314 | 41 |  |  |  |
|  | 1055 | SB | SBL | 21 | 15 | 27.5 | 249 | 3 |  |  |  |
|  | 1055 |  | SBT | 706 | 716 | 21.7 | 249 | 3 |  |  |  |
| N Wheeler Ave/ N Williams Ave/ N Ramsey Way \& l-5 SB Ramps | 1067 | EB | EBL | 0 | 0 | 0.0 | 88 | 12 | 1,341 | 1,352 | 26.6 |
|  | 1067 |  | EBT | 66 | 66 | 30.8 | 88 | 12 |  |  |  |
|  | 1067 |  | EBR | 17 | 15 | 28.5 | 88 | 12 |  |  |  |
|  | 1067 | WB | WBL | 108 | 106 | 41.4 | 388 | 45 |  |  |  |
|  | 1067 |  | WBT | 191 | 190 | 41.9 | 388 | 45 |  |  |  |
|  | 1067 | SB | SBL | 826 | 828 | 22.1 | 280 | 3 |  |  |  |
|  | 1067 |  | SBT | 125 | 138 | 17.4 | 185 | 47 |  |  |  |
|  | 1067 | NB | NBT | 8 | 10 | 40.6 | 47 | 0 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  |  | Intersection |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |
| N/NE Weidler St \& N Williams Ave | 1068 | EB | EBL | 158 | 148 | 2.5 | 133 | 57 | 519 | 523 | 3.3 |
|  | 1068 |  | EBT | 353 | 365 | 2.8 | 130 | 57 |  |  |  |
|  | 1068 | NB | NBT | 8 | 10 | 31.4 | 47 | 0 |  |  |  |
| N Broadway \& N Benton Ave | 1098 | EB | EBL | 8 | 10 | 59.5 | 61 | 31 | 1,681 | 1,678 | 9.7 |
|  | 1098 |  | EBT | 627 | 642 | 4.9 | 207 | 22 |  |  |  |
|  | 1098 |  | EBR | 25 | 24 | 4.0 | 207 | 22 |  |  |  |
|  | 1098 | SB | SBL | 8 | 5 | 53.4 | 108 | 13 |  |  |  |
|  | 1098 |  | SBT | 21 | 18 | 56.2 | 108 | 13 |  |  |  |
|  | 1098 |  | SBR | 12 | 12 | 60.0 | 108 | 13 |  |  |  |
|  | 1098 | WB | WBL | 4 | 3 | 52.3 | 31 | 18 |  |  |  |
|  | 1098 |  | WBT | 876 | 867 | 6.7 | 326 | 92 |  |  |  |
|  | 1098 |  | WBR | 29 | 27 | 16.8 | 326 | 92 |  |  |  |
|  | 1098 | NB | NBL | 12 | 10 | 74.1 | 61 | 31 |  |  |  |
|  | 1098 |  | NBT | 17 | 16 | 56.2 | 163 | 32 |  |  |  |
|  | 1098 |  | NBR | 42 | 44 | 53.2 | 163 | 32 |  |  |  |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 25 | 24 | 9.6 | 33 | 9 | 2,092 | 2,067 | 18.3 |
|  | 2001 | WB | WBT | 1295 | 1289 | 25.9 | 471 | 71 |  |  |  |
|  | 2001 |  | WBR | 8 | 10 | 37.6 | 471 | 71 |  |  |  |
|  | 2001 | NB | NBL | 718 | 701 | 5.0 | 125 | 39 |  |  |  |
|  | 2001 |  | NBT | 46 | 45 | 6.4 | 125 | 39 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  |  |  | Intersection |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 12 | 12 | 19.1 | 161 | 22 | 2,307 | 2,290 | 17.8 |
|  | 2091 |  | EBT | 340 | 350 | 10.0 | 161 | 22 |  |  |  |
|  | 2091 | NB | NBT | 751 | 732 | 17.2 | 188 | 32 |  |  |  |
|  | 2091 |  | NBR | 1204 | 1195 | 20.3 | 582 | 56 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 83 | 82 | 6.3 | 229 | 32 | 1,614 | 1,609 | 5.3 |
|  | 2247 |  | EBT | 1453 | 1455 | 4.7 | 229 | 32 |  |  |  |
|  | 2247 |  | EBR | 8 | 7 | 3.5 | 232 | 32 |  |  |  |
|  | 2247 | SB | SBL | 21 | 20 | 15.4 | 55 | 24 |  |  |  |
|  | 2247 |  | SBT | 8 | 10 | 19.9 | 55 | 24 |  |  |  |
|  | 2247 | NB | NBT | 33 | 29 | 24.4 | 64 | 13 |  |  |  |
|  | 2247 |  | NBR | 8 | 6 | 8.4 | 71 | 13 |  |  |  |
| NE Broadway \& NE 2nd Ave | 2248 | SB | SBT | 21 | 20 | 23.1 | 121 | 22 | 1,466 | 1,462 | 7.8 |
|  | 2248 |  | SBR | 125 | 124 | 13.5 | 122 | 22 |  |  |  |
|  | 2248 | WB | WBL | 8 | 10 | 3.7 | 225 | 93 |  |  |  |
|  | 2248 |  | WBT | 1150 | 1156 | 5.5 | 225 | 93 |  |  |  |
|  | 2248 |  | WBR | 46 | 44 | 6.2 | 227 | 94 |  |  |  |
|  | 2248 | NB | NBL | 29 | 29 | 16.5 | 148 | 48 |  |  |  |
|  | 2248 |  | NBT | 87 | 81 | 27.5 | 148 | 48 |  |  |  |



Table F-8 Future Revised Build Alternative 2-W ay Ramsay 4-5 PM

| Intersection | Node | Approach | Movement | Movement |  |  |  |  | Intersection |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  | Std. Dev. (feet) | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |
| N Williams Ave \& N/NE Hancock St | 1001 | EB | EBL | 10 | 9 | 35.9 | 57 | 10 | 620 | 587 | 28.5 |
|  | 1001 | WB | WBT | 48 | 44 | 97.2 | 269 | 61 |  |  |  |
|  | 1001 |  | WBR | 72 | 69 | 96.7 | 269 | 61 |  |  |  |
|  | 1001 | NB | NBL | 5 | 5 | 2.4 | 299 | 79 |  |  |  |
|  | 1001 |  | NBT | 466 | 446 | 12.0 | 299 | 79 |  |  |  |
|  | 1001 |  | NBR | 19 | 15 | 4.9 | 299 | 79 |  |  |  |
| N/NE Broadway \& N Williams Ave | 1008 | WB | WBT | 907 | 867 | 4.6 | 157 | 21 | 2,088 | 2,006 | 11.2 |
|  | 1008 |  | WBR | 826 | 776 | 13.1 | 294 | 17 |  |  |  |
|  | 1008 | NB | NBL | 19 | 19 | 21.1 | 234 | 16 |  |  |  |
|  | 1008 |  | NBT | 336 | 346 | 22.9 | 234 | 16 |  |  |  |
| N Broadway \& N Vancouver Ave | 1009 | SB | SBT | 211 | 214 | 22.9 | 217 | 45 | 1,180 | 1,144 | 7.1 |
|  | 1009 |  | SBR | 43 | 45 | 32.4 | 94 | 37 |  |  |  |
|  | 1009 | WB | WBL | 336 | 331 | 2.2 | 108 | 39 |  |  |  |
|  | 1009 |  | WBT | 590 | 554 | 1.8 | 91 | 17 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Broadway \& N Larrabee Ave | 1010 | EB | EBT | 1104 | 1121 | 21.6 | 685 | 116 | 2,539 | 2,492 | 26.7 |
|  | 1010 |  | EBR | 269 | 267 | 36.4 | 426 | 117 |  |  |  |
|  | 1010 | SB | SBL | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1010 |  | SBT | 24 | 24 | 77.4 | 78 | 15 |  |  |  |
|  | 1010 | WB | WBL | 14 | 14 | 84.9 | 56 | 12 |  |  |  |
|  | 1010 |  | WBT | 590 | 570 | 2.7 | 170 | 54 |  |  |  |
|  | 1010 |  | WBR | 82 | 81 | 36.8 | 149 | 24 |  |  |  |
|  | 1010 | NB | NBL | 365 | 327 | 59.3 | 227 | 15 |  |  |  |
|  | 1010 |  | NBT | 19 | 17 | 58.0 | 227 | 15 |  |  |  |
|  | 1010 |  | NBR | 72 | 72 | 65.8 | 150 | 32 |  |  |  |
| N Weidler St \& $N$ Vancouver Ave | 1055 | EB | EBT | 1051 | 1047 | 5.2 | 318 | 49 | 1,934 | 1,889 | 14.3 |
|  | 1055 |  | EBR | 336 | 281 | 52.8 | 379 | 21 |  |  |  |
|  | 1055 | SB | SBL | 43 | 42 | 20.1 | 185 | 24 |  |  |  |
|  | 1055 |  | SBT | 504 | 520 | 11.3 | 185 | 24 |  |  |  |
| N Wheeler Ave/ N Williams Ave/ N Ramsey Way \& I-5 SB Ramps | 1067 | EB | EBL | 10 | 9 | 47.9 | 210 | 30 | 1,590 | 1,542 | 41.8 |
|  | 1067 |  | EBT | 230 | 234 | 45.3 | 210 | 30 |  |  |  |
|  | 1067 |  | EBR | 101 | 98 | 49.4 | 210 | 30 |  |  |  |
|  | 1067 | WB | WBL | 125 | 116 | 49.6 | 507 | 50 |  |  |  |
|  | 1067 |  | WBR | 322 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1067 | SB | SBL | 710 | 710 | 35.8 | 278 | 4 |  |  |  |
|  | 1067 |  | SBT | 82 | 92 | 31.2 | 161 | 32 |  |  |  |
|  | 1067 | NB | NBT | 10 | 10 | 31.8 | 47 | 0 |  |  |  |



| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 43 | 40 | 15.4 | 197 | 41 | 2,919 | 2,719 | 22.7 |
|  | 2091 |  | EBT | 706 | 704 | 7.7 | 197 | 41 |  |  |  |
|  | 2091 | NB | NBT | 936 | 861 | 29.8 | 416 | 136 |  |  |  |
|  | 2091 |  | NBR | 1234 | 1113 | 26.9 | 756 | 259 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 134 | 129 | 14.0 | 384 | 54 | 2,014 | 1,896 | 10.7 |
|  | 2247 |  | EBT | 1646 | 1550 | 9.9 | 384 | 54 |  |  |  |
|  | 2247 |  | EBR | 158 | 146 | 10.9 | 388 | 54 |  |  |  |
|  | 2247 | SB | SBL | 14 | 13 | 14.4 | 73 | 28 |  |  |  |
|  | 2247 |  | SBT | 19 | 18 | 32.6 | 73 | 28 |  |  |  |
|  | 2247 | NB | NBT | 29 | 30 | 21.9 | 58 | 13 |  |  |  |
|  | 2247 |  | NBR | 14 | 11 | 9.2 | 65 | 13 |  |  |  |
| NE Broadway \& NE 2nd Ave | 2248 | SB | SBT | 14 | 13 | 14.7 | 101 | 36 | 1,089 | 1,081 | 11.0 |
|  | 2248 |  | SBR | 91 | 91 | 10.5 | 103 | 36 |  |  |  |
|  | 2248 | WB | WBL | 19 | 18 | 6.2 | 323 | 86 |  |  |  |
|  | 2248 |  | WBT | 778 | 778 | 10.5 | 323 | 86 |  |  |  |
|  | 2248 |  | WBR | 24 | 24 | 11.9 | 325 | 86 |  |  |  |
|  | 2248 | NB | NBL | 29 | 30 | 14.7 | 163 | 25 |  |  |  |
|  | 2248 |  | NBT | 134 | 128 | 13.5 | 163 | 25 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Vancouver Ave \& N/NE Hancock St | 2249 | EB | EBT | 10 | 9 | 15.3 | 25 | 2 | 313 | 320 | 2.8 |
|  | 2249 |  | EBR | 0 | 0 | 0.0 | 25 | 2 |  |  |  |
|  | 2249 | WB | WBL | 5 | 3 | 6.3 | 84 | 21 |  |  |  |
|  | 2249 |  | WBT | 48 | 46 | 8.2 | 78 | 21 |  |  |  |
|  | 2249 | SB | SBT | 250 | 263 | 1.4 | 0 | 0 |  |  |  |
|  | 2249 |  | SBR | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
| N Williams Ave \& N/NE Multnomah St | 1066 | EB | EBT | 240 | 237 | 10.4 | 206 | 35 | 1,004 | 988 | 11.7 |
|  | 1066 |  | EBR | 5 | 6 | 11.7 | 206 | 35 |  |  |  |
|  | 1066 | SB | SBL | 202 | 189 | 15.1 | 175 | 23 |  |  |  |
|  | 1066 |  | SBT | 14 | 14 | 14.0 | 175 | 23 |  |  |  |
|  | 1066 |  | SBR | 101 | 102 | 14.3 | 110 | 32 |  |  |  |
|  | 1066 | WB | WBL | 0 | 0 | 0.0 | 113 | 9 |  |  |  |
|  | 1066 |  | WBT | 432 | 431 | 9.8 | 113 | 9 |  |  |  |
|  | 1066 | NB | NBT | 10 | 10 | 29.0 | 47 | 0 |  |  |  |
|  | 1066 |  | NBR | 0 | 0 | 0.0 | 47 | 0 |  |  |  |

Table F-9 Future Revised Build Alternative 2-Way Wheeler 8-9 A M


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume <br> Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Broadway \& N Larrabee Ave | 1010 | EB | EBT | 715 | 717 | 11.2 | 341 | 98 | 2,495 | 2,354 | 17.2 |
|  | 1010 |  | EBR | 245 | 235 | 37.2 | 406 | 66 |  |  |  |
|  | 1010 | SB | SBL | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1010 |  | SBT | 30 | 29 | 80.1 | 99 | 19 |  |  |  |
|  | 1010 | WB | WBL | 5 | 4 | 68.0 | 33 | 13 |  |  |  |
|  | 1010 |  | WBT | 1135 | 1017 | 2.3 | 203 | 53 |  |  |  |
|  | 1010 |  | WBR | 120 | 109 | 32.0 | 204 | 30 |  |  |  |
|  | 1010 | NB | NBL | 100 | 98 | 59.5 | 155 | 18 |  |  |  |
|  | 1010 |  | NBT | 65 | 63 | 60.7 | 155 | 18 |  |  |  |
|  | 1010 |  | NBR | 80 | 83 | 68.5 | 186 | 28 |  |  |  |
| N Weidler St \& N Vancouver Ave | 1055 | EB | EBT | 580 | 589 | 5.4 | 202 | 95 | 1,975 | 1,888 | 17.3 |
|  | 1055 |  | EBR | 260 | 252 | 30.9 | 310 | 48 |  |  |  |
|  | 1055 | SB | SBL | 20 | 22 | 30.8 | 267 | 16 |  |  |  |
|  | 1055 |  | SBT | 885 | 845 | 21.0 | 267 | 16 |  |  |  |
|  | 1055 | NB | NBT | 180 | 142 | 18.3 | 187 | 18 |  |  |  |
|  | 1055 |  | NBR | 50 | 37 | 18.0 | 187 | 18 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Wheeler Ave/ N Williams Ave/ N Ramsey Way \& I-5 SB Ramps | 1067 | EB | EBL | 0 | 0 | 0.0 | 78 | 14 | 1,615 | 1,500 | 38.0 |
|  | 1067 |  | EBT | 80 | 76 | 33.3 | 78 | 14 |  |  |  |
|  | 1067 |  | EBR | 20 | 19 | 32.4 | 78 | 14 |  |  |  |
|  | 1067 | WB | WBL | 130 | 115 | 81.3 | 513 | 41 |  |  |  |
|  | 1067 |  | WBR | 230 | 183 | 83.3 | 513 | 41 |  |  |  |
|  | 1067 | SB | SBL | 995 | 967 | 26.9 | 311 | 15 |  |  |  |
|  | 1067 |  | SBT | 150 | 131 | 21.9 | 188 | 53 |  |  |  |
|  | 1067 | NB | NBT | 10 | 10 | 41.1 | 47 | 0 |  |  |  |
| N/NE Weidler St \& N Williams Ave | 1068 | EB | EBL | 225 | 214 | 3.6 | 166 | 58 | 660 | 655 | 4.3 |
|  | 1068 |  | EBT | 425 | 432 | 4.0 | 163 | 58 |  |  |  |
|  | 1068 | NB | NBT | 10 | 10 | 31.1 | 47 | 0 |  |  |  |
| N Broadway \& N Benton Ave | 1098 | EB | EBL | 10 | 11 | 65.2 | 49 | 14 | 2,155 | 2,025 | 11.3 |
|  | 1098 |  | EBT | 755 | 761 | 5.0 | 248 | 38 |  |  |  |
|  | 1098 |  | EBR | 30 | 27 | 4.8 | 248 | 38 |  |  |  |
|  | 1098 | SB | SBL | 10 | 6 | 52.0 | 114 | 16 |  |  |  |
|  | 1098 |  | SBT | 25 | 22 | 51.1 | 114 | 16 |  |  |  |
|  | 1098 |  | SBR | 15 | 17 | 52.6 | 114 | 16 |  |  |  |
|  | 1098 | WB | WBL | 5 | 4 | 79.2 | 36 | 17 |  |  |  |
|  | 1098 |  | WBT | 1230 | 1101 | 11.2 | 489 | 84 |  |  |  |
|  | 1098 |  | WBR | 40 | 35 | 26.8 | 489 | 84 |  |  |  |
|  | 1098 | NB | NBL | 15 | 15 | 63.9 | 52 | 17 |  |  |  |
|  | 1098 |  | NBT | 15 | 17 | 55.5 | 85 | 13 |  |  |  |
|  | 1098 |  | NBR | 5 | 7 | 56.1 | 85 | 13 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 30 | 28 | 11.8 | 40 | 7 | 2,520 | 2,332 | 24.8 |
|  | 2001 | WB | WBT | 1560 | 1548 | 33.4 | 541 | 18 |  |  |  |
|  | 2001 |  | WBR | 10 | 12 | 56.0 | 541 | 18 |  |  |  |
|  | 2001 | NB | NBL | 865 | 699 | 7.0 | 178 | 55 |  |  |  |
|  | 2001 |  | NBT | 55 | 46 | 5.7 | 178 | 55 |  |  |  |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 15 | 14 | 25.5 | 202 | 35 | 2,780 | 2,348 | 17.7 |
|  | 2091 |  | EBT | 410 | 421 | 12.2 | 202 | 35 |  |  |  |
|  | 2091 | NB | NBT | 905 | 731 | 17.0 | 175 | 16 |  |  |  |
|  | 2091 |  | NBR | 1450 | 1183 | 20.0 | 582 | 65 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 100 | 90 | 7.0 | 258 | 66 | 1,945 | 1,676 | 5.9 |
|  | 2247 |  | EBT | 1750 | 1503 | 5.1 | 258 | 66 |  |  |  |
|  | 2247 |  | EBR | 10 | 7 | 4.1 | 262 | 66 |  |  |  |
|  | 2247 | SB | SBL | 25 | 22 | 15.3 | 65 | 16 |  |  |  |
|  | 2247 |  | SBT | 10 | 12 | 21.0 | 65 | 16 |  |  |  |
|  | 2247 | NB | NBT | 40 | 35 | 24.3 | 71 | 12 |  |  |  |
|  | 2247 |  | NBR | 10 | 8 | 9.2 | 77 | 12 |  |  |  |



Table F-10 Future Revised Build Alternative 2-Way Wheeler 5-6 PM

| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume <br> Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Williams Ave \& N/NE Hancock St | 1001 | EB | EBL | 10 | 10 | 34.2 | 63 | 11 | 645 | 613 | 32.5 |
|  | 1001 | WB | WBT | 50 | 45 | 111.1 | 288 | 48 |  |  |  |
|  | 1001 |  | WBR | 75 | 73 | 108.4 | 288 | 48 |  |  |  |
|  | 1001 | NB | NBL | 5 | 5 | 3.8 | 301 | 83 |  |  |  |
|  | 1001 |  | NBT | 485 | 464 | 14.1 | 301 | 83 |  |  |  |
|  | 1001 |  | NBR | 20 | 16 | 6.9 | 301 | 83 |  |  |  |
| N/NE Broadway \& N Williams Ave | 1008 | WB | WBT | 945 | 899 | 4.9 | 173 | 35 | 2,185 | 2,083 | 11.7 |
|  | 1008 |  | WBR | 860 | 797 | 14.1 | 299 | 17 |  |  |  |
|  | 1008 | NB | NBL | 30 | 28 | 26.3 | 240 | 9 |  |  |  |
|  | 1008 |  | NBT | 350 | 361 | 22.4 | 240 | 9 |  |  |  |
| N Broadway \& N Vancouver Ave | 1009 | SB | SBT | 220 | 222 | 32.5 | 227 | 26 | 1,485 | 1,377 | 17.3 |
|  | 1009 | WB | WBL | 370 | 355 | 9.6 | 130 | 39 |  |  |  |
|  | 1009 |  | WBT | 605 | 569 | 2.2 | 88 | 25 |  |  |  |
|  | 1009 | NB | NBL | 290 | 233 | 51.5 | 225 | 34 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Broadway \& N Larrabee Ave | 1010 | EB | EBT | 1150 | 1154 | 22.3 | 732 | 166 | 2,655 | 2,558 | 22.4 |
|  | 1010 |  | EBR | 280 | 276 | 38.1 | 488 | 115 |  |  |  |
|  | 1010 | SB | SBL | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1010 |  | SBT | 25 | 25 | 71.0 | 77 | 22 |  |  |  |
|  | 1010 | WB | WBL | 20 | 18 | 82.9 | 66 | 21 |  |  |  |
|  | 1010 |  | WBT | 860 | 777 | 2.2 | 205 | 58 |  |  |  |
|  | 1010 |  | WBR | 100 | 90 | 33.0 | 182 | 30 |  |  |  |
|  | 1010 | NB | NBL | 140 | 138 | 56.8 | 161 | 27 |  |  |  |
|  | 1010 |  | NBT | 5 | 6 | 47.3 | 161 | 27 |  |  |  |
|  | 1010 |  | NBR | 75 | 74 | 68.6 | 157 | 31 |  |  |  |
| N Weidler St \& $N$ Vancouver Ave | 1055 | EB | EBT | 1060 | 1077 | 5.5 | 284 | 66 | 2,265 | 2,211 | 15.5 |
|  | 1055 |  | EBR | 280 | 278 | 43.4 | 339 | 40 |  |  |  |
|  | 1055 | SB | SBL | 45 | 46 | 59.0 | 246 | 33 |  |  |  |
|  | 1055 |  | SBT | 545 | 538 | 25.4 | 246 | 33 |  |  |  |
|  | 1055 | NB | NBT | 290 | 233 | 28.2 | 225 | 11 |  |  |  |
|  | 1055 |  | NBR | 45 | 39 | 25.1 | 225 | 11 |  |  |  |



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| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 25 | 24 | 15.1 | 38 | 8 | 1,980 | 1,845 | 33.4 |
|  | 2001 | WB | WBT | 920 | 911 | 50.5 | 527 | 63 |  |  |  |
|  | 2001 |  | WBR | 15 | 13 | 138.2 | 527 | 63 |  |  |  |
|  | 2001 | NB | NBL | 860 | 761 | 17.1 | 272 | 5 |  |  |  |
|  | 2001 |  | NBT | 160 | 137 | 3.7 | 272 | 5 |  |  |  |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 45 | 39 | 10.0 | 195 | 41 | 3,040 | 2,756 | 23.9 |
|  | 2091 |  | EBT | 735 | 749 | 7.2 | 195 | 41 |  |  |  |
|  | 2091 | NB | NBT | 975 | 858 | 32.9 | 598 | 266 |  |  |  |
|  | 2091 |  | NBR | 1285 | 1110 | 28.6 | 685 | 129 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 140 | 141 | 15.3 | 419 | 53 | 2,100 | 1,934 | 10.8 |
|  | 2247 |  | EBT | 1715 | 1564 | 9.8 | 419 | 53 |  |  |  |
|  | 2247 |  | EBR | 165 | 153 | 11.0 | 422 | 53 |  |  |  |
|  | 2247 | SB | SBL | 15 | 14 | 13.4 | 68 | 14 |  |  |  |
|  | 2247 |  | SBT | 20 | 18 | 31.5 | 68 | 14 |  |  |  |
|  | 2247 | NB | NBT | 30 | 29 | 23.1 | 68 | 10 |  |  |  |
|  | 2247 |  | NBR | 15 | 15 | 11.1 | 75 | 10 |  |  |  |



Table F-11 Future Revised Build Alternative 2-Way Wheeler 7-8 A M

| Intersection | Node | Approach | Movement | Movement |  |  | Max <br> Queue <br> (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Williams Ave \& N/NE Hancock St | 1001 | EB | EBL | 8 | 8 | 21.9 | 64 | 21 | 490 | 488 | 15.5 |
|  | 1001 | WB | WBT | 50 | 49 | 29.5 | 167 | 20 |  |  |  |
|  | 1001 |  | WBR | 104 | 102 | 31.6 | 167 | 20 |  |  |  |
|  | 1001 | NB | NBL | 0 | 0 | 0.0 | 229 | 34 |  |  |  |
|  | 1001 |  | NBT | 320 | 324 | 8.2 | 229 | 34 |  |  |  |
|  | 1001 |  | NBR | 8 | 7 | 9.8 | 229 | 34 |  |  |  |
| N/NE Broadway \& N Williams Ave | 1008 | WB | WBT | 1274 | 1254 | 6.8 | 208 | 21 | 2,225 | 2,205 | 10.2 |
|  | 1008 |  | WBR | 764 | 756 | 12.3 | 278 | 12 |  |  |  |
|  | 1008 | NB | NBL | 33 | 38 | 11.4 | 157 | 9 |  |  |  |
|  | 1008 |  | NBT | 154 | 156 | 27.9 | 157 | 9 |  |  |  |
| N Broadway \& N Vancouver Ave | 1009 | SB | SBT | 249 | 251 | 35.4 | 285 | 51 | 1,705 | 1,691 | 10.9 |
|  | 1009 | WB | WBL | 502 | 501 | 10.4 | 172 | 21 |  |  |  |
|  | 1009 |  | WBT | 805 | 787 | 2.5 | 156 | 38 |  |  |  |
|  | 1009 | NB | NBL | 149 | 152 | 16.0 | 184 | 13 |  |  |  |


| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| N Broadway \& N Larrabee Ave | 1010 | EB | EBT | 593 | 603 | 8.8 | 235 | 98 | 2,070 | 2,071 | 15.4 |
|  | 1010 |  | EBR | 203 | 207 | 35.3 | 296 | 66 |  |  |  |
|  | 1010 | SB | SBL | 0 | 0 | 0.0 | 0 | 0 |  |  |  |
|  | 1010 |  | SBT | 25 | 21 | 80.4 | 66 | 19 |  |  |  |
|  | 1010 | WB | WBL | 4 | 3 | 20.7 | 26 | 13 |  |  |  |
|  | 1010 |  | WBT | 942 | 941 | 1.7 | 150 | 53 |  |  |  |
|  | 1010 |  | WBR | 100 | 95 | 31.7 | 167 | 30 |  |  |  |
|  | 1010 | NB | NBL | 83 | 79 | 60.2 | 158 | 18 |  |  |  |
|  | 1010 |  | NBT | 54 | 56 | 63.0 | 158 | 18 |  |  |  |
|  | 1010 |  | NBR | 66 | 68 | 68.9 | 182 | 28 |  |  |  |
| N Weidler St \& $N$ Vancouver Ave | 1055 | EB | EBT | 481 | 490 | 4.7 | 164 | 95 | 1,640 | 1,660 | 15.4 |
|  | 1055 |  | EBR | 216 | 217 | 24.7 | 266 | 48 |  |  |  |
|  | 1055 | SB | SBL | 17 | 19 | 31.0 | 261 | 16 |  |  |  |
|  | 1055 |  | SBT | 735 | 744 | 18.5 | 261 | 16 |  |  |  |
|  | 1055 | NB | NBTNBR | 149 | 151 | 18.6 | 190 | 18 |  |  |  |
|  | 1055 |  |  | 42 | 40 | 17.6 | 190 | 18 |  |  |  |



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| Intersection | Node | Approach | Movement | Movement |  |  | Max Queue (feet) | Std. Dev. (feet) | Volume Demand (vph) | Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |  |  |  | Volume Served (vph) | Vehicle Delay (sec) |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 25 | 24 | 9.7 | 33 | 7 | 2,092 | 2,069 | 18.2 |
|  | 2001 | WB | WBT | 1295 | 1290 | 25.8 | 485 | 18 |  |  |  |
|  | 2001 |  | WBR | 8 | 10 | 40.9 | 485 | 18 |  |  |  |
|  | 2001 | NB | NBL | 718 | 701 | 5.0 | 127 | 55 |  |  |  |
|  | 2001 |  | NBT | 46 | 45 | 6.5 | 127 | 55 |  |  |  |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 12 | 12 | 25.3 | 162 | 35 | 2,307 | 2,291 | 18.0 |
|  | 2091 |  | EBT | 340 | 350 | 10.7 | 162 | 35 |  |  |  |
|  | 2091 | NB | NBT | 751 | 732 | 17.4 | 192 | 16 |  |  |  |
|  | 2091 |  | NBR | 1204 | 1196 | 20.5 | 611 | 65 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 83 | 81 | 6.4 | 227 | 66 | 1,614 | 1,609 | 5.4 |
|  | 2247 |  | EBT | 1453 | 1455 | 4.8 | 227 | 66 |  |  |  |
|  | 2247 |  | EBR | 8 | 7 | 3.7 | 230 | 66 |  |  |  |
|  | 2247 | SB | SBL | 21 | 20 | 16.5 | 55 | 16 |  |  |  |
|  | 2247 |  | SBT | 8 | 10 | 20.2 | 55 | 16 |  |  |  |
|  | 2247 | NB | NBT | 33 | 29 | 24.4 | 64 | 12 |  |  |  |
|  | 2247 |  | NBR | 8 | 6 | 8.2 | 71 | 12 |  |  |  |



Table F-12 Future Revised Build Alternative 2-Way Wheeler 4-5 PM




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| Intersection | Node | Approach | Movement | Movement |  |  |  |  | Intersection |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volume Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) | Max Queue (feet) | Std. Dev. (feet) | Volume <br> Demand (vph) | Volume Served (vph) | Vehicle Delay (sec) |
| NE Broadway \& NE Victoria Ave | 2001 | SB | SBR | 24 | 23 | 12.6 | 34 | 10 | 1,901 | 1,812 | 27.2 |
|  | 2001 | WB | WBT | 883 | 875 | 39.9 | 511 | 66 |  |  |  |
|  | 2001 |  | WBR | 14 | 14 | 98.7 | 511 | 66 |  |  |  |
|  | 2001 | NB | NBL | 826 | 758 | 16.1 | 268 | 23 |  |  |  |
|  | 2001 |  | NBT | 154 | 143 | 3.5 | 268 | 23 |  |  |  |
| NE Weidler St \& NE Victoria Ave/ I-5 NB Ramp | 2091 | EB | EBL | 43 | 40 | 9.8 | 192 | 42 | 2,919 | 2,724 | 23.6 |
|  | 2091 |  | EBT | 706 | 708 | 7.2 | 192 | 42 |  |  |  |
|  | 2091 | NB | NBT | 936 | 864 | 31.6 | 551 | 204 |  |  |  |
|  | 2091 |  | NBR | 1234 | 1112 | 28.4 | 724 | 229 |  |  |  |
| NE Weidler St \& NE 2nd Ave | 2247 | EB | EBL | 134 | 129 | 14.1 | 412 | 40 | 2,014 | 1,896 | 10.9 |
|  | 2247 |  | EBT | 1646 | 1549 | 10.1 | 412 | 40 |  |  |  |
|  | 2247 |  | EBR | 158 | 146 | 11.6 | 416 | 40 |  |  |  |
|  | 2247 | SB | SBL | 14 | 13 | 14.0 | 73 | 28 |  |  |  |
|  | 2247 |  | SBT | 19 | 18 | 31.1 | 73 | 28 |  |  |  |
|  | 2247 | NB | NBT | 29 | 30 | 21.7 | 58 | 13 |  |  |  |
|  | 2247 |  | NBR | 14 | 11 | 8.2 | 65 | 13 |  |  |  |



## Appendix G: 2045 No Build and 2045 Build AM and PM Peak Hour Bike Volumes

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[^6]



[^0]:    ${ }^{1}$ City of Portland operational target: LOS D for signalized intersections and LOS E for unsignalized intersections. n.d. Portland Policy Document. TRN-10.27 - Traffic Capacity Analysis for Land Use Review Cases. Available: https://www.portlandoregon.gov/citycode/article/41049

[^1]:    ${ }^{2}$ The time during which a given traffic movement or set of movements may proceed; it is equal to the cycle length minus the effective red time.
    Traffic Signal Timing Manual: Chapter 3-Office of Operations (dot.gov)

[^2]:    ${ }^{3}$ Pedestrians were modeled using traditional "vehicle" inputs with footpath (no interaction) behavior on crosswalk links as opposed to the VisWalk functionality in Vissim.

[^3]:    ${ }^{1}$ I-205 Toll Project Comparison of Screening Alternatives (March 31, 2021).
    https://www.oregon.gov/odot/tolling/Documents/FINAL\%20I-
    205\%20Comparison\%20of\%20Screening\%20Alternatives\%20Report\%20033121 508.pdf

[^4]:    ${ }^{4}$ ODOT Analysis Procedures Manual Version 2 Appendix 10A - Auxiliary Lanes, APM Appendix 10A

[^5]:    Revised Traffic Analysis Supplemental Technical Report

[^6]:    Revised Traffic Analysis Supplemental Technical Report

